HUGHES DEVELOPMENT LLC

Petition for Zoning Map Amendment Wake County, North Carolina

Case No. PLG-RZ-001350-2019

Revised Submittal: March 12, 2021 Updated: April 7, 2021 April 23, 2021

Prepared for:

Hughes Development LLC 901-F Paverstone Drive Raleigh NC 27615

Prepared by:

Andrew Petesch Petesch Law 127 W. Hargett Street, Suite 500 Raleigh, NC 27601 (919) 747-8611 andy@peteschlaw.com

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Location & Vicinity Map



The subject property, highlighted in red above, is an undeveloped parcel created as part of the Huntsboro subdivision circa 1998. At that time, access was only available from the south via Knotts Hill Place, which would require crossing a USGS stream. An alternate plan for access to and development of the subject parcel would allow preservation of environmentally sensitive land on both sides of the stream as open space.

Rutledge Landing Subdivision Phase 3 to the immediate west of the subject property provides new connectivity to the subject parcel via Rutledgeville Lane (indicated by green star in the map above). This would provide ingress and egress through both the Ashley Hills subdivision to the north and through the Rutledge Landing subdivision to the south. Ashley Hills provides close access to Pine Run and Sandy Run, both designated as collector streets on the Wake County Collector Street Plan, which feed Smithfield Road. Rutledge Landing provides close access to Rutledge Landing Drive, which feeds into Poole Road.

Project Data

PIN: 1763007038

Property Address: 900 Knotts Hill Place, Knightdale NC 27545-8112

Property Size: 10.08± acres

Property Status: Vacant – Wooded

Current Zoning Designation: Residential-30 (R-30)

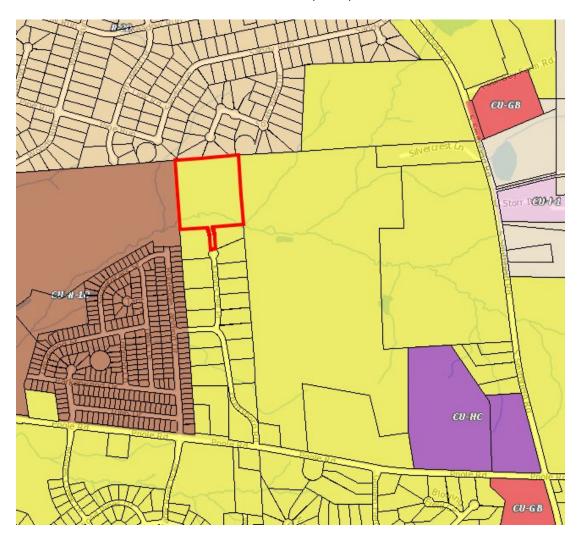
Proposed Zoning Designation: Conditional Use-Residential-10 (CU-R-10)

Existing Area Zoning:

North Area: Residential-20 (R-20)

• West Area: Conditional Use-Residential-10 (CU-R-10)

East Area: Residential-30 (R-30)
South Area: Residential-30 (R-30)



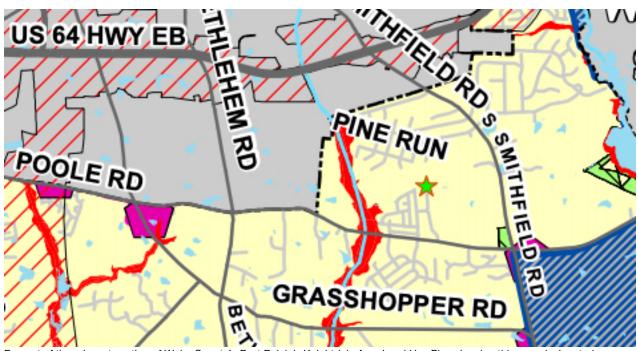
Area Land Use Plan: East Raleigh / Knightdale

Short Range Planning Area: Knightdale

Current Land Use Plan Designation: Residential (Less Than 1.5 Units Per Acre)

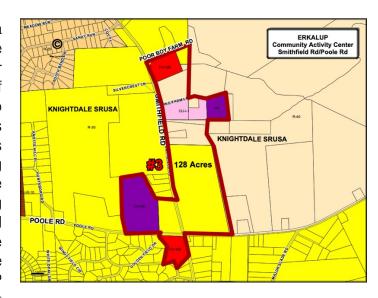
Proposed Land Use Plan Designation: Residential (1.5 to 4 Units Per Acre)

Land Use Plan Amendment Petition: PLG-LUPA-002583-2020



Excerpt of the relevant section of Wake County's East Raleigh-Knightdale Area Land Use Plan showing this area designated as Residential less than 1.5 dwelling units per acre. The subject property is shown with the green star.

The Petitioner seeks to maintain a Residential land use designation, but one that allows up to four (4) dwelling units per acre, rather than the current maximum of 1.5 units per acre. Such an amendment to the Land Use Plan and associated maps would increase the Subject Property's compatibility with the current zoning designations and developments to the North and West. See Existing Area Zoning Map supra. The Subject Property is located approximately miles from 0.9 intersection of Smithfield Road and Poole Road, which is the hub of a LUP Community Activity Center. See East Raleigh-Knightdale Area Land Use Plan (ERKALUP) Map.



Rezoning Petition Narrative

How is this proposed use a public necessity?

The subject ten (10±) acre parcel was originally part of the Huntsboro Subdivision, but was left undeveloped (i.e. reserved by the owner) in large part due to feasibility challenges of crossing an environmentally sensitive stream area (e.g. Neuse River stream buffers, flood hazard soils, and steeper slopes) on the southern portion of the property. The proposed rezoning from Residential-30 (R-30) to Residential-10 (R-10) would allow for the construction of up to 26 additional single-family homes (i.e. 40 versus 14 homes). Housing is generally accepted as a public necessity.

The Wake County Land Use Plan (LUP), when adopted many years ago, projected that the County population would exceed one million people by 2027. (LUP p. I.1). The North Carolina State Demographer Office's current population estimate for Wake County as of July 2020 was 1,109,883. That Office's projection for July 2025 is 1,217,614 – demonstrating that continued strong growth and population increase is expected. Therefore, in addition to housing being a public necessity, there is an ongoing market need for housing in Wake County.

What is the impact on adjacent properties and the surrounding neighborhood?

The Subject Parcel is currently zoned R-30, and this rezoning petition requests a change in the base zoning district to R-10. The Wake County Unified Development Ordinance (UDO) Use Table shows that the permitted uses in both zoning districts are identical, with the only difference being the allowed density for single-family detached dwellings. In addition, the setbacks and vegetative buffers required around the perimeter of the proposed subdivision are essentially identical regardless of whether it is developed under the density limits of R-30 or R-10.

The R-10 zoning would allow for up to 40 single-family homes versus a maximum of 14 under the existing R-30 zoning. While the additional homes would lead to additional traffic on the area road network, it is well below what is required to trigger a formal Traffic Impact Analysis ("TIA"). Even though a formal TIA is not required, the Wake County Planning Staff required a detailed Traffic Assessment Statement, which was prepared by the engineering firm Ramey Kemp Associates. After performing a thorough analysis, the traffic engineer concluded that the increased traffic associated with an R-10 zoning designation and a proposed 40-parcel residential subdivision is expected to have minimal impact on key intersections in the area. Residential development of the Subject Property under a R-10 designation is not predicted to adversely affect the level of service of the roadways and intersections studied, even accounting for annual background traffic growth and the addition of the future traffic from Rutledge Landing Phases 3 and 4.

Connection to existing and underutilized community water and sewer service with sufficient capacity for a 40-lot residential subdivision mitigates any potential adverse impacts to the water quality, water pressure, and wastewater treatment of neighboring residential properties. These systems, which currently serve the adjacent Rutledge Landing subdivision, are permitted by the State of North Carolina and are operated and maintained by Carolina Water Service of North Carolina.

Petitioner has held multiple meetings with neighboring residents. A summary of those meetings is attached as Exhibit A.

How does the proposed use benefit the adjacent and surrounding properties?

An increase in density under a R-10 zoning designation allows for subdivision development that connects to Phase 3 of the Rutledge Landing subdivision, which also has a R-10 base zoning. With a street connection via Rutledgeville Lane, the Petitioner is able to offer a condition that prohibits access through the Huntsboro Subdivision to the south. This change in access allows for the preservation of a natural area, which includes a USGS stream and ensures that area can be designated as open space and will not be disturbed.

Development of a small subdivision on the subject property would extend Rutledgeville Lane across the parcel to the large vacant tracts between this property and Smithfield Road, which will provide future street connectivity on the east side of the Subject Property and support growth of the nearby Smithfield Rd / Poole Rd Community Activity Center. Interconnected roadways generally result in more efficient movement of traffic, especially for school buses, trash pick-up, delivery vehicles, dispersion of traffic, and emergency response vehicles, although these benefits may not be fully realized until the properties to the east are developed. If the subject property were developed pursuant to its current zoning designation and as a single parcel, this connectivity link could not exist.

Statement of How the Rezoning Complies with the Land Use Plan

This Rezoning Petition is accompanied by a Land Use Plan Amendment Petition requesting a change to Residential (1.5 to 4 Units Per Acre). Although the Subject Property was designated as Residential Less Than 1.5 Units Per Acre when the East Raleigh/Knightdale Area Land Use Plan map was created, the type of growth in the vicinity of the Subject Property makes an amendment to the ERKALUP map reasonable, appropriate, and – on balance – compatible with the Wake County Land Use Plan. Additionally, the LUP envisions the County as

an outstanding community of urban and rural areas, where the demand for quality and affordable growth is met, economic development and opportunity is enhanced, environmental quality and cultural heritage are maintained, and all of these objectives are balanced with protecting the property rights of landowners.

(LUP p II.1). Plotting a path to this vision, the LUP sets out eleven goals and strategies, including:

- To encourage growth close to municipalities, to take advantage of existing and planned infrastructure, such as transportation, water and sewer facilities.
 - o (Goal #2)
- To encourage the development of communities which provide adequate land for anticipated demands, in a pattern which allows a mixture of uses.
 - o (Goal #3)
- To ensure that the land use plan and transportation plan mutually support each other.
 - o (Goal #7)
- To ensure that the County always protects the property rights of landowners.
 - o (Goal #8)

The Subject Property is within the Town of Knightdale's Short-Range Urban Services Area ("SRUSA"). The LUP established Urban Services Area classifications to define areas in the County's jurisdiction expected and intended to be urbanized in the foreseeable future, i.e. "developed at the range of urban intensities typically found in area municipalities, served by the urban facilities and services typically available in municipalities, and eventually becoming part of an adjacent municipality." (LUP p III.1). SRUSAs are most closely connected to Goal #2's call for encouraging growth close to municipalities, Goal #3's call for ensuring the availability of sufficient land zoned for short-range growth demands, and Goal #7's call for ensuring planning transportation facilities in relation to planned growth and promoting transit-oriented development. (LUP p III.3).

The proposed amendment will allow for increased residential density on a parcel that was originally reserved by the developer of the Huntsboro Subdivision ("Huntsboro"). Developed between 1994 and 1998, Huntsboro is comprised of 17 parcels, generally ranging from 1 to 2 acres and improved with single-family detached homes. The Subject Property was the 18th Huntsboro lot and located at the north end of the subdivision. It is significantly larger than the other Huntsboro lots at 10.08± acres. The requested rezoning is comparable to the adjacent existing development to the north and west.

North of the Subject Property is the Ashley Hills Subdivision ("Ashley Hills"), which was developed in the 1980s and includes over 200 lots ranging generally from .45 to .80 acres. Although Ashley Hills is designated as Residential Less Than 1.5 Units Per Acre on the ERKALU map, the subdivision is zoned R-20, which supports a density of approximately 2.1 units per acre.

West of the Subject Property is the Rutledge Landing Subdivision ("Rutledge Landing"). Rutledge Landing Phase 1 was developed around 2001, Phase 2 around 2003, and Phases 3 and 4, which are currently under construction or pending. Although Rutledge Landing is

designated as Residential Less Than 1.5 Units Per Acre on the ERKALU map, the subdivision is zoned CU-R-10, which supports a density of just over 4.0 units per acre.

East of the Subject Property is an 86.2 acre property, which is largely undeveloped. That property is designated as Residential Less Than 1.5 Units Per Acre on the ERKALU map and zoned R-30.

The Subject Property is also covered by the East Raleigh-Knightdale Area Land Use Plan. The proposed LUPA is consistent with that Plan's adopted goals including:

#2 Encourage growth that will take advantage of existing and planned infrastructure so that municipalities are able to provide basic public services in accordance with their adopted plans.

The subject property will utilize existing infrastructure such as community water and sanitary sewer, which allows for increased density without imposing on public water and sewer resources. Per UDO § 12-11-1(C)(5), proposed water and wastewater systems must be designed and installed in accordance with the applicable standards of the relevant municipality (in this case the Town of Knightdale).

#3 Focus compact development in mixed-use activity centers that include housing, commercial services and employment opportunities designed with convenient pedestrian and vehicular access from surrounding development areas.

The Subject Property is located approximately 0.9 miles from the intersection of Smithfield Road and Poole Road, which is the hub of a LUP Community Activity Center. Increased density in proximity to an activity center is supportive of mixed-use development and growth.

In response to Petitioner's inquiry, Knightdale Planning Staff indicated that the proposed change in allowed density would be inconsistent with the KnightdaleNext 2035 Comprehensive Plan ("2035 Comp Plan").

However, Knightdale Planning Staff also noted that the 2035 Comp Plan uses a "playbook approach" that allows for aspects of the Plan to evolve over time as conditions change. (See attached 2035 Comp Plan excerpt (Exhibit B)). Because the Subject Property is in the County's planning jurisdiction rather than Knightdale's, there is no opportunity for the Town to apply these playbook principles to the Subject Property and make a determination as to whether current conditions would actually align this rezoning request with the 2035 Comp Plan. Consequently, Planning Staff could not consider current conditions in providing their comment on Plan consistency.

Compliance with Transitional Urban Development Policies

The subject property will be served by centralized community water and sanitary sewer. Allowing for increased density will help better utilize existing water and sewer capacity without directly impacting the capacity of public water and sewer services. A letter from Carolina Water Service of North Carolina confirming capacity for up to 40 parcels adjacent to the Rutledge Landing subdivision is attached as Exhibit C. Connectivity to community water and sewer allows for the promotion of more urban intensities. Per UDO § 12-11-1(C)(5), proposed water and wastewater systems must be designed and installed in accordance with the applicable standards of the relevant municipality (in this case the Town of Knightdale).

As noted above, development of the Subject Property as a small subdivision would extend Rutledgeville Lane to the large vacant tracts between the Subject Property and Smithfield Road, which would provide future street connectivity on the east side of the Subject Property and help support growth of the nearby Smithfield Rd / Poole Rd Community Activity Center.

Statement of How Rezoning Otherwise Advances the Public Health, Safety, and General Welfare

As discussed above, given recent growth in the area, new street connectivity through Phase 3 of the Rutledge Landing subdivision, availability of community water and sewer, and identical permitted uses as is currently allowed, the requested zoning change is compatible with surrounding uses. In addition, the requested CU-R-10 rezoning would allow a cluster subdivision development that preserves the natural areas on the southern portion of the Subject Property both by the rezoning condition prohibiting access via Knotts Hill place and by designation of open space in the subdivision approval process. Not only does this prevent disturbance of a U.S.G.S. stream, but also provides a substantial buffer for the existing lower-density residential development to the south.

As noted in the next section, a very detailed Traffic Assessment Statement was prepared by Ramey Kemp Associates. Their conclusion was that the increased traffic associated with an R-10 zoning designation and proposed residential subdivision is expected to have minimal impact on key intersections in the area.

Traffic Impact Analysis Requirement: Traffic Assessment Statement

The proposed land use plan amendment does not trigger either the 100 peak hour trips or 1000 trips per day thresholds that would require the preparation of a formal traffic impact analysis. In consultation with Planning Staff, the Petitioner has attached a Traffic Assessment Statement prepared by Ramey Kemp Associates. Based on that assessment, the increased traffic associated with the proposed residential subdivision developed pursuant to an R-10 zoning designation is expected to have a minimal impact on the studied intersections.

Rezoning Petition Addendum (Miscellaneous Section)

Valuable natural features (rare plant community, wildlife habitat, lake, stream, geology, etc.) on or adjoining site:

A USGS perennial stream runs from east to west across the southern portion of the Subject Property. There are 50-foot Neuse River buffers on either side of this perennial stream as well as Wake County flood hazard soils. Environmentally sensitive areas will be protected in accordance with the provisions of the Wake County UDO and other applicable State laws. Amending the LUP to allow higher residential density will allow development of a cluster subdivision whereby the environmentally sensitive areas associated with the perennial stream will be preserved and protected in their natural state. Additionally, the steeper slopes dropping down to the stream are heavily wooded and would serve as a natural buffer/screen between such development and the lower-density Huntsboro subdivision to the south.

There are no known existing rare plants or wildlife habitats that will be adversely impacted by the proposed map amendment.

Hughes Development LLC Rezoning Case No. ZP-900-19

Neighborhood Meeting Summaries

I. 2019 Neighborhood Meeting

A neighborhood meeting was held on Thursday, March 21, 2019 from 5:30pm to 7:30pm at the Marsh Creek Park Community Center, 3050 N New Hope Road. The following members of the applicant team were present:

Richard Stockett, Principal, Hughes Development LLC Andy Petesch, Attorney, Petesch Law James McConnell, Spanish Interpreter, N.C. State University

An estimated 40-50 people attended the March 21, 2019 neighbor meeting. The following people signed the attendance sheets (attached hereto):

- Lisa Wynn Newbanks
- Robert Newbanks
- Anonymous (Huntsboro Rd)
- Kreais
- Dustin Worley
- Amy Worley
- Chris Koch
- Pat Koch
- Shirley M Smith
- Vance Smith, Jr.
- Tony C. Veale

- Deborah Veale
- Richie Savage
- Michael Little
- Ida Little
- Roque Montano
- Maria Montano
- Tommy Gresham
- Dawn Zuccarini
- Art Threatt
- Suzanne Mealy
- Bryan Morgan

Mr. Petesch began the meeting by orienting the group to the subject property and providing an overview of the proposed rezoning.

The group asked a variety of questions focused on the following topics:

- Subdivision access through Huntsboro Subdivision
- Safety & Crime Issues
- Screening & Buffer on South Boundary
- Covenants
- Traffic from Rutledge Landing through Huntsboro Subdivision

There was discussion about the process for rezoning approvals, including Planning Board meeting and public hearing before the Board of Commissioners.

Mr. Petesch and Mr. Stockett offered to remain in contact with attendees, reminding them that the letter from Mr. Petesch included his contact information.

II. 2020 Neighborhood Meetings

Hughes Development held a second set of neighbor meetings on October 19, 20, and 21, 2020. Due to the pandemic, these meetings were held by video conference on Zoom. A telephone call-in number was also provided. The notice and invitation letter were sent to approximately 400 area property owners. Given the number of invitees, meetings were generally divided by adjacent neighborhood to more efficiently address respective concerns.

A. The first neighborhood meeting was held on Monday, October 19, 2020 from 7:00pm to 8:00pm. The following members of the applicant team were present at each meeting:

Richard Stockett, Principal, Hughes Development LLC Andy Petesch, Attorney, Petesch Law

Approximately 10 people attended the October 19, 2020 neighbor meeting, including but not limited to:

- Dawn Zuccarini
- Art Threat
- Melanie Hall

Mr. Petesch began the meeting by updating the attendees on the Petitioner's rezoning request since the last meeting and providing an overview of the proposed rezoning.

Attendee guestions focused on the following topics:

- Subdivision access through Huntsboro Subdivision
- Screening & Buffer on South Boundary
- Covenants
- Procedural aspects of rezoning process

There was discussion about the process for rezoning approvals, including Planning Board meeting and public hearing before the Board of Commissioners.

Mr. Petesch and Mr. Stockett offered to remain in contact with attendees, reminding them that the letter from Mr. Petesch included his contact information.

B. The second neighborhood meeting was held on Tuesday, October 20, 2020 from 7:00pm to 8:00pm. The following members of the applicant team were present at each meeting:

Richard Stockett, Principal, Hughes Development LLC Andy Petesch, Attorney, Petesch Law

Approximately 6-8 people attended the October 20, 2020 neighbor meeting, including but not limited to:

- Bonnie Hart
- Kathie Watkins
- Phyllis Fairley-Keating
- Marniece Bryant

Mr. Petesch began the meeting by updating the attendees on the Petitioner's rezoning request since the last meeting and providing an overview of the proposed rezoning.

Attendee questions focused on the following topics:

- Relation to Rutledge Landing Subdivision
- Open space on west side of Stoll Lane
- Driveway access to Stoll Lane
- Procedural aspects of rezoning process

There was discussion about the process for rezoning approvals, including Planning Board meeting and public hearing before the Board of Commissioners.

Mr. Petesch and Mr. Stockett offered to remain in contact with attendees, reminding them that the letter from Mr. Petesch included his contact information.

C. The third neighborhood meeting was held on Wednesday, October 21, 2020 from 7:00pm to 8:00pm. The following members of the applicant team were present at each meeting:

Richard Stockett, Principal, Hughes Development LLC Andy Petesch, Attorney, Petesch Law

Approximately 14-16 people attended the October 21, 2020 neighbor meeting, including but not limited to:

- Tanyon Rainey
- Michael Passer
- Palmer & Vickie Randall
- Patrick Lynch
- Phyllis Rush

Mr. Petesch began the meeting by updating the attendees on the Petitioner's rezoning request since the last meeting and providing an overview of the proposed rezoning.

Attendee guestions focused on the following topics:

- Screening & Buffer on North Boundary
- HOA effects on Ashley Hills subdivision and property owners
- Potential zoning changes to properties within the Ashley Hills subdivision
- Traffic impacts
- Environmental impacts
- Procedural aspects of rezoning process

There was discussion about the process for rezoning approvals, including Planning Board meeting and public hearing before the Board of Commissioners.

Mr. Petesch and Mr. Stockett offered to remain in contact with attendees, reminding them that the letter from Mr. Petesch included his contact information.

- **D.** The neighbor meeting letter noted that anyone who was not able to attend could contact Mr. Petesch by phone or email. The following property owners made inquiries by email either because they could not attend a meeting or had follow-up questions (correspondence attached):
 - Sharon Andrews (obo Dustin & Amy Worley)
 - Jesse Forte
 - Levaisha Eley
 - Patrick Lynch
 - Michael Passer

III. Supporting Documents

Documents related to the neighbor meetings, including notice letters and mailing lists, have been uploaded to Permit Portal separately.

From: Andrew Petesch apetesch@peteschlaw.com

Subject: Re: Proposed Rezoning - Hughes Development - Knotts Hill Place

Date: March 11, 2021 at 4:43 PM

To: Sharon Andrews sandrews@eratrlangle.com



From: Sharon Andrews <sandrews@eratriangle.com>

Date: Friday, October 16, 2020 at 3:52 PM

To: Andrew Petesch <apetesch@peteschlaw.com>

Cc: Dustin Worley <dustin.4seasons@gmail.com>, Amy Worley <amyworley4@gmail.com>

Subject: Re: Proposed Rezoning - Hughes Development - Knotts Hill Place

Thanks Andy for the quick response and explanation! They will have a better weekend now!!!

Thanks so much!!

Sharon Andrews,
MIRM, CSP, NC Real Estate Broker | Luxury Distinctive Properties Specialist
Relocation Specialist | Navy Federal Certified & CNAS

On Fri, Oct 16, 2020 at 3:45 PM Andrew Petesch apetesch@peteschlaw.com wrote:

Sharon,

Thank you for your questions. The rezoning is to allow for development of single-family detached homes more compatible with (but separate from) the Rutledge Landing subdivision. It would <u>not</u> include townhomes, only single-family detached homes.

Also, as a condition to this request, access to the subdivision would be through the newest phase of Rutledge Landing (Rutledgeville Lane). No access would be available through Knotts Hill Place, thereby protecting both the stream that runs across the southern portion of the subject property and the character of the Huntsboro Subdivision, which is lower density. The drawing on the back of my letter shows the boundaries of the subject property, which was originally intended to be part of the Huntsboro subdivision. As such, it still includes the anticipated access to Knotts Hill Place. My client will voluntarily close that access and connect to the new Rutledgeville Lane street instead.

Please let me know if you or your family members have any other questions about the proposed rezoning or residential subdivision.

With kind regards,

Andy

Andrew J. Petesch
Petesch Law
127 W. Hargett St., Suite 500
Raleigh, North Carolina 27601
T: (919) 747-8611

E: andy@peteschlaw.com

From: Sharon Andrews <sandrews@eratriangle.com>

Date: Friday, October 16, 2020 at 3:30 PM

To: Andrew Petesch apetesch@peteschlaw.com>

Cc: Dustin Worley < dustin.4seasons@gmail.com >, Amy Worley

<amyworley4@gmail.com>

Subject: Proposed Rezoning - Hughes Development - Knotts Hill Place

Hey Andy,

I'm emailing you in response to your letter of notification of a Zoom meeting on Monday, 10/19/2020 regarding the above referenced. My daughter and son-in-law live on Huntsboro Road and they would like to know if this is trying to be rezoned to townhomes? And if so, will those residents use Huntsboro Road to access the property?

Thanks so much!!

Sharon Andrews.

MIRM, CSP, NC Real Estate Broker | Luxury Distinctive Properties Specialist Relocation Specialist | Navy Federal Certified & CNAS

Subject: Re: Proposed rezoning meeting

Date: Wednesday, October 21, 2020 at 2:52:15 PM Eastern Daylight Time

From: Andrew Petesch <apetesch@peteschlaw.com>

To: Phyllis Fairley-Keaton <itsanewday2003@hotmail.com>

Phyliis,

Thank you for participating. Please let me know if you have any questions in the future.

With kind regards, Andy

Andrew J. Petesch
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Raleigh, North Carolina 27601
T: (919) 747-8611

F: (888) 848-9605 E: andy@peteschlaw.com

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From: Phyllis Fairley-Keaton <itsanewday2003@hotmail.com>

Date: Tuesday, October 20, 2020 at 7:34 PM

client, work product, or other applicable privilege. Thank you.

To: Andrew Petesch <apetesch@peteschlaw.com>

Subject: Proposed rezoning meeting

Hi Mr. Petesch:

My name is Phyllis. I am a home owner in Rutledge Landing. All of my questions were answered tonight. Thank you for the information.

Kindest Regards,

Phyllis

Sent from my Verizon, Samsung Galaxy smartphone Get Outlook for Android Subject: Re: Proposed Rezoning

Date: Sunday, October 25, 2020 at 4:13:51 PM Eastern Daylight Time

From: Andrew Petesch <apetesch@peteschlaw.com>

To: Jesse Forte <junior1forte@gmail.com>

Mr. Forte,

Thank you for contacting me with your questions. Because I am not your attorney, the NC State Bar's Rules of Professional Conduct prevent me from advising you as to how the proposed rezoning would affect your property or the Ashley Hills subdivision. I hope you understand that limitation on what I can tell you.

I can share objective information about our request. The owner of the property, Hughes Development, plans to develop that property as a small subdivision of approximately 38-40 lots, which would be consistent with the density in the Rutledge Landing subdivision. The proposed Hughes subdivision would have street access through Rutledge Landing, which avoids any disturbance of the stream that crosses the southern portion of the property.

I hope you find this helpful. Please let me know if you have any additional questions or comments.

With kind regards, Andy

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From: Jesse Forte <junior1forte@gmail.com> Date: Friday, October 23, 2020 at 1:03 AM

To: Andrew Petesch <apetesch@peteschlaw.com>

Subject: Proposed Rezoning

Hello Mr. Petesch,

I'm sorry I'm missed the virtual community meeting however; I do have a questions for you, this proposed rezoning what will this mean for me as regards to 205 Meadow Run, Knightdale, NC 27545.

The letter states that this site is currently zoned Residential-30 (R-30) and is proposed to be rezoned to conditional-Residents-10 so what does that mean? And how will it affect my property or subdivision?

So please feel free to get in contact with me

And I like to thank you for your time and consideration.

Jesse Jr. Forte (919) 803-0783

Subject: Re: Proposed Rezoning- Knotts Hill Place

Date: Sunday, October 25, 2020 at 4:20:32 PM Eastern Daylight Time

From: Andrew Petesch <apetesch@peteschlaw.com>

To: L Eley <eleylhe@gmail.com>

Thank you for contacting me with your questions. In an abundance of caution, I'd like to start out by clarifying that because I am not your attorney, the NC State Bar's Rules of Professional Conduct prevent me from advising you as to how the proposed rezoning would affect neighboring property owner's property. I hope you understand that limitation on what I can discuss.

I can share objective information about our request. The owner of the property, Hughes Development, plans to develop that property as a small subdivision of approximately 38-40 lots, which would be consistent with the density in the Rutledge Landing subdivision. The proposed Hughes subdivision would have street access through Rutledge Landing, which avoids substantial disturbance to the stream that crosses the southern portion of the property.

One of the key results of the meeting was a discussion about what could be done to mitigate the potential impacts to those property owners in Ashley Hills that directly abut the proposed development.

I hope you find this helpful. Please let me know if you have any additional questions or comments.

With kind regards, Andy

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From: L Eley <eleylhe@gmail.com>

Date: Wednesday, October 21, 2020 at 2:38 PM **To:** Andrew Petesch apetesch@peteschlaw.com **Subject:** Proposed Rezoning- Knotts Hill Place

Hello,

I was unable to attend the virtual meeting held yesterday. I am inquiring about the result of the meeting and also details of the development. Please advise.

Thank you

Subject: Re: R-30 or R-20?

Date: Sunday, October 25, 2020 at 4:28:37 PM Eastern Daylight Time

From: Patrick Lynch <patricklynch1969@gmail.com>
To: Andrew Petesch <apetesch@peteschlaw.com>

Attachments: image001.jpg

Thanks so much. Enjoy your weekend



From: Andrew Petesch apetesch@peteschlaw.com

Sent: Sunday, October 25, 2020 4:27:11 PM
To: Patrick Lynch cpatricklynch1969@gmail.com>

Subject: Re: R-30 or R-20?

Mr. Lynch,

Thank you for attending and for your follow-up questions. Wake County GIS indicates that the Ashley Hills subdivision is zoned R-20:





If the parcel highlighted in red above is rezoned from R-30 to R-10, none of the zoning designations of the surrounding properties with be changed or otherwise altered. The only zoning designation change would be to the Hughes Development property (highlighted in red).

Please let me know if you have any additional comments or questions.

With kind regards, Andy

Andrew J. Petesch

Petesch Law

127 W. Hargett St., Suite 500 Raleigh, North Carolina 27601

T: (919) 747-8611 F: (888) 848-9605

E: andy@peteschlaw.com

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From: Patrick Lynch <patricklynch1969@gmail.com>

Date: Thursday, October 22, 2020 at 9:40 AM **To:** Andrew Petesch apetesch@peteschlaw.com

Subject: R-30 or R-20?

Hello sir,

I'd like to thank you for how you conducted the Zoom meeting. We had to leave the meeting around 8:00 and didn't get the opportunity to ask you some questions. I'm just a bit confused and would appreciate your clarifying

Our house is on the inside of the curve, two doors to counter clockwise of the three houses sharing the border with your client.

I heard the term R-20 from yourself and one or two of the participants. I believe our current designation is R-30. Is that correct? If your client gets his parcel changed to R-10, will that impact our designation?

Thank you for your consideration.

Sincerely,

Patrick Lynch 301 S Bend Dr Knightdale NC



Subject: Re: Proposed Rezoning Meeting

Date: Tuesday, October 27, 2020 at 3:06:59 PM Eastern Daylight Time

From: Andrew Petesch <apetesch@peteschlaw.com>
To: Michael Passer <mbpasser13@gmail.com>

Michael.

Thank you for the follow-up. I will include your comments with the rezoning application updates later this week.

Sincerely, Andy

Andrew J. Petesch
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Raleigh, North Carolina 27601
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F: (888) 848-9605

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From: Michael Passer <mbpasser13@gmail.com>
Date: Tuesday, October 27, 2020 at 12:28 PM
To: Andrew Petesch apetesch@peteschlaw.com

Subject: Re: Proposed Rezoning Meeting

HI Andy.

I am totally opposed to HOA's in general, and that is why I purchased my home in the area that I did. I am also opposed to reducing the natural area because we do need to protect more of this area for the wildlife. This also helps provide more permeable areas for natural drainage.

I have concerns about tapping into the current water and sewage systems since these systems are already about forty years old and may become over stressed. Many systems throughout the county in this age range are breaking and causing serious damages.

Regards, Michael

On Wed, Oct 21, 2020 at 8:20 PM Andrew Petesch apetesch@peteschlaw.com wrote:

Michael,

Received. Thank you.

To clarify, are you saying you are opposed to HOA's in general and do not want one to be created that

would involve your property? Or do you have concerns about an HOA existing for this proposed new subdivision?

With kind regards, Andy

Andrew J. Petesch
Petesch Law
127 W. Hargett St., Suite 500
Raleigh, North Carolina 27601

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E: andy@peteschlaw.com

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From: Michael Passer < mbpasser13@gmail.com
Date: Wednesday, October 21, 2020 at 8:07 PM
To: Andrew Petesch < apetesch@peteschlaw.com

Subject: Proposed Rezoning Meeting

Hi Andy,

I was in the Meeting and I live at 102 Dwelling PL. I do disagree with HOA's.

Sincerely, Michael Passer

THE PLAYBOOK

Because the Town should be able to take advantage of opportunities when they present themselves, KnightdaleNext uses a 'playbook approach' to guiding future growth and development in the community.

Some parts of the document—things like the community vision, guiding principles, and *Growth Framework Map*—should remain constant and keep Knightdale on a focused path for success.

Other parts of the document—things like the general recommendations, focus area study recommendations, the *Growth and Conservation Map*, and other supporting infrastructure maps—may need to evolve over time as conditions change that were not contemplated at the time this document was adopted.

Any changes considered under the playbook mindset for the document should be evaluated against the community vision, guiding principles, and *Growth Framework Map* to determine if they are in the best long-term interests of the Town and its residents, businesses, and property owners.

Patience may be needed for some aspects of the plan to evolve, as it sets a long-term vision to guide growth over an extended period of time. Town officials should avoid 'short-sighted' decisions to modify the Plan as a playbook unless reasons to change it are supported by staff.



22 September 2019

Richard Stockett

Re: 40 Lots Adjacent to Rutledge Landing Tax Parcels 1763350850 and 1763007038 Wake County NC

Mr. Stockett:

As you know, Carolina Water Service of NC, Inc. (CWSNC) provides sanitary sewer utility service to the area adjacent to the above referenced property. CWSNC is a franchised and regulated public utility company in the State of North Carolina.

CWSNC hereby agrees to accommodate the sanitary sewer utility needs for the referenced property under the existing permit provided that a mutually agreed upon developer agreement is executed prior to construction. The peak design flows as presented must concur with Wastewater Design Flow Rates found within 15A NCAC 02T.0114. All standard connection or other fees apply and may change from time to time as approved by the NC Utilities Commission.

As a part of any proposed development, the developer is required to perform necessary water and/or sewer system improvements to meet the needs of the proposed development and insure that the existing customers' services are not affected by proposed development. Not only do these system improvements include internal ones to the development, but external ones also, including but not limited to expansion of current lift stations and wastewater treatment facilities. The developer is required to provide a set of drawings to allow the proposed system improvements to be evaluated by CWSNC. If any systems improvements are determined necessary, the developer is notified, and these improvements must be included in the proposed development plans and constructed. All revised construction designs shall be submitted to CWSNC for review and approval. The end result is that a willingness and capability letter may be issued, but any proposed development will not be approved until all requirements as detailed above are met.

As a result of the Tax Cuts and Jobs Act of 2017 (TCJA), the exemption for water and sewer property transferred to a public utility from current year taxation has been removed from the tax code. Contributions in Aid of Construction (CIAC), whether paid in cash or in the form of contributed property, are now immediately taxable to the recipient of these contributions. The Tax Multiplier to be used to increase CIAC based on the Act is **29.836%**. To calculate the Tax Multiplier for contributed property or cash, simply multiply the transferred amount by 0.29836. This figure assumes a 21% federal tax rate and a 2.5% North Carolina state rate.

Should you have any questions, please do not hesitate to contact me directly in our Charlotte Office at 704-319-0517 or via email bryce.mendenhall@carolinawaterservicenc.com.

Sincerely,

J Bryce Mendenhall VP of Operations

cc:

Martin Scanlon, Project Manager Dana Hill, Director of Operations

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February 27, 2020

Sean Brennan, PE
Senior Assistant District Engineer [NCDOT District 1]
4009 District Drive
Raleigh, NC 27607
P: 919.733.7759 E: spbrennan@ncdot.gov

Subject: **Traffic Assessment -** Poole Road Project Wake County, North Carolina

Dear Mr. Brennan:

This report provides a traffic assessment for the proposed Poole Road Residential Project to be located between Knotts Hill Place and South Bend Drive in Wake County, North Carolina. Refer to Figure 1 for the site location map. The proposed development is expected to consist of up to 40 detached single-family homes and is expected to be built-out by 2023. Access to Smithfield Road and Poole Road is proposed to be provided via cross-access with the Rutledge Landing Subdivision [Phases 3 and 4]. Refer to the attached site plan for reference. The purpose of this study is to evaluate the traffic conditions for the study intersections during the weekday AM and PM peak hours for the following scenarios:

- Existing (2020) Traffic Conditions
- Background (2023) Traffic Conditions
- Combined (2023) Traffic Conditions

It should be noted that due to the low number of single-family lots being proposed, the development is not expected to exceed the Wake County Unified Development Ordinance's threshold for triggering the need for a Traffic Impact Analysis (TIA) outlined in Section 15-2-2.

Existing Roadways

Based on coordination with Wake County (County), the study area is proposed to consist of the following intersections:

- Smithfield Road and Poole Road (signalized)
- Smithfield Road and Sandy Run (signalized)
- Smithfield Road and Meadow Run (unsignalized)
- Poole Road and Water Rock Way / Rutledge Landing Drive (unsignalized)



Existing lane configurations (number of traffic lanes on each intersection approach), lane widths, storage capacities, and other intersection and roadway information was obtained by Ramey Kemp & Associates, Inc. (RKA). Table 1, on the following page, provides a summary of the data collected. Refer to Figure 3 for an illustration of the existing lane configurations and traffic control within the study area.

Table 1: Existing Roadway Inventory

| Road Name | Route Number | Typical Cross Section | Speed Limit | Maintained By | 2017 ADT (vpd) |
|---------------------------|-----------------|-----------------------------|-------------|------------------|-------------------|
| Smithfield Road | SR 2233 | 2-lane undivided | 55 mph | NCDOT | 14,000 |
| Poole Road | SR 1007 | 2-lane undivided | 55 mph | NCDOT | 4,700 |
| Sandy Run | N/A | 2-lane undivided | 25 mph | Town | 710* |
| Meadow Run | N/A | 2-lane undivided | 25 mph | Town | 230* |
| Water Rock Way | N/A | 2-lane undivided | 25 mph | Town | 760* |
| Rutledge Landing Drive | N/A | 2-lane undivided | 25 mph | Town | 870* |

^{*}ADT based on the traffic counts from 2020 and assuming the weekday PM peak hour volume is 10% of the average daily traffic.

Existing (2020) Traffic Volumes

Existing peak hour traffic volumes were determined based on traffic counts conducted at the study intersections by RKA during the AM (7:00 AM – 9:00 AM) and PM (4:00 PM – 6:00 PM) peak periods on a typical weekday in January of 2020 while schools were in session. Traffic volumes were balanced where appropriate. Refer to Figure 4 for existing (2020) AM and PM peak hour traffic volumes. Refer to the attachments for the traffic count data.

Background (2023) Traffic Volumes

In order to account for growth of traffic and subsequent traffic conditions at a future year, background traffic projections are needed. Background traffic is the component of traffic due to



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the growth of the community and surrounding area that is anticipated to occur regardless of whether or not the proposed development is constructed. Background traffic is comprised of existing traffic growth within the study area and additional traffic created as a result of adjacent approved developments.

Through coordination with the County, it was determined that an annual growth rate of 3% would be used to generate projected (2023) AM and PM peak hour traffic volumes. Refer to Figure 5 for projected (2023) peak hour traffic. Additionally, Rutledge Landing [Phases 3 and 4] was included as an adjacent development.

Although a Traffic Impact Analysis (TIA) was completed for *Phases 3 and 4 of Rutledge Landing* by Kimley-Horn and Associates, Inc. on January 13, 2012 [and was approved on April 27, 2017], revisions to the trip distributions and assignments from the previously approved TIA were required due to access that is to be provided to Poole Road via an easement that was previously marked for emergency use only. The updated trip distributions were estimated based on existing traffic patterns, the 2020 traffic counts, and engineering judgment. Refer to the attachments for the previously approved adjacent development information. The updated adjacent development trips are shown in Figure 6.

The background (2023) traffic volumes were determined by adding the adjacent development trips to the projected (2023) peak hour traffic volumes. Refer to Figure 7 for an illustration of the background (2023) peak hour traffic volumes at the study intersections.

Trip Generation

The proposed development is expected to consist of up to 40 detached single-family homes. Average weekend peak hour trips for the proposed development were estimated using methodology contained within the ITE *Trip Generation Manual*, 10th Edition. Table 2 provides a summary of the trip generation potential for the site.

Table 2: Trip Generation Summary

| Land Use | Intensity | Weekday Daily | AM Peak Hour Trips (vph) | | PM Peak Hour Trips (vph) | |
|------------------------------------|--------------|------------------|-----------------------------|------|-----------------------------|------|
| (ITE Code) | | Traffic (vpd) | Enter | Exit | Enter | Exit |
| Detached Single-Family Homes (210) | 40 dwellings | 448 | 8 | 25 | 26 | 16 |



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It is estimated that the proposed development will generate 448 total site trips (in and out) on the roadway network during a typical 24-hour weekday. Of the daily traffic volumes, it is anticipated that 33 trips (8 entering and 25 exiting) will occur during the AM peak hour and 42 trips (26 entering and 16 exiting) will occur during the PM peak hour.

As mentioned previously, the low trip generation potential of the proposed development does not meet the County UDO's requirement of 1,000 [or more] vehicle trips generated during a 24-hour period or 100 [or more] vehicle trips generated during the peak hour outlined in Section 15-2-2.

Site Trip Distribution and Assignment

Trip distribution percentages used in assigning site traffic for this development were estimated based on existing traffic patterns, volumes, and engineering judgement. The trip distributions are summarized below:

- 60% to/from the north via Smithfield Road
- 20% to/from the south via Smithfield Road
- 15% to/from the east via Poole Road
- 5% to/from the west via Poole Road

Refer to Figures 8 and 9 for the site trip distribution and site trip assignment, respectively.

Combined (2023) Peak Hour Traffic

To estimate traffic conditions with the site fully built out, the site trip assignment (Figure 9) was added to the background (2023) traffic volumes (Figure 7) to determine the combined (2023) traffic volumes. Refer to Figure 10 for an illustration of the combined (2023) peak hour traffic volumes with the proposed site developed.

Capacity Analysis

Study intersections were analyzed using the methodology outlined in the *Highway Capacity Manual*, 6th Edition (HCM) published by the Transportation Research Board. Capacity and level of service are the design criteria for this traffic study. A computer software package, Synchro (Version 10.3), was used to complete the analyses for each of the study area intersections. Please note that the unsignalized capacity analysis does not provide an overall level of service for an intersection; only delay for an approach with a conflicting movement.

The HCM defines capacity as "the maximum hourly rate at which persons or vehicles can reasonably be expected to traverse a point or uniform section of a lane or roadway during a given





time period under prevailing roadway, traffic, and control conditions." Level of service (LOS) is a term used to represent different driving conditions and is defined as a "qualitative measure describing operational conditions within a traffic stream, and their perception by motorists and/or passengers." Level of service varies from Level "A" representing free flow, to Level "F" where breakdown conditions are evident. Refer to Table 3, on the next page, for HCM levels of service and related average control delay per vehicle for both signalized and unsignalized intersections. Control delay as defined by the HCM includes "initial deceleration delay, queue move-up time, stopped delay, and final acceleration delay". An average control delay of 50 seconds at a signalized intersection results in LOS "D" operation at the intersection.

Table 3: Highway Capacity Manual - Levels-of-Service and Delay

| UNSIGNAL | LIZED INTERSECTION | SIGNALIZED INTERSECTION | | | |
|---------------------|---|-------------------------|---|--|--|
| LEVEL OF SERVICE | AVERAGE CONTROL DELAY PER VEHICLE (SECONDS) | LEVEL OF SERVICE | AVERAGE CONTROL DELAY PER VEHICLE (SECONDS) | | |
| A | 0-10 | A | 0-10 | | |
| В | 10-15 | В | 10-20 | | |
| С | 15-25 | С | 20-35 | | |
| D | 25-35 | D | 35-55 | | |
| E | 35-50 | E | 55-80 | | |
| F | >50 | F | >80 | | |

Capacity analysis at all study intersections was completed according to the NCDOT Congestion Management Guidelines. Signal information was obtained from NCDOT and is included in the attachments. Signal information from the signal plans was utilized in all analysis scenarios. Please note that a minimum peak hour volume of 4 vehicles per hour [1 vehicle per each 15-minute period] was utilized for the purpose of this analysis.

Smithfield Road and Poole Road

The signalized intersection of Smithfield Road and Poole Road was analyzed under existing (2020), background (2023), and combined (2023) traffic conditions with the lane configurations and traffic control shown in Table 4. Refer to Table 4 for a summary of the capacity analysis results. The Synchro capacity analysis reports are included in the attachments.





Table 4: Analysis Summary of Smithfield Road and Poole Road

| ANALYSIS | A P P R | LANE | WEEKDAY AM PEAK HOUR LEVEL OF SERVICE | | WEEKDAY PM PEAK HOUR LEVEL OF SERVICE | |
|----------------------------|------------------|--------------------------|---------------------------------------|----------------------|---|----------------------|
| SCENARIO | O A C H | LANE CONFIGURATIONS | Approach | Overall (seconds) | Approach | Overall (seconds) |
| Existing | NB SB | 1 LT-TH-RT 1 LT-TH-RT | C A | С | B C | С |
| (2020) | EB | 1 LT-TH-RT | D | | D | |
| Conditions | WB | 1 LT-TH-RT | D | | D | |
| Background | NB | 1 LT-TH-RT | С | | В | |
| (2023) | SB | 1 LT-TH-RT | A | С | С | C |
| Conditions | EB | 1 LT-TH-RT | Е | C | E | |
| Conditions | WB | 1 LT-TH-RT | D | | D | |
| Combined (2023) Conditions | NB | 1 LT-TH-RT | D | | В | |
| | SB | 1 LT-TH-RT | A | C | С | C |
| | EB | 1 LT-TH-RT | E | | E | |
| Conditions | WB | 1 LT-TH-RT | D | | D | |

Capacity analysis of existing (2020), background (2023), and combined (2023) traffic conditions indicates that the intersection and each of the approaches are expected to operate at LOS D or better, with the exception of the eastbound approach [of Poole Road] during the AM and PM peak hours under background and combined conditions. Although the eastbound approach is expected to experience heavier delays during the AM and PM peak hours, the approach delay is not expected to increase by more than 0.5 seconds per vehicle with the additional traffic associated with the proposed residential development. While the LOS of the northbound approach [of Smithfield Road] is expected to degrade one (1) letter grade between background (2023) and combined (2023) conditions during the weekday AM peak hour (3.2% increase in overall delay), the approach is expected to operate at an acceptable level-of-service under combined (2023) conditions. Additionally, the site traffic associated with the proposed development is expected to account for less than 1% of the total weekday AM and PM peak hour traffic under combined (2023) conditions. Therefore, no improvements are recommended at this intersection.



Smithfield Road and Sandy Run

The signalized intersection of Smithfield Road and Sandy Run was analyzed under existing (2020), background (2023), and combined (2023) traffic conditions with the lane configurations and traffic control shown in Table 5. Refer to Table 5 for a summary of the capacity analysis results. The Synchro capacity analysis reports are included in the attachments.

Table 5: Analysis Summary of Smithfield Road and Sandy Run

| ANALYSIS | A P P R | LANE | WEEKDAY AM PEAK HOUR LEVEL OF SERVICE | | WEEKDAY PM PEAK HOUR LEVEL OF SERVICE | |
|----------------------------|------------------|-----------------------|---------------------------------------|---------|---|---------|
| SCENARIO | O A C H | CONFIGURATIONS | Approach | Overall | Approach | Overall |
| Evicting | NB | 1 LT-TH-RT | В | | A | В |
| Existing | SB | 1 LT-TH-RT | A | В | В | |
| (2020) Conditions | EB | 1 LT-TH-RT | D | | D | |
| Conditions | WB | 1 LT-TH-RT | D | | D | |
| D 1 1 | NB | 1 LT , 1 TH-RT | С | С | В | В |
| Background | SB | 1 LT , 1 TH-RT | A | | В | |
| (2023) Conditions | EB | 1 LT-TH-RT | F | | E | |
| Conditions | WB | 1 LT-TH-RT | E | | D | |
| Combined (2023) Conditions | NB | 1 LT, 1 TH-RT | С | | В | |
| | SB | 1 LT, 1 TH-RT | A | C | В | В |
| | EB | 1 LT-TH-RT | F | | E | D |
| | WB | 1 LT-TH-RT | D | | D | |

^{*}Bold denotes an improvement required as part of Rutledge Landing Phases 3 and 4 [see attachments].

Capacity analysis of existing (2020) traffic conditions indicates that the intersection and each of the approaches operate at LOS D or better during the AM and PM peak hours. With the construction of exclusive northbound and southbound left turns lanes on Smithfield Road [required as part of the Rutledge Landing development Phases 3 and 4], capacity analysis of background (2023) and combined (2023) traffic conditions indicates that the intersection and each of the approaches are expected to operate at LOS D or better, with the exception of the eastbound [AM and PM peak hours] and westbound [AM peak hour (background conditions only)] approaches. Although the eastbound and westbound approaches are expected to experience heavier delays during the AM and PM peak hours, the approach delays [of Sandy Run] are not



expected to increase by more than 3.0 seconds per vehicle with the additional traffic associated with the proposed residential development. Additionally, the site traffic associated with the proposed development is expected to account for less than 1.5% of the total weekday AM and PM peak hour traffic under combined (2023) conditions. Therefore, no improvements are recommended at this intersection.

Smithfield Road and Meadow Run

The unsignalized intersection of Smithfield Road and Meadow Run was analyzed under existing (2020), background (2023), and combined (2023) traffic conditions with the lane configurations and traffic control shown in Table 6. Refer to Table 6 for a summary of the capacity analysis results. The Synchro capacity analysis reports are included in the attachments.

Table 6: Analysis Summary of Smithfield Road and Meadow Run

| ANALYSIS | A P P R | LANE | WEEKDAY AM PEAK HOUR LEVEL OF SERVICE | | WEEKDAY PM PEAK HOUR LEVEL OF SERVICE | |
|----------------------------|------------------|--------------------------|---------------------------------------|---------|---|---------|
| SCENARIO | O A C H | CONFIGURATIONS | Approach | Overall | Approach | Overall |
| | NB | 1 LT-TH-RT | A ¹ | | B ¹ | |
| Existing | SB | 1 LT-TH-RT 1 LT-TH-RT | B1 | N/A | A^1 | N/A |
| (2020) Conditions | EB | 1 LT-TH-RT | E ² | | F2 | |
| | WB | 1 LT-TH-RT | E ² | | E ² | |
| D 1 1 | NB | 1 LT-TH-RT | A^1 | | B ¹ | |
| Background | SB | 1 LT-TH-RT | B^1 | NT / A | A^1 | N/A |
| (2023) | EB | 1 LT-TH-RT | F ² | N/A | F ² | |
| Conditions | WB | 1 LT-TH-RT | F ² | | F ² | |
| Combined (2023) Conditions | NB | 1 LT-TH-RT | A^1 | | B^1 | |
| | SB | 1 LT-TH-RT | B^1 | NI / A | A^1 | N/A |
| | EB | 1 LT-TH-RT | F ² | N/A | F ² | IN/ A |
| | WB | 1 LT-TH-RT | F ² | | F ² | |

- 1. Level of service for major-street left-turn movement.
- 2. Level of service for minor-street approach.

Capacity analysis of existing (2020), background (2023), and combined (2023) traffic conditions indicates that the major-street left-turn movements are expected to operate at LOS B or better



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during the weekday AM and PM peak hours. While the minor-street approaches are expected to see heavier delays during the peak hours, the overall approach delays [of Meadow Run] are not expected to increase by more than 5.5 seconds per vehicle with the additional traffic associated with the proposed residential development. Additionally, the site traffic associated with the proposed development is expected to account for less than 1.5% of the total weekday AM and PM peak hour traffic under combined (2023) conditions. Therefore, no improvements are recommended at this intersection.

Poole Road and Water Rock Way / Rutledge Landing Drive

The unsignalized intersection of Poole Road and Water Rock Way / Rutledge Landing Drive was analyzed under existing (2020), background (2023), and combined (2023) traffic conditions with the lane configurations and traffic control shown in Table 7. Refer to Table 7 for a summary of the capacity analysis results. The Synchro capacity analysis reports are included in the attachments.

Table 7: Analysis Summary of Poole Road and Water Rock Way / Rutledge Landing Drive

| | A P | | WEEKD PEAK | | WEEKD PEAK | |
|----------------------|--------|----------------|----------------|----------|----------------|----------|
| | P | | LEVEL OF | | LEVEL OF | |
| ANALYSIS | R | LANE | | | | |
| SCENARIO | O A | CONFIGURATIONS | Ammuoodh | Orvowall | Ammuoodh | Orvowall |
| | C | | Approach | Overall | Approach | Overall |
| | Н | | | | | |
| Existing | EB | 1 LT, 1 TH-RT | A^1 | | A^1 | |
| (2020) | WB | 1 LT, 1 TH-RT | A^1 | N/A | A^1 | NI / A |
| Conditions | NB | 1 LT-TH-RT | B ² | IN/A | B ² | N/A |
| Conditions | SB | 1 LT-TH-RT | B ² | | B ² | |
| Rackground | EB | 1 LT, 1 TH-RT | A^1 | | A^1 | |
| Background | WB | 1 LT, 1 TH-RT | A^1 | N/A | A^1 | NT / A |
| (2023) Conditions | NB | 1 LT-TH-RT | B ² | IN/A | B ² | N/A |
| Conditions | SB | 1 LT-TH-RT | B ² | | B ² | |
| Combined | EB | 1 LT, 1 TH-RT | A^1 | | A^1 | |
| | WB | 1 LT, 1 TH-RT | A^1 | NT / A | A^1 | NT / A |
| (2023) | NB | 1 LT-TH-RT | B ² | N/A | B ² | N/A |
| Conditions | SB | 1 LT-TH-RT | B ² | | B ² | |

- 1. Level of service for major-street left-turn movement.
- Level of service for minor-street approach.



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Capacity analysis of existing (2020), background (2023), and combined (2023) traffic conditions indicates that the major-street left-turn movements and minor-street approaches at this intersection are expected to operate at LOS B or better during the weekday AM and PM peak hours. Therefore, no improvements are recommended at this intersection.

Findings and Summary

As mentioned previously, the proposed development is estimated to generate 448 total site trips (in and out) on the roadway network during a typical 24-hour weekday with 33 trips (8 entering and 25 exiting) generated during the AM peak hour and 42 trips (26 entering and 16 exiting) generated during the PM peak hour. Based on the Wake County UDO's TIA threshold of vehicle trips generated (1,000 per day or 100 per peak hour) outline in Section 15-2-2, the requirements are not met for a formal TIA to be submitted.

Based on the findings of this study, the traffic associated with the proposed development is expected to have minimal impact on the study intersections. The site traffic associated with the proposed development is expected to account for less than 2.5% of the total weekday AM and PM peak hour traffic at any of the study intersections under combined (2023) conditions.

If you should have any questions, please feel free to contact me at (919) 872-5115.

Sincerely,

Chase Smith, P.E.

Ramey Kemp & Associates, Inc.

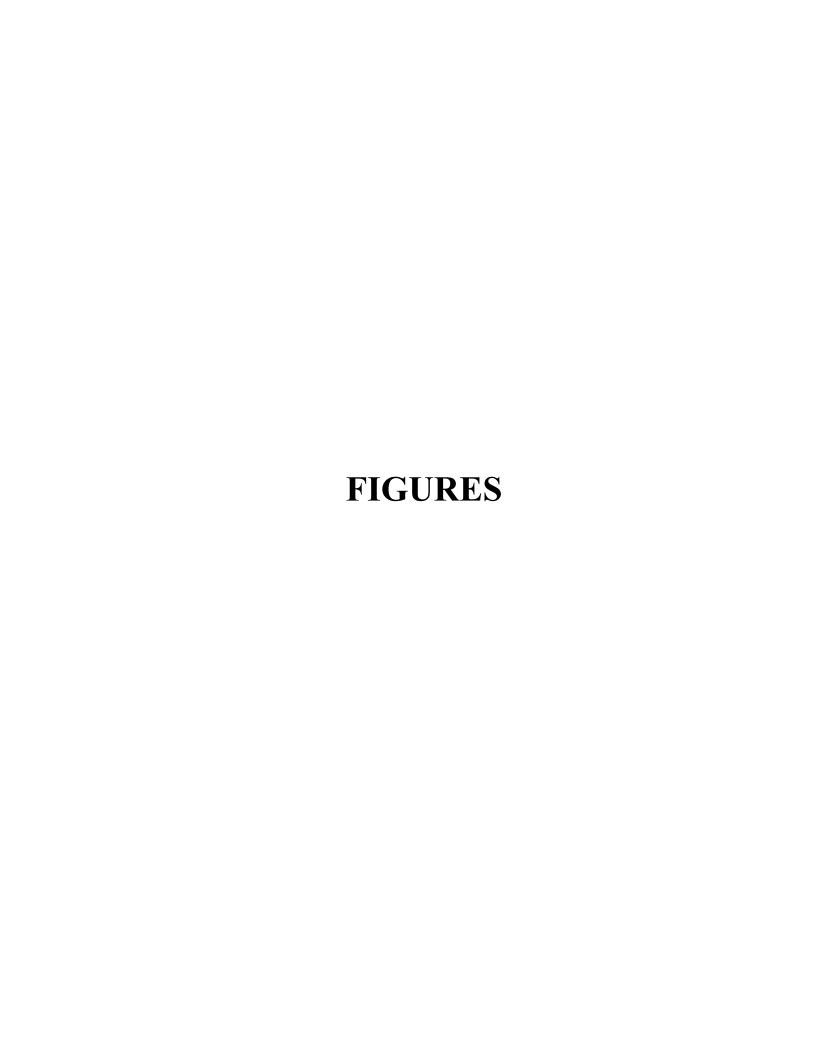
NC Corporate License # C-0910

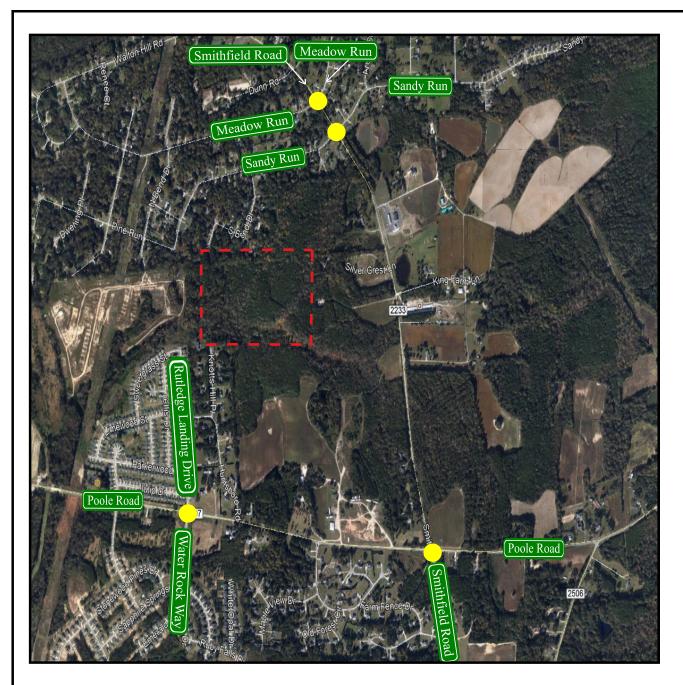
Cc: Keith Lankford, Wake County

Attachments



APPENDIX









Proposed Site Location



Study Intersection



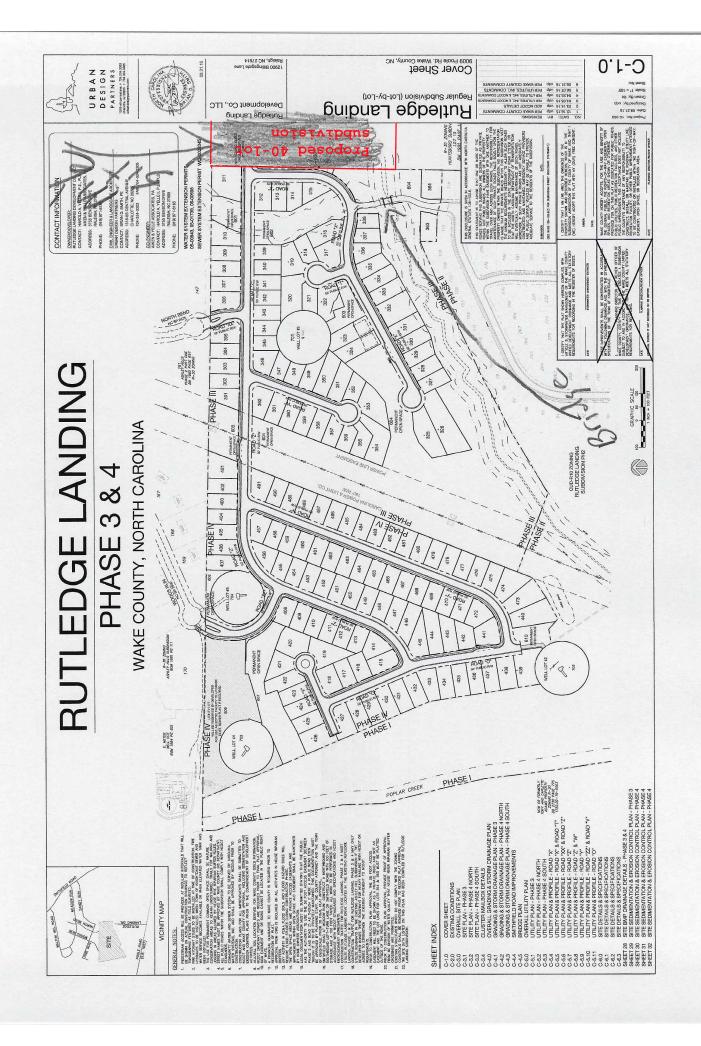


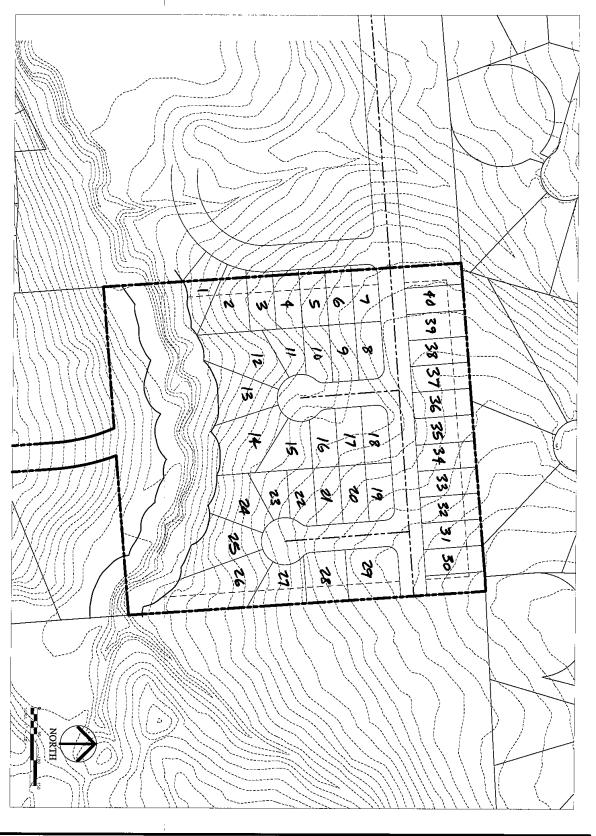
Poole Road Project Wake County, NC

Site Location Map

Scale: Not to Scale

Figure 1



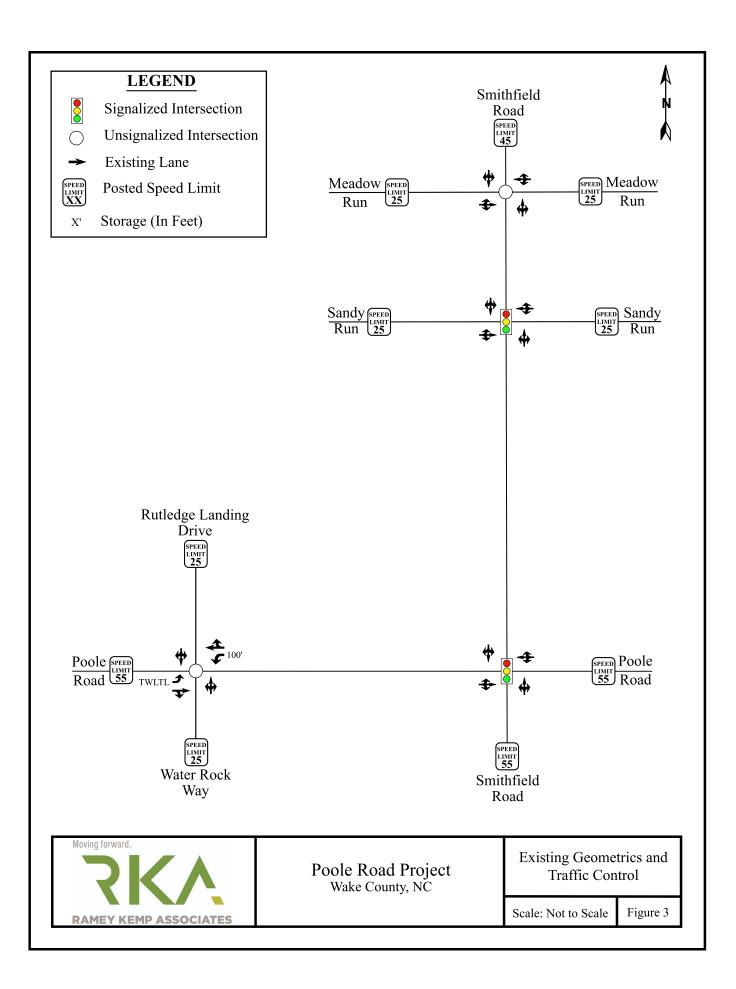


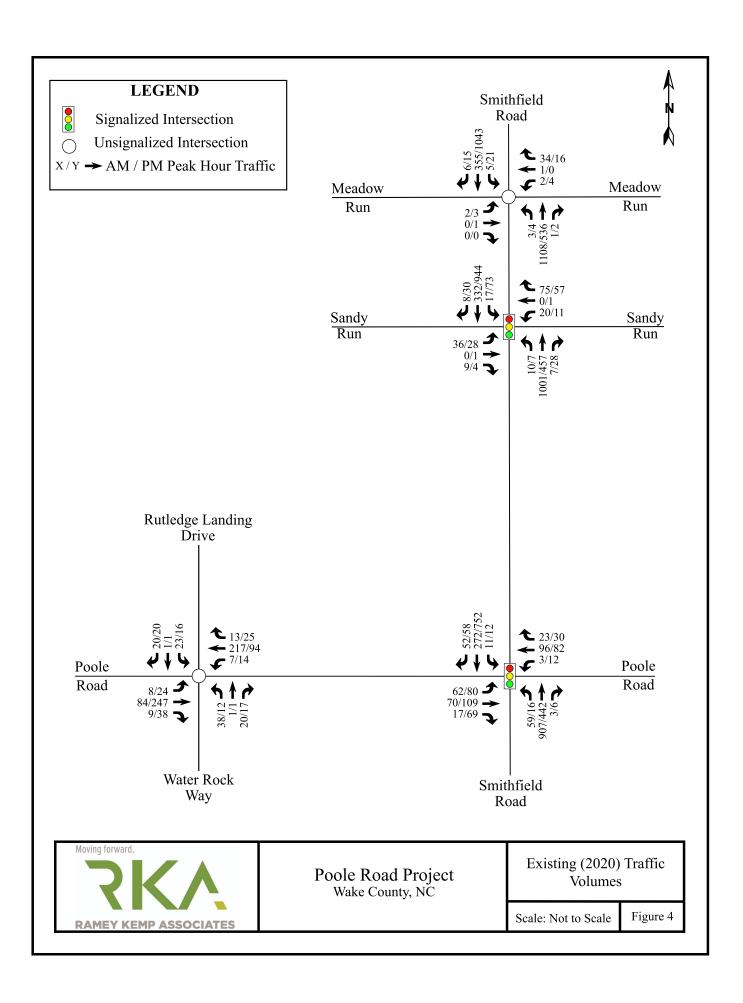
REVISIONS:

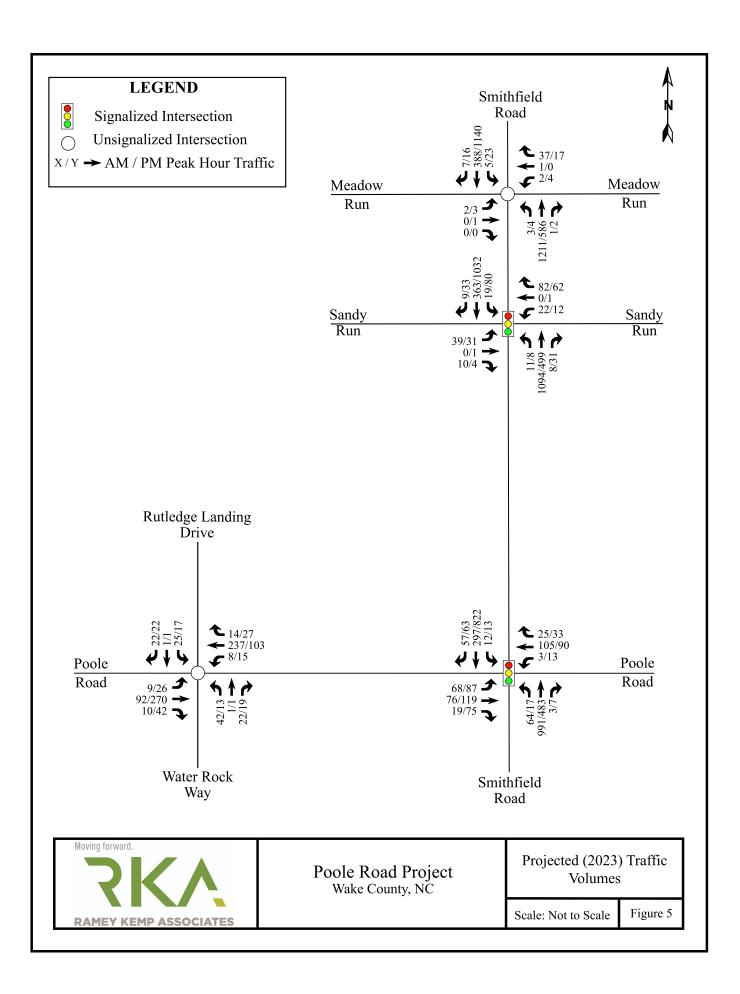
SUBDIVISION

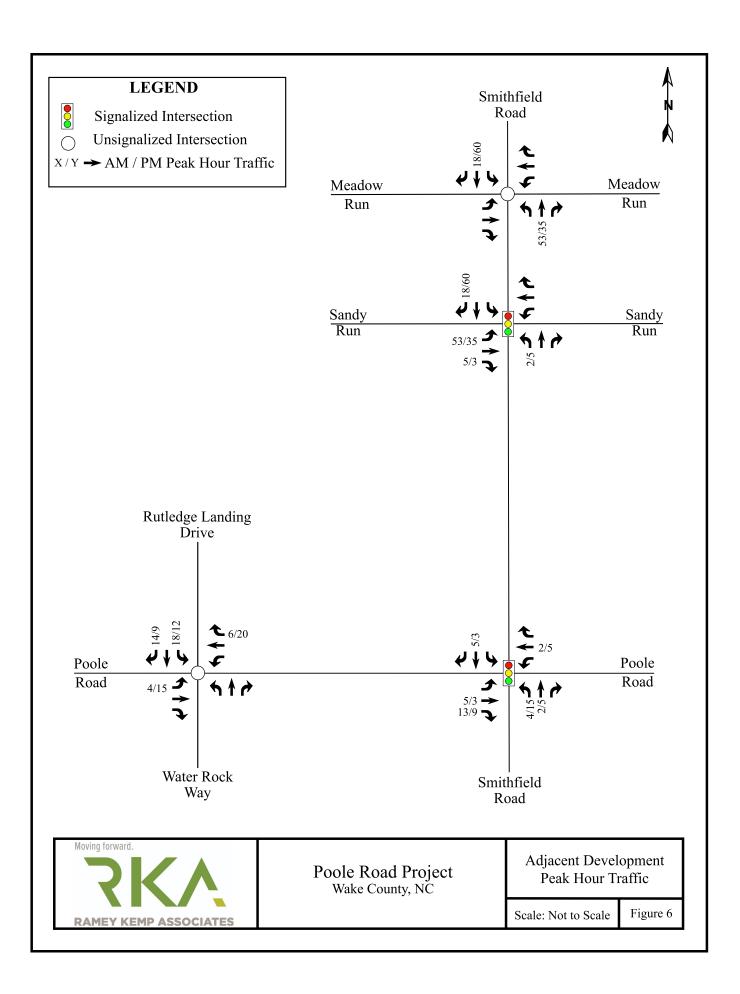
KNOTT'S HILL PLACE WENDELL, NORTH CAROLINA

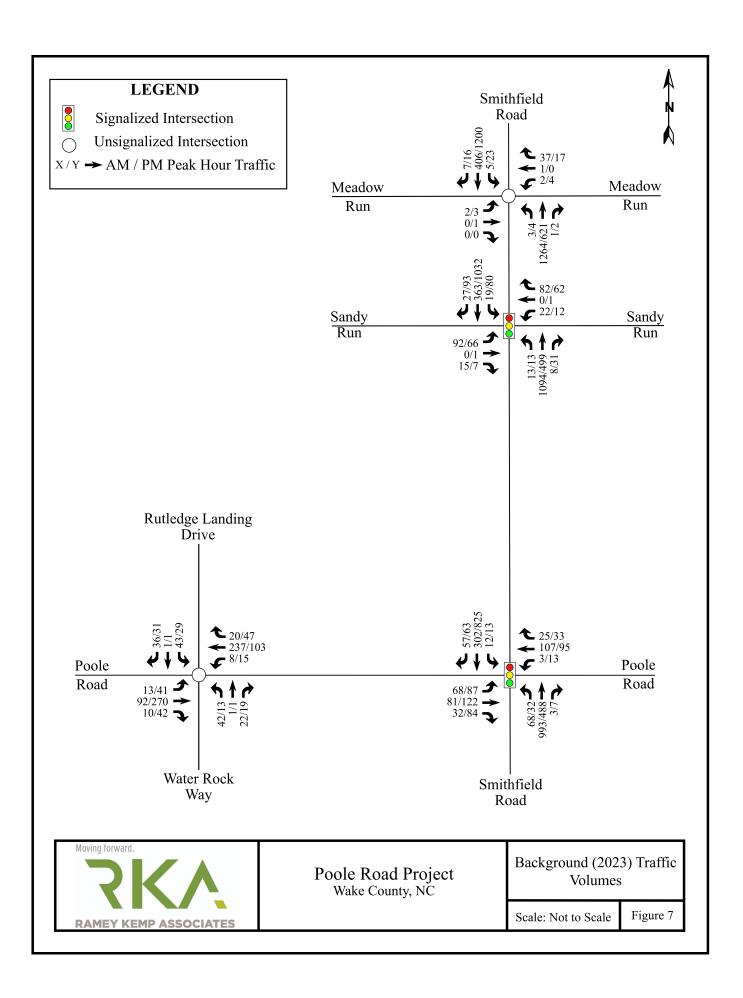


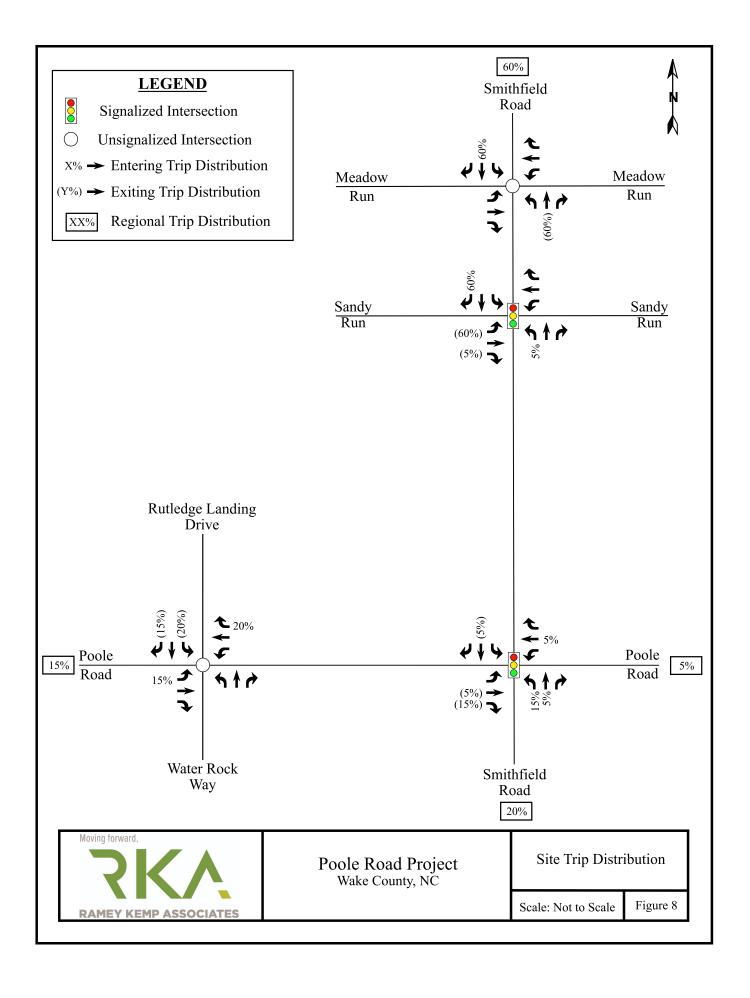


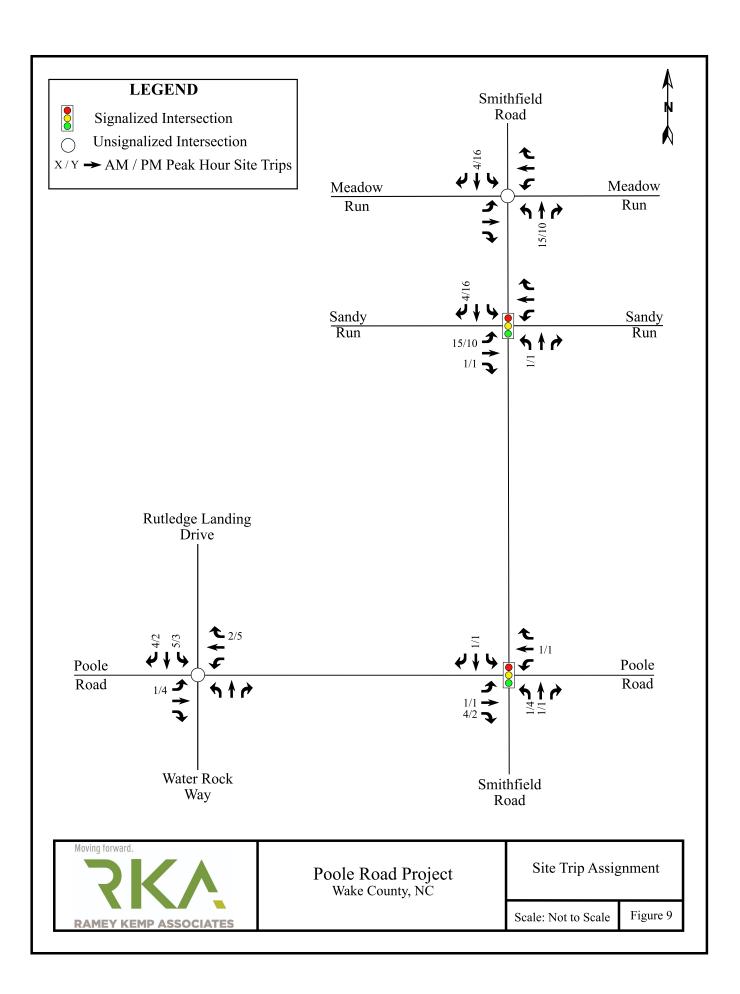


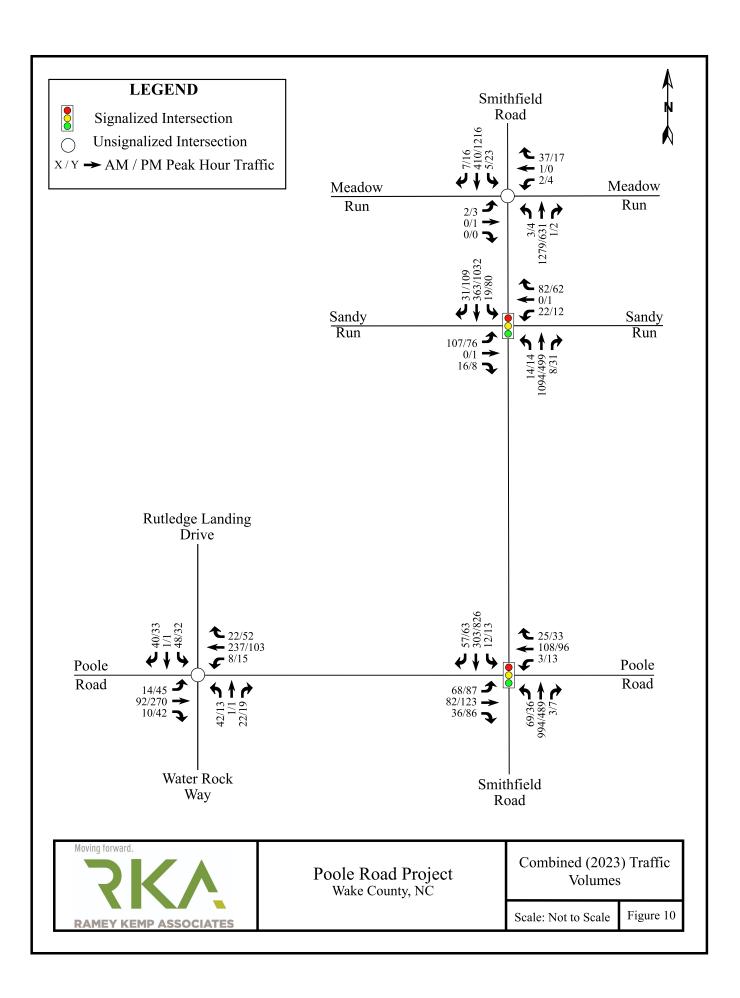


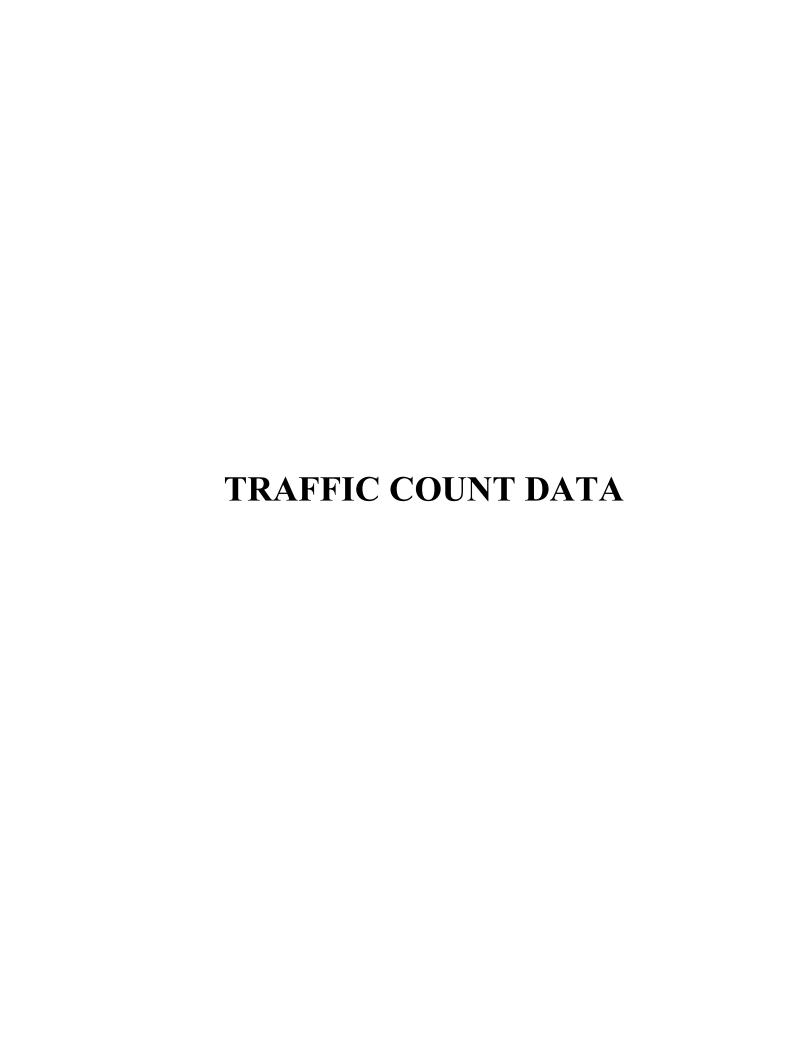














File Name: Knightdale(Smithfield and Poole)AM Peak

Site Code:

Start Date : 1/9/2020

Page No : 1

| | | | | | | | | Gro | ups Pi | rinted- (| Cars + | - Truc | ks | | | | | | | | |
|-------------|-------|------|--------|------|------------|-------|------|--------|--------|------------|--------|--------|---------|------|------------|-------|------|--------|------|------------|------------|
| | | Smit | hfield | Road | | | Po | oole R | oad | | | Smi | thfield | Road | | | Po | oole R | oad | | |
| | | Sc | uthbo | und | | | W | estbo | und | | | No | orthbo | und | | | E | astbou | und | | |
| Start Time | Right | Thru | Left | UTrn | App. Total | Right | Thru | Left | UTrn | App. Total | Right | Thru | Left | UTrn | App. Total | Right | Thru | Left | UTrn | App. Total | Int. Total |
| 07:00 AM | 16 | 71 | 3 | 0 | 90 | 0 | 23 | 0 | 0 | 23 | 0 | 229 | 22 | 0 | 251 | 3 | 15 | 18 | 0 | 36 | 400 |
| 07:15 AM | 17 | 65 | 3 | 0 | 85 | 9 | 24 | 1 | 0 | 34 | 2 | 211 | 14 | 0 | 227 | 5 | 21 | 17 | 0 | 43 | 389 |
| 07:30 AM | 8 | 79 | 4 | 0 | 91 | 5 | 23 | 0 | 0 | 28 | 1 | 250 | 11 | 0 | 262 | 3 | 17 | 13 | 0 | 33 | 414 |
| 07:45 AM | 11 | 57_ | 1_ | 0 | 69 | 9 | 26 | 2 | 0 | 37 | 0 | 217 | 12 | 0 | 229 | 6 | 17 | 14 | 0 | 37 | 372 |
| Total | 52 | 272 | 11 | 0 | 335 | 23 | 96 | 3 | 0 | 122 | 3 | 907 | 59 | 0 | 969 | 17 | 70 | 62 | 0 | 149 | 1575 |
| | | | | | | | | | | | | | | | | | | | | | |
| 08:00 AM | 9 | 69 | 7 | 0 | 85 | 6 | 20 | 1 | 0 | 27 | 2 | 205 | 11 | 0 | 218 | 0 | 15 | 7 | 0 | 22 | 352 |
| 08:15 AM | 9 | 57 | 3 | 0 | 69 | 9 | 16 | 1 | 0 | 26 | 0 | 229 | 8 | 0 | 237 | 4 | 11 | 5 | 0 | 20 | 352 |
| 08:30 AM | 11 | 82 | 2 | 0 | 95 | 4 | 20 | 0 | 0 | 24 | 0 | 254 | 8 | 0 | 262 | 5 | 11 | 11 | 0 | 27 | 408 |
| 08:45 AM | 10 | 73 | 2 | 0 | 85 | 8 | 18 | 1 | 0 | 27 | 0 | 174 | 5 | 0 | 179 | 2 | 10 | 12 | 0 | 24 | 315 |
| Total | 39 | 281 | 14 | 0 | 334 | 27 | 74 | 3 | 0 | 104 | 2 | 862 | 32 | 0 | 896 | 11 | 47 | 35 | 0 | 93 | 1427 |
| | | | | | | | | | | | | | | | | | | | | | |
| Grand Total | 91 | 553 | 25 | 0 | 669 | 50 | 170 | 6 | 0 | 226 | 5 | 1769 | 91 | 0 | 1865 | 28 | 117 | 97 | 0 | 242 | 3002 |
| Apprch % | 13.6 | 82.7 | 3.7 | 0 | | 22.1 | 75.2 | 2.7 | 0 | | 0.3 | 94.9 | 4.9 | 0 | | 11.6 | 48.3 | 40.1 | 0 | | |
| Total % | 3 | 18.4 | 0.8 | 0 | 22.3 | 1.7 | 5.7 | 0.2 | 0 | 7.5 | 0.2 | 58.9 | 3 | 0 | 62.1 | 0.9 | 3.9 | 3.2 | 0 | 8.1 | |
| Cars + | 90 | 526 | 25 | 0 | 641 | 49 | 167 | 6 | 0 | 222 | 5 | 1744 | 91 | 0 | 1840 | 28 | 114 | 94 | 0 | 236 | 2939 |
| % Cars + | 98.9 | 95.1 | 100 | 0 | 95.8 | 98 | 98.2 | 100 | 0 | 98.2 | 100 | 98.6 | 100 | 0 | 98.7 | 100 | 97.4 | 96.9 | 0 | 97.5 | 97.9 |
| Trucks | 1 | 27 | 0 | 0 | 28 | 1 | 3 | 0 | 0 | 4 | 0 | 25 | 0 | 0 | 25 | 0 | 3 | 3 | 0 | 6 | 63 |
| % Trucks | 11 | 49 | 0 | 0 | 42 | 2 | 18 | 0 | 0 | 1.8 | 0 | 14 | 0 | 0 | 1.3 | 0 | 26 | 3 1 | 0 | 2.5 | 21 |

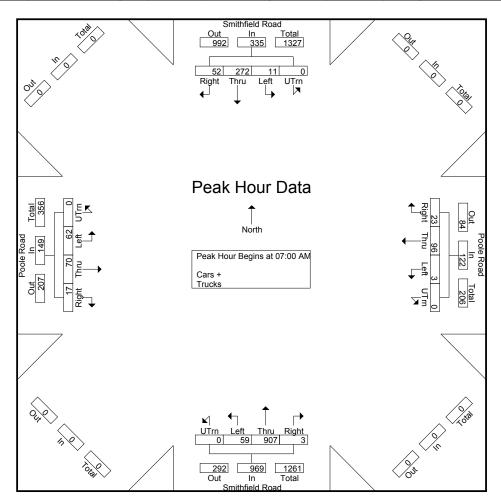


File Name: Knightdale(Smithfield and Poole)AM Peak

Site Code:

Start Date : 1/9/2020

| | | | hfield | | | | | ole R | | | | | | Road | | | | oole R | | |] |
|--------------|---------|---------|--------------|--------|------------|--------|--------|-------|------|------------|-------|------|---------------|------|------------|-------|------|---------------|------|------------|------------|
| | | Sc | <u>uthbo</u> | und | | | W | estbo | und | | | N | <u>orthbo</u> | und | | | E | <u>astbou</u> | und | | <u> </u> |
| Start Time | Right | Thru | Left | UTrn | App. Total | Right | Thru | Left | UTrn | App. Total | Right | Thru | Left | UTrn | App. Total | Right | Thru | Left | UTrn | App. Total | Int. Total |
| Peak Hour A | nalysi | s From | n 07:00 | 0 AM t | o 08:45 | AM - | Peak 1 | of 1 | | | | | | | | | | | | | |
| Peak Hour fo | or Enti | re Inte | rsection | n Beg | ins at 0 | 7:00 A | M | | | | | | | | | | | | | | |
| 07:00 AM | 16 | 71 | 3 | 0 | 90 | 0 | 23 | 0 | 0 | 23 | 0 | 229 | 22 | 0 | 251 | 3 | 15 | 18 | 0 | 36 | 400 |
| 07:15 AM | 17 | 65 | 3 | 0 | 85 | 9 | 24 | 1 | 0 | 34 | 2 | 211 | 14 | 0 | 227 | 5 | 21 | 17 | 0 | 43 | 389 |
| 07:30 AM | 8 | 79 | 4 | 0 | 91 | 5 | 23 | 0 | 0 | 28 | 1 | 250 | 11 | 0 | 262 | 3 | 17 | 13 | 0 | 33 | 414 |
| 07:45 AM | 11 | 57 | 1 | 0 | 69 | 9 | 26 | 2 | 0 | 37 | 0 | 217 | 12 | 0 | 229 | 6 | 17 | 14 | 0 | 37 | 372 |
| Total Volume | 52 | 272 | 11 | 0 | 335 | 23 | 96 | 3 | 0 | 122 | 3 | 907 | 59 | 0 | 969 | 17 | 70 | 62 | 0 | 149 | 1575 |
| % App. Total | 15.5 | 81.2 | 3.3 | 0 | | 18.9 | 78.7 | 2.5 | 0 | | 0.3 | 93.6 | 6.1 | 0 | | 11.4 | 47 | 41.6 | 0 | | |
| PHF | .765 | .861 | .688 | .000 | .920 | .639 | .923 | .375 | .000 | .824 | .375 | .907 | .670 | .000 | .925 | .708 | .833 | .861 | .000 | .866 | .951 |





File Name: Knightdale(Smithfield and Poole)PM Peak

Site Code:

Start Date : 1/9/2020

Page No : 1

| | | | | | | G | roups F | <u> Printed- C</u> | ars + - | Trucks | | | | | | | |
|-------------|-------|----------|--------|------------|-------|-------|---------|--------------------|---------|----------|----------|------------|-------|-------|-------|------------|------------|
| | | Smithfie | ld Roa | ıd | | Poole | Road | | | Smithfie | eld Road | d | | Poole | Road | | |
| | | South | bound | | | West | bound | | | North | bound | | | East | bound | | |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| 04:00 PM | 13 | 193 | 8 | 214 | 10 | 22 | 2 | 34 | 2 | 97 | 1 | 100 | 15 | 19 | 16 | 50 | 398 |
| 04:15 PM | 10 | 199 | 4 | 213 | 8 | 16 | 0 | 24 | 2 | 98 | 1 | 101 | 8 | 19 | 15 | 42 | 380 |
| 04:30 PM | 8 | 226 | 4 | 238 | 7 | 12 | 0 | 19 | 1 | 91 | 2 | 94 | 12 | 20 | 11 | 43 | 394 |
| 04:45 PM | 13 | 195 | 3 | 211 | 8 | 22 | 4 | 34 | 1 | 106 | 4 | 111 | 8 | 25 | 24 | 57 | 413 |
| Total | 44 | 813 | 19 | 876 | 33 | 72 | 6 | 111 | 6 | 392 | 8 | 406 | 43 | 83 | 66 | 192 | 1585 |
| | | | | | | | | | | | | | | | | | |
| 05:00 PM | 15 | 186 | 3 | 204 | 5 | 18 | 2 | 25 | 0 | 99 | 2 | 101 | 19 | 39 | 18 | 76 | 406 |
| 05:15 PM | 21 | 185 | 1 | 207 | 8 | 26 | 4 | 38 | 3 | 130 | 6 | 139 | 22 | 27 | 14 | 63 | 447 |
| 05:30 PM | 9 | 186 | 5 | 200 | 9 | 16 | 2 | 27 | 2 | 107 | 4 | 113 | 20 | 18 | 24 | 62 | 402 |
| 05:45 PM | 8 | 173 | 5 | 186 | 6 | 19 | 4 | 29 | 0 | 121 | 6 | 127 | 13 | 33 | 11 | 57 | 399 |
| Total | 53 | 730 | 14 | 797 | 28 | 79 | 12 | 119 | 5 | 457 | 18 | 480 | 74 | 117 | 67 | 258 | 1654 |
| | | | | | | | | | | | | | i. | | | | i. |
| Grand Total | 97 | 1543 | 33 | 1673 | 61 | 151 | 18 | 230 | 11 | 849 | 26 | 886 | 117 | 200 | 133 | 450 | 3239 |
| Apprch % | 5.8 | 92.2 | 2 | | 26.5 | 65.7 | 7.8 | | 1.2 | 95.8 | 2.9 | | 26 | 44.4 | 29.6 | | |
| Total % | 3_ | 47.6 | 1_ | 51.7 | 1.9 | 4.7 | 0.6 | 7.1 | 0.3 | 26.2 | 0.8 | 27.4 | 3.6 | 6.2 | 4.1 | 13.9 | |
| Cars + | 96 | 1520 | 33 | 1649 | 60 | 145 | 18 | 223 | 11 | 824 | 25 | 860 | 117 | 193 | 132 | 442 | 3174 |
| % Cars + | 99 | 98.5 | 100 | 98.6 | 98.4 | 96 | 100 | 97 | 100 | 97.1 | 96.2 | 97.1 | 100 | 96.5 | 99.2 | 98.2 | 98 |
| Trucks | 1 | 23 | 0 | 24 | 1 | 6 | 0 | 7 | 0 | 25 | 1 | 26 | 0 | 7 | 1 | 8 | 65 |
| % Trucks | 1 | 1.5 | 0 | 1.4 | 1.6 | 4 | 0 | 3 | 0 | 2.9 | 3.8 | 2.9 | 0 | 3.5 | 0.8 | 1.8 | 2 |

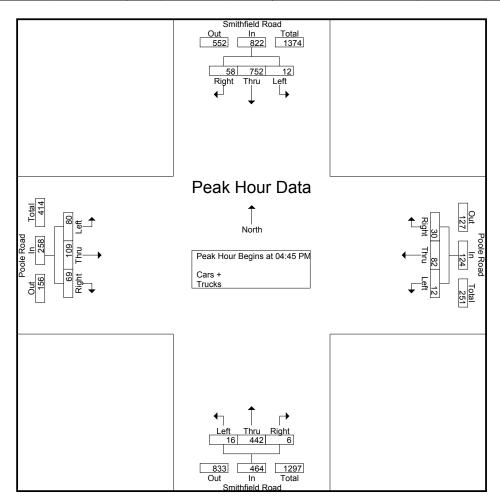


File Name: Knightdale(Smithfield and Poole)PM Peak

Site Code:

Start Date : 1/9/2020

| | ; | Smithfie | ld Roa | ıd | | Poole | Road | | | Smithfie | eld Roa | d | | Poole | Road | |] |
|-----------------|------------|----------|--------|------------|---------|-----------|-------|------------|-------|----------|---------|------------|-------|-------|-------|------------|------------|
| | | South | bound | | | Westl | oound | | | North | bound | | | East | bound | | |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| Peak Hour Ana | alysis Fro | om 04:0 | 0 PM t | o 05:45 F | M - Pea | ak 1 of 1 | | | _ | | | | _ | | | | |
| Peak Hour for I | Entire In | tersecti | on Beg | ins at 04 | 45 PM | | | | | | | | | | | | |
| 04:45 PM | 13 | 195 | 3 | 211 | 8 | 22 | 4 | 34 | 1 | 106 | 4 | 111 | 8 | 25 | 24 | 57 | 413 |
| 05:00 PM | 15 | 186 | 3 | 204 | 5 | 18 | 2 | 25 | 0 | 99 | 2 | 101 | 19 | 39 | 18 | 76 | 406 |
| 05:15 PM | 21 | 185 | 1 | 207 | 8 | 26 | 4 | 38 | 3 | 130 | 6 | 139 | 22 | 27 | 14 | 63 | 447 |
| 05:30 PM | 9 | 186 | 5 | 200 | 9 | 16 | 2 | 27 | 2 | 107 | 4 | 113 | 20 | 18 | 24 | 62 | 402 |
| Total Volume | 58 | 752 | 12 | 822 | 30 | 82 | 12 | 124 | 6 | 442 | 16 | 464 | 69 | 109 | 80 | 258 | 1668 |
| % App. Total | 7.1 | 91.5 | 1.5 | | 24.2 | 66.1 | 9.7 | | 1.3 | 95.3 | 3.4 | | 26.7 | 42.2 | 31 | | |
| PHF | .690 | .964 | .600 | .974 | .833 | .788 | .750 | .816 | .500 | .850 | .667 | .835 | .784 | .699 | .833 | .849 | .933 |





File Name: Knightdale(Smithfield and Sandy Run)AM Peak

Site Code:

Start Date : 1/9/2020

Page No : 1

| | | | | | | G | roups I | <u> Printed-C</u> | ars + - | Trucks | | | | | | | , |
|--------------------|-------|----------|---------|------------|-------|------|---------|-------------------|---------|----------|---------|------------|-------|------|--------|------------|------------|
| | | Smithfie | eld Roa | ıd | | Sand | ly Run | | | Smithfie | eld Roa | ıd | | Sand | ly Run | | |
| | | South | bound | | | West | bound | | | North | bound | | | East | bound | | |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| 07:00 AM | 1 | 80 | 3 | 84 | 24 | 0 | 4 | 28 | 2 | 245 | 4 | 251 | 4 | 0 | 12 | 16 | 379 |
| 07:15 AM | 2 | 78 | 1 | 81 | 19 | 0 | 7 | 26 | 3 | 248 | 1 | 252 | 1 | 0 | 7 | 8 | 367 |
| 07:30 AM | 1 | 93 | 9 | 103 | 18 | 0 | 4 | 22 | 2 | 260 | 3 | 265 | 3 | 0 | 9 | 12 | 402 |
| 07:45 AM | 4 | 81 | 4 | 89 | 14 | 0 | 5 | 19 | 0 | 248 | 2 | 250 | 1 | 0 | 8 | 9 | 367 |
| Total | 8 | 332 | 17 | 357 | 75 | 0 | 20 | 95 | 7 | 1001 | 10 | 1018 | 9 | 0 | 36 | 45 | 1515 |
| | | | | | | | | | | | | | | | | | |
| 08:00 AM | 3 | 60 | 4 | 67 | 14 | 0 | 7 | 21 | 2 | 219 | 2 | 223 | 3 | 0 | 11 | 14 | 325 |
| 08:15 AM | 5 | 80 | 7 | 92 | 17 | 0 | 1 | 18 | 1 | 243 | 3 | 247 | 5 | 0 | 9 | 14 | 371 |
| 08:30 AM | 3 | 79 | 3 | 85 | 15 | 1 | 5 | 21 | 5 | 250 | 2 | 257 | 2 | 3 | 5 | 10 | 373 |
| 08:45 AM | 2 | 80 | 2 | 84 | 18 | 0 | 7 | 25 | 3 | 205 | 5 | 213 | 1 | 0 | 6 | 7 | 329 |
| Total | 13 | 299 | 16 | 328 | 64 | 1 | 20 | 85 | 11 | 917 | 12 | 940 | 11 | 3 | 31 | 45 | 1398 |
| | | | | | | | | | | | | | | | | | |
| Grand Total | 21 | 631 | 33 | 685 | 139 | 1 | 40 | 180 | 18 | 1918 | 22 | 1958 | 20 | 3 | 67 | 90 | 2913 |
| Apprch % | 3.1 | 92.1 | 4.8 | | 77.2 | 0.6 | 22.2 | | 0.9 | 98 | 1.1 | | 22.2 | 3.3 | 74.4 | | |
| Total % | 0.7 | 21.7 | 1.1 | 23.5 | 4.8 | 0 | 1.4 | 6.2 | 0.6 | 65.8 | 0.8 | 67.2 | 0.7 | 0.1 | 2.3 | 3.1 | |
| Cars + | 21 | 606 | 33 | 660 | 139 | 1 | 40 | 180 | 18 | 1897 | 22 | 1937 | 20 | 3 | 67 | 90 | 2867 |
| <u> % Cars +</u> | 100 | 96 | 100 | 96.4 | 100 | 100 | 100 | 100 | 100 | 98.9 | 100 | 98.9 | 100 | 100 | 100 | 100 | 98.4 |
| Trucks | 0 | 25 | 0 | 25 | 0 | 0 | 0 | 0 | 0 | 21 | 0 | 21 | 0 | 0 | 0 | 0 | 46 |
| % Trucks | 0 | 4 | 0 | 3.6 | 0 | 0 | 0 | 0 | 0 | 1.1 | 0 | 1.1 | 0 | 0 | 0 | 0 | 1.6 |

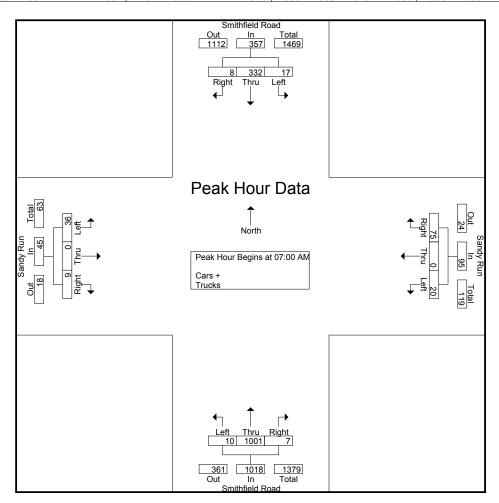


File Name: Knightdale(Smithfield and Sandy Run)AM Peak

Site Code:

Start Date : 1/9/2020

| | , | Smithfie | ld Roa | ıd | | Sand | y Run | | | Smithfie | eld Roa | d | | Sano | ly Run | | |
|-----------------|------------|----------|--------|------------|---------|-----------|-------|------------|-------|----------|---------|------------|-------|------|--------|------------|------------|
| | | South | bound | | | Westl | oound | | | North | bound | | | East | bound | | |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| Peak Hour Ana | alysis Fro | om 07:0 | 0 AM t | o 08:45 A | AM - Pe | ak 1 of 1 | | | | | | | | | | | |
| Peak Hour for I | Entire In | tersecti | on Beg | ins at 07 | :00 AM | | | | | | | | | | | | |
| 07:00 AM | 1 | 80 | 3 | 84 | 24 | 0 | 4 | 28 | 2 | 245 | 4 | 251 | 4 | 0 | 12 | 16 | 379 |
| 07:15 AM | 2 | 78 | 1 | 81 | 19 | 0 | 7 | 26 | 3 | 248 | 1 | 252 | 1 | 0 | 7 | 8 | 367 |
| 07:30 AM | 1 | 93 | 9 | 103 | 18 | 0 | 4 | 22 | 2 | 260 | 3 | 265 | 3 | 0 | 9 | 12 | 402 |
| 07:45 AM | 4 | 81 | 4 | 89 | 14 | 0 | 5 | 19 | 0 | 248 | 2 | 250 | 1 | 0 | 8 | 9 | 367 |
| Total Volume | 8 | 332 | 17 | 357 | 75 | 0 | 20 | 95 | 7 | 1001 | 10 | 1018 | 9 | 0 | 36 | 45 | 1515 |
| % App. Total | 2.2 | 93 | 4.8 | | 78.9 | 0 | 21.1 | | 0.7 | 98.3 | 1 | | 20 | 0 | 80 | | |
| PHF | .500 | .892 | .472 | .867 | .781 | .000 | .714 | .848 | .583 | .963 | .625 | .960 | .563 | .000 | .750 | .703 | .942 |





File Name: Knightdale(Smithfield and Sandy Run)PM Peak

Site Code:

Start Date : 1/9/2020

Page No : 1

| | | | | | | | | Gro | oups P | <u>rinted- (</u> | Cars + | - Truc | ks | | | | | | | | _ |
|-------------|-------|------|--------|------|------------|-------|------|--------|--------|------------------|--------|--------|---------|------|------------|-------|------|--------|------|------------|------------|
| | | Smit | hfield | Road | | | S | andy F | Run | | | Smi | thfield | Road | | | S | andy F | Run | | |
| | | Sc | uthbo | und | | | W | estbo | und | | | N | orthbo | und | | | E | astbou | und | | |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| 04:00 PM | 7 | 211 | 15 | 0 | 233 | 14 | 0 | 2 | 0 | 16 | 6 | 112 | 2 | 2 | 122 | 1 | 0 | 6 | 0 | 7 | 378 |
| 04:15 PM | 8 | 229 | 23 | 1 | 261 | 13 | 0 | 3 | 0 | 16 | 9 | 109 | 2 | 2 | 122 | 0 | 0 | 5 | 0 | 5 | 404 |
| 04:30 PM | 3 | 268 | 17 | 0 | 288 | 15 | 1 | 3 | 0 | 19 | 5 | 102 | 1 | 0 | 108 | 3 | 1 | 7 | 0 | 11 | 426 |
| 04:45 PM | 12 | 228 | 18 | 0 | 258 | 15 | 0 | 3 | 0 | 18 | 8 | 131 | 2 | 0 | 141 | 0 | 0 | 10 | 0 | 10 | 427 |
| Total | 30 | 936 | 73 | 1 | 1040 | 57 | 1 | 11 | 0 | 69 | 28 | 454 | 7 | 4 | 493 | 4 | 1 | 28 | 0 | 33 | 1635 |
| | | | | | | | | | | | | | | | | | | | | | |
| 05:00 PM | 9 | 192 | 16 | 0 | 217 | 14 | 0 | 2 | 0 | 16 | 10 | 114 | 1 | 0 | 125 | 1 | 0 | 8 | 0 | 9 | 367 |
| 05:15 PM | 10 | 209 | 14 | 0 | 233 | 16 | 0 | 4 | 0 | 20 | 4 | 141 | 5 | 0 | 150 | 1 | 0 | 6 | 0 | 7 | 410 |
| 05:30 PM | 9 | 224 | 26 | 0 | 259 | 9 | 0 | 1 | 0 | 10 | 10 | 143 | 2 | 0 | 155 | 2 | 0 | 4 | 0 | 6 | 430 |
| 05:45 PM | 9 | 191 | 22 | 0 | 222 | 17 | 0 | 1 | 0 | 18 | 8 | 143 | 5 | 0 | 156 | 2 | 0 | 3 | 0 | 5 | 401 |
| Total | 37 | 816 | 78 | 0 | 931 | 56 | 0 | 8 | 0 | 64 | 32 | 541 | 13 | 0 | 586 | 6 | 0 | 21 | 0 | 27 | 1608 |
| | | | | | | | | | | | | | | | | | | | | | |
| Grand Total | 67 | 1752 | 151 | 1 | 1971 | 113 | 1 | 19 | 0 | 133 | 60 | 995 | 20 | 4 | 1079 | 10 | 1 | 49 | 0 | 60 | 3243 |
| Apprch % | 3.4 | 88.9 | 7.7 | 0.1 | | 85 | 8.0 | 14.3 | 0 | | 5.6 | 92.2 | 1.9 | 0.4 | | 16.7 | 1.7 | 81.7 | 0 | | |
| Total % | 2.1 | 54 | 4.7 | 0 | 60.8 | 3.5 | 0 | 0.6 | 0 | 4.1 | 1.9 | 30.7 | 0.6 | 0.1 | 33.3 | 0.3 | 0 | 1.5 | 0 | 1.9 | |
| Cars + | 66 | 1733 | 151 | 1 | 1951 | 113 | 1 | 19 | 0 | 133 | 60 | 976 | 20 | 4 | 1060 | 10 | 1 | 49 | 0 | 60 | 3204 |
| % Cars + | 98.5 | 98.9 | 100 | 100 | 99 | 100 | 100 | 100 | 0 | 100 | 100 | 98.1 | 100 | 100 | 98.2 | 100 | 100 | 100 | 0 | 100 | 98.8 |
| Trucks | 1 | 19 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 0 | 0 | 19 | 0 | 0 | 0 | 0 | 0 | 39 |
| % Trucks | 1.5 | 11 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 0 | 0 | 1.8 | 0 | 0 | 0 | 0 | 0 | 12 |

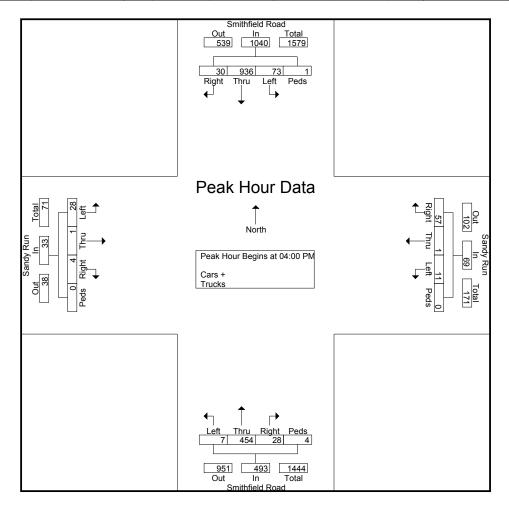


File Name: Knightdale(Smithfield and Sandy Run)PM Peak

Site Code:

Start Date : 1/9/2020

| | | | hfield | | | | | andy F | | | | | thfield | | | | | andy F | | | |
|--------------|--------|---------|--------------|--------|------------|--------|--------|--------|------|------------|-------|------|---------------|------|------------|-------|------|---------------|------|------------|------------|
| | | Sc | <u>uthbo</u> | und | | | W | estbo | und | | | N | <u>orthbo</u> | und | | | E | <u>astboı</u> | ınd | | |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour A | nalysi | s From | า 04:00 | 0 PM t | o 05:45 | PM - | Peak 1 | 1 of 1 | | | | | | | | | | | | | |
| Peak Hour fo | | re Inte | rsection | on Beg | jins at 0 | 4:00 F | PM | | | | | | | | | | | | | | |
| 04:00 PM | 7 | 211 | 15 | 0 | 233 | 14 | 0 | 2 | 0 | 16 | 6 | 112 | 2 | 2 | 122 | 1 | 0 | 6 | 0 | 7 | 378 |
| 04:15 PM | 8 | 229 | 23 | 1 | 261 | 13 | 0 | 3 | 0 | 16 | 9 | 109 | 2 | 2 | 122 | 0 | 0 | 5 | 0 | 5 | 404 |
| 04:30 PM | 3 | 268 | 17 | 0 | 288 | 15 | 1 | 3 | 0 | 19 | 5 | 102 | 1 | 0 | 108 | 3 | 1 | 7 | 0 | 11 | 426 |
| 04:45 PM | 12 | 228 | 18 | 0 | 258 | 15 | 0 | 3 | 0 | 18 | 8 | 131 | 2 | 0 | 141 | 0 | 0 | 10 | 0 | 10 | 427 |
| Total Volume | 30 | 936 | 73 | 1 | 1040 | 57 | 1 | 11 | 0 | 69 | 28 | 454 | 7 | 4 | 493 | 4 | 1 | 28 | 0 | 33 | 1635 |
| % App. Total | 2.9 | 90 | 7 | 0.1 | | 82.6 | 1.4 | 15.9 | 0 | | 5.7 | 92.1 | 1.4 | 0.8 | | 12.1 | 3 | 84.8 | 0 | | |
| PHF | .625 | .873 | .793 | .250 | .903 | .950 | .250 | .917 | .000 | .908 | .778 | .866 | .875 | .500 | .874 | .333 | .250 | .700 | .000 | .750 | .957 |





File Name: Knightdale(Smithfield and Meadow Run)AM Peak

Site Code:

Start Date : 1/9/2020

Page No : 1

| | | | | | | G | roups F | <u> Printed- C</u> | ars + - | Trucks | | | | | | | |
|-------------|-------|----------|--------|------------|-------|------|---------|--------------------|---------|---------|---------|------------|-------|------|-------|------------|------------|
| | | Smithfie | ed Roa | d | | Medo | w Run | | | Smithfi | ed Road | d | | Medo | w Run | | |
| | | South | bound | | | West | bound | | | North | bound | | | East | oound | | |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| 07:00 AM | 1 | 77 | 1 | 79 | 9 | 0 | 0 | 9 | 1 | 279 | 0 | 280 | 0 | 0 | 2 | 2 | 370 |
| 07:15 AM | 2 | 80 | 1 | 83 | 8 | 0 | 0 | 8 | 0 | 270 | 0 | 270 | 0 | 0 | 0 | 0 | 361 |
| 07:30 AM | 1 | 103 | 1 | 105 | 11 | 1 | 0 | 12 | 0 | 289 | 1 | 290 | 0 | 0 | 0 | 0 | 407 |
| 07:45 AM | 2 | 84 | 2 | 88 | 6 | 0 | 2 | 8 | 0 | 259 | 2 | 261 | 0 | 0 | 0 | 0 | 357 |
| Total | 6 | 344 | 5 | 355 | 34 | 1 | 2 | 37 | 1 | 1097 | 3 | 1101 | 0 | 0 | 2 | 2 | 1495 |
| | | | | | | | | | | | | | | | | | |
| 08:00 AM | 1 | 65 | 2 | 68 | 7 | 0 | 1 | 8 | 1 | 222 | 0 | 223 | 0 | 0 | 1 | 1 | 300 |
| 08:15 AM | 2 | 94 | 4 | 100 | 4 | 0 | 0 | 4 | 1 | 267 | 0 | 268 | 0 | 0 | 3 | 3 | 375 |
| 08:30 AM | 1 | 85 | 3 | 89 | 2 | 0 | 0 | 2 | 0 | 267 | 1 | 268 | 0 | 0 | 6 | 6 | 365 |
| 08:45 AM | 3 | 90 | 3 | 96 | 5 | 0 | 0 | 5 | 0 | 226 | 1 | 227 | 0 | 0 | 2 | 2 | 330 |
| Total | 7 | 334 | 12 | 353 | 18 | 0 | 1 | 19 | 2 | 982 | 2 | 986 | 0 | 0 | 12 | 12 | 1370 |
| | | | | | | | | | | | | | | | | | i |
| Grand Total | 13 | 678 | 17 | 708 | 52 | 1 | 3 | 56 | 3 | 2079 | 5 | 2087 | 0 | 0 | 14 | 14 | 2865 |
| Apprch % | 1.8 | 95.8 | 2.4 | | 92.9 | 1.8 | 5.4 | | 0.1 | 99.6 | 0.2 | | 0 | 0 | 100 | | |
| Total % | 0.5 | 23.7 | 0.6 | 24.7 | 1.8 | 0 | 0.1 | 2 | 0.1 | 72.6 | 0.2 | 72.8 | 0 | 0 | 0.5 | 0.5 | |
| Cars + | 13 | 658 | 17 | 688 | 52 | 1 | 3 | 56 | 3 | 2055 | 5 | 2063 | 0 | 0 | 14 | 14 | 2821 |
| % Cars + | 100 | 97.1 | 100 | 97.2 | 100 | 100 | 100 | 100 | 100 | 98.8 | 100 | 98.9 | 0 | 0 | 100 | 100 | 98.5 |
| Trucks | 0 | 20 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 24 | 0 | 24 | 0 | 0 | 0 | 0 | 44 |
| % Trucks | 0 | 2.9 | 0 | 2.8 | 0 | 0 | 0 | 0 | 0 | 1.2 | 0 | 1.1 | 0 | 0 | 0 | 0 | 1.5 |

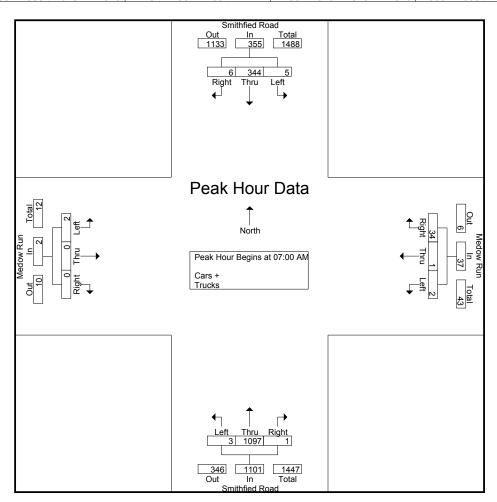


File Name: Knightdale(Smithfield and Meadow Run)AM Peak

Site Code:

Start Date : 1/9/2020

| | | Smithfie | ed Roa | d | | Medo | w Run | | | Smithfie | ed Roa | d | | Medo | w Run | | |
|-----------------|------------|----------|---------|------------|----------|-----------|-------|------------|-------|----------|--------|------------|-------|------|-------|------------|------------|
| | | South | bound | | | West | oound | | | North | bound | | | East | bound | | |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| Peak Hour Ana | alysis Fro | om 07:0 | 00 AM t | o 08:45 A | AM - Pea | ak 1 of 1 | | | _ | | | | _ | | | | |
| Peak Hour for I | Entire In | tersecti | on Beg | ins at 07 | :00 AM | | | | | | | | | | | | |
| 07:00 AM | 1 | 77 | 1 | 79 | 9 | 0 | 0 | 9 | 1 | 279 | 0 | 280 | 0 | 0 | 2 | 2 | 370 |
| 07:15 AM | 2 | 80 | 1 | 83 | 8 | 0 | 0 | 8 | 0 | 270 | 0 | 270 | 0 | 0 | 0 | 0 | 361 |
| 07:30 AM | 1 | 103 | 1 | 105 | 11 | 1 | 0 | 12 | 0 | 289 | 1 | 290 | 0 | 0 | 0 | 0 | 407 |
| 07:45 AM | 2 | 84 | 2 | 88 | 6 | 0 | 2 | 8 | 0 | 259 | 2 | 261 | 0 | 0 | 0 | 0 | 357 |
| Total Volume | 6 | 344 | 5 | 355 | 34 | 1 | 2 | 37 | 1 | 1097 | 3 | 1101 | 0 | 0 | 2 | 2 | 1495 |
| % App. Total | 1.7 | 96.9 | 1.4 | | 91.9 | 2.7 | 5.4 | | 0.1 | 99.6 | 0.3 | | 0 | 0 | 100 | | |
| PHF | .750 | .835 | .625 | .845 | .773 | .250 | .250 | .771 | .250 | .949 | .375 | .949 | .000 | .000 | .250 | .250 | .918 |





File Name: Knightdale(Smithfield and Meadow Run)PM Peak

Site Code:

Start Date : 1/9/2020

Page No : 1

| | | | | | | G | roups F | rinted- C | ars + - | Irucks | | | | | | | |
|-------------|-------|----------|---------|------------|-------|------|---------|------------|---------|----------|---------|------------|-------|-------|-------|------------|------------|
| | | Smithfie | eld Roa | ad | | Medo | w Run | | | Smithfie | eld Roa | d | | Medo | w Run | | |
| | | South | bound | | | West | bound | | | North | bound | | | Eastl | bound | | |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| 04:00 PM | 5 | 233 | 9 | 247 | 8 | 0 | 1 | 9 | 2 | 132 | 0 | 134 | 0 | 1 | 2 | 3 | 393 |
| 04:15 PM | 4 | 266 | 2 | 272 | 1 | 0 | 2 | 3 | 0 | 130 | 1 | 131 | 0 | 0 | 1 | 1 | 407 |
| 04:30 PM | 2 | 288 | 9 | 299 | 4 | 0 | 1 | 5 | 0 | 118 | 0 | 118 | 0 | 0 | 0 | 0 | 422 |
| 04:45 PM | 4 | 256 | 1 | 261 | 3 | 0 | 0 | 3 | 0 | 156 | 3 | 159 | 0 | 0 | 0 | 0 | 423 |
| Total | 15 | 1043 | 21 | 1079 | 16 | 0 | 4 | 20 | 2 | 536 | 4 | 542 | 0 | 1 | 3 | 4 | 1645 |
| | | | | | | | | | | | | | | | | | |
| 05:00 PM | 4 | 208 | 5 | 217 | 2 | 0 | 0 | 2 | 3 | 134 | 2 | 139 | 4 | 0 | 2 | 6 | 364 |
| 05:15 PM | 4 | 241 | 8 | 253 | 3 | 0 | 1 | 4 | 1 | 161 | 2 | 164 | 0 | 0 | 1 | 1 | 422 |
| 05:30 PM | 5 | 244 | 4 | 253 | 0 | 0 | 0 | 0 | 0 | 163 | 0 | 163 | 2 | 0 | 0 | 2 | 418 |
| 05:45 PM | 5 | 232 | 7 | 244 | 4 | 0 | 0 | 4 | 0 | 157 | 3 | 160 | 2 | 0 | 1_ | 3 | 411 |
| Total | 18 | 925 | 24 | 967 | 9 | 0 | 1 | 10 | 4 | 615 | 7 | 626 | 8 | 0 | 4 | 12 | 1615 |
| | | | | | | | | | | | | | | | | | |
| Grand Total | 33 | 1968 | 45 | 2046 | 25 | 0 | 5 | 30 | 6 | 1151 | 11 | 1168 | 8 | 1 | 7 | 16 | 3260 |
| Apprch % | 1.6 | 96.2 | 2.2 | | 83.3 | 0 | 16.7 | | 0.5 | 98.5 | 0.9 | | 50 | 6.2 | 43.8 | | |
| Total % | 1 | 60.4 | 1.4 | 62.8 | 0.8 | 0 | 0.2 | 0.9 | 0.2 | 35.3 | 0.3 | 35.8 | 0.2 | 0 | 0.2 | 0.5 | |
| Cars + | 33 | 1947 | 45 | 2025 | 24 | 0 | 5 | 29 | 6 | 1131 | 11 | 1148 | 8 | 0 | 7 | 15 | 3217 |
| % Cars + | 100 | 98.9 | 100 | 99 | 96 | 0 | 100 | 96.7 | 100 | 98.3 | 100 | 98.3 | 100 | 0 | 100 | 93.8 | 98.7 |
| Trucks | 0 | 21 | 0 | 21 | 1 | 0 | 0 | 1 | 0 | 20 | 0 | 20 | 0 | 1 | 0 | 1 | 43 |
| % Trucks | 0 | 1.1 | 0 | 1 | 4 | 0 | 0 | 3.3 | 0 | 1.7 | 0 | 1.7 | 0 | 100 | 0 | 6.2 | 1.3 |

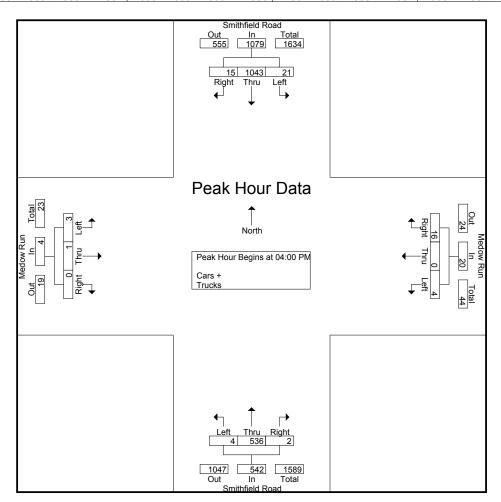


File Name: Knightdale(Smithfield and Meadow Run)PM Peak

Site Code:

Start Date : 1/9/2020

| | Smithfield Road | | | | Medow Run | | | | | Smithfie | eld Roa | d | | | | | |
|-----------------|-----------------|-----------|--------|------------|-----------|-----------|------|------------|------------|----------|---------|------------|-------|------|------|------------|------------|
| | | South | bound | | Westbound | | | | Northbound | | | | | | | | |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| Peak Hour Ana | lysis Fr | om 04:0 | 0 PM t | o 05:45 F | M - Pea | ak 1 of 1 | | | | | | | | | | | |
| Peak Hour for I | Entire In | ntersecti | on Beg | ins at 04 | :00 PM | | | | | | | | | | | | |
| 04:00 PM | 5 | 233 | 9 | 247 | 8 | 0 | 1 | 9 | 2 | 132 | 0 | 134 | 0 | 1 | 2 | 3 | 393 |
| 04:15 PM | 4 | 266 | 2 | 272 | 1 | 0 | 2 | 3 | 0 | 130 | 1 | 131 | 0 | 0 | 1 | 1 | 407 |
| 04:30 PM | 2 | 288 | 9 | 299 | 4 | 0 | 1 | 5 | 0 | 118 | 0 | 118 | 0 | 0 | 0 | 0 | 422 |
| 04:45 PM | 4 | 256 | 1 | 261 | 3 | 0 | 0 | 3 | 0 | 156 | 3 | 159 | 0 | 0 | 0 | 0 | 423 |
| Total Volume | 15 | 1043 | 21 | 1079 | 16 | 0 | 4 | 20 | 2 | 536 | 4 | 542 | 0 | 1 | 3 | 4 | 1645 |
| % App. Total | 1.4 | 96.7 | 1.9 | | 80 | 0 | 20 | | 0.4 | 98.9 | 0.7 | | 0 | 25 | 75 | | |
| PHF | .750 | .905 | .583 | .902 | .500 | .000 | .500 | .556 | .250 | .859 | .333 | .852 | .000 | .250 | .375 | .333 | .972 |





File Name: Knightdale(Water Rock and Poole)AM Peak

Site Code:

Start Date : 1/9/2020

Page No : 1

| | | | | | | G | roups I | rinted- C | ars + - | Irucks | | | | | | | |
|--------------------|-------|---------|--------|------------|-------|------|---------|------------|---------|---------|---------|------------|-------|------|------|------------|------------|
| | Rutl | adge La | anding | Drive | | Pool | Road | | , | Water F | Rock Wa | ay | | | | | |
| | | South | bound | | | West | bound | | | North | | | | | | | |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| 07:00 AM | 11 | 0 | 4 | 15 | 6 | 72 | 2 | 80 | 3 | 0 | 13 | 16 | 2 | 26 | 2 | 30 | 141 |
| 07:15 AM | 2 | 0 | 7 | 9 | 1 | 52 | 2 | 55 | 3 | 0 | 6 | 9 | 1 | 21 | 3 | 25 | 98 |
| 07:30 AM | 2 | 1 | 7 | 10 | 3 | 45 | 0 | 48 | 6 | 1 | 15 | 22 | 3 | 15 | 3 | 21 | 101 |
| 07:45 AM | 5 | 0 | 5 | 10 | 3 | 48 | 3 | 54 | 8 | 0 | 4 | 12 | 3 | 22 | 0 | 25 | 101 |
| Total | 20 | 1 | 23 | 44 | 13 | 217 | 7 | 237 | 20 | 1 | 38 | 59 | 9 | 84 | 8 | 101 | 441 |
| | | | | | | | | | | | | | | | | | |
| 08:00 AM | 3 | 0 | 1 | 4 | 2 | 42 | 2 | 46 | 4 | 0 | 10 | 14 | 2 | 20 | 4 | 26 | 90 |
| 08:15 AM | 4 | 0 | 3 | 7 | 2 | 24 | 1 | 27 | 6 | 1 | 5 | 12 | 0 | 8 | 1 | 9 | 55 |
| 08:30 AM | 7 | 0 | 4 | 11 | 1 | 42 | 2 | 45 | 4 | 0 | 11 | 15 | 0 | 19 | 1 | 20 | 91 |
| 08:45 AM | 7 | 0 | 1 | 8 | 5 | 27 | 4 | 36 | 1 | 0 | 7 | 8 | 0 | 16 | 2 | 18 | 70 |
| Total | 21 | 0 | 9 | 30 | 10 | 135 | 9 | 154 | 15 | 1 | 33 | 49 | 2 | 63 | 8 | 73 | 306 |
| | | | | | | | | | | | | | | | | | |
| Grand Total | 41 | 1 | 32 | 74 | 23 | 352 | 16 | 391 | 35 | 2 | 71 | 108 | 11 | 147 | 16 | 174 | 747 |
| Apprch % | 55.4 | 1.4 | 43.2 | | 5.9 | 90 | 4.1 | | 32.4 | 1.9 | 65.7 | | 6.3 | 84.5 | 9.2 | | |
| Total % | 5.5 | 0.1 | 4.3 | 9.9 | 3.1 | 47.1 | 2.1 | 52.3 | 4.7 | 0.3 | 9.5 | 14.5 | 1.5 | 19.7 | 2.1 | 23.3 | |
| Cars + | 41 | 1 | 32 | 74 | 23 | 344 | 16 | 383 | 34 | 2 | 71 | 107 | 11 | 145 | 16 | 172 | 736 |
| % Cars + | 100 | 100 | 100 | 100 | 100 | 97.7 | 100 | 98 | 97.1 | 100 | 100 | 99.1 | 100 | 98.6 | 100 | 98.9 | 98.5 |
| Trucks | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 1 | 0 | 0 | 1 | 0 | 2 | 0 | 2 | 11 |
| % Trucks | 0 | 0 | 0 | 0 | 0 | 2.3 | 0 | 2 | 2.9 | 0 | 0 | 0.9 | 0 | 1.4 | 0 | 1.1 | 1.5 |

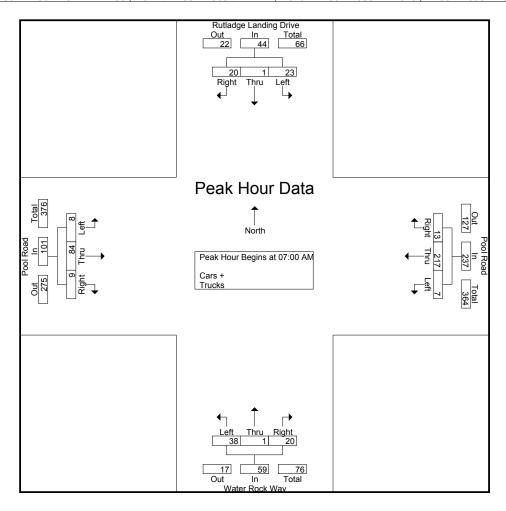


File Name: Knightdale(Water Rock and Poole)AM Peak

Site Code:

Start Date : 1/9/2020

| | Rutladge Landing Drive | | | | Pool Road | | | | Water Rock Way | | | | |] | | | |
|---------------|------------------------|----------|---------|------------|-----------|-----------|------|------------|----------------|------|------|------------|-------|------|------|------------|------------|
| | | South | bound | | Westbound | | | | Northbound | | | | | | | | |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| Peak Hour Ana | alysis Fro | om 07:0 | 00 AM t | o 08:45 A | AM - Pea | ak 1 of 1 | | | _ | | | | _ | | | | |
| Peak Hour for | Entire In | tersecti | on Beg | ins at 07 | :00 AM | | | | | | | | | | | | |
| 07:00 AM | 11 | 0 | 4 | 15 | 6 | 72 | 2 | 80 | 3 | 0 | 13 | 16 | 2 | 26 | 2 | 30 | 141 |
| 07:15 AM | 2 | 0 | 7 | 9 | 1 | 52 | 2 | 55 | 3 | 0 | 6 | 9 | 1 | 21 | 3 | 25 | 98 |
| 07:30 AM | 2 | 1 | 7 | 10 | 3 | 45 | 0 | 48 | 6 | 1 | 15 | 22 | 3 | 15 | 3 | 21 | 101 |
| 07:45 AM | 5 | 0 | 5 | 10 | 3 | 48 | 3 | 54 | 8 | 0 | 4 | 12 | 3 | 22 | 0 | 25 | 101 |
| Total Volume | 20 | 1 | 23 | 44 | 13 | 217 | 7 | 237 | 20 | 1 | 38 | 59 | 9 | 84 | 8 | 101 | 441 |
| % App. Total | 45.5 | 2.3 | 52.3 | | 5.5 | 91.6 | 3 | | 33.9 | 1.7 | 64.4 | | 8.9 | 83.2 | 7.9 | | |
| PHF | .455 | .250 | .821 | .733 | .542 | .753 | .583 | .741 | .625 | .250 | .633 | .670 | .750 | .808 | .667 | .842 | .782 |





File Name: Knightdale(Water Rock and Poole)PM Peak

Site Code:

Start Date : 1/9/2020

Page No : 1

| | | | | | | G | roups I | <u> Printed-C</u> | ars + - | Trucks | | | | | | | |
|-------------|-------|----------|--------|------------|-------|-------|---------|-------------------|------------|---------|---------|------------|-------|------|------|------------|------------|
| | Rut | ledge La | anding | Drive | | Poole | Road | | | Water F | Rock Wa | ay | | | | | |
| | | South | bound | | | West | bound | | Northbound | | | | | | | | |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| 04:00 PM | 4 | 0 | 4 | 8 | 6 | 25 | 4 | 35 | 2 | 1 | 3 | 6 | 5 | 43 | 7 | 55 | 104 |
| 04:15 PM | 8 | 0 | 2 | 10 | 6 | 21 | 0 | 27 | 2 | 0 | 3 | 5 | 6 | 43 | 4 | 53 | 95 |
| 04:30 PM | 6 | 0 | 7 | 13 | 7 | 13 | 2 | 22 | 7 | 0 | 3 | 10 | 10 | 41 | 8 | 59 | 104 |
| 04:45 PM | 3 | 1 | 3 | 7 | 4 | 26 | 4 | 34 | 2 | 0 | 2 | 4 | 6 | 54 | 4 | 64 | 109 |
| Total | 21 | 1 | 16 | 38 | 23 | 85 | 10 | 118 | 13 | 1 | 11 | 25 | 27 | 181 | 23 | 231 | 412 |
| | | | | | | | | | | | | | | | | | |
| 05:00 PM | 5 | 1 | 3 | 9 | 1 | 24 | 5 | 30 | 7 | 0 | 0 | 7 | 6 | 63 | 8 | 77 | 123 |
| 05:15 PM | 8 | 0 | 8 | 16 | 11 | 30 | 4 | 45 | 6 | 0 | 2 | 8 | 8 | 68 | 6 | 82 | 151 |
| 05:30 PM | 5 | 0 | 3 | 8 | 6 | 16 | 4 | 26 | 2 | 1 | 5 | 8 | 9 | 54 | 10 | 73 | 115 |
| 05:45 PM | 2 | 0 | 2 | 4 | 7 | 24 | 1 | 32 | 2 | 0 | 5 | 7 | 15 | 62 | 0 | 77 | 120 |
| Total | 20 | 1 | 16 | 37 | 25 | 94 | 14 | 133 | 17 | 1 | 12 | 30 | 38 | 247 | 24 | 309 | 509 |
| | | | | | | | | | | | | | | | | | |
| Grand Total | 41 | 2 | 32 | 75 | 48 | 179 | 24 | 251 | 30 | 2 | 23 | 55 | 65 | 428 | 47 | 540 | 921 |
| Apprch % | 54.7 | 2.7 | 42.7 | | 19.1 | 71.3 | 9.6 | | 54.5 | 3.6 | 41.8 | | 12 | 79.3 | 8.7 | | |
| Total % | 4.5 | 0.2 | 3.5 | 8.1 | 5.2 | 19.4 | 2.6 | 27.3 | 3.3 | 0.2 | 2.5 | 6 | 7.1 | 46.5 | 5.1 | 58.6 | |
| Cars + | 41 | 2 | 32 | 75 | 48 | 176 | 24 | 248 | 30 | 2 | 23 | 55 | 65 | 417 | 47 | 529 | 907 |
| % Cars + | 100 | 100 | 100 | 100 | 100 | 98.3 | 100 | 98.8 | 100 | 100 | 100 | 100 | 100 | 97.4 | 100 | 98 | 98.5 |
| Trucks | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 11 | 14 |
| % Trucks | 0 | 0 | 0 | 0 | 0 | 1.7 | 0 | 1.2 | 0 | 0 | 0 | 0 | 0 | 2.6 | 0 | 2 | 1.5 |

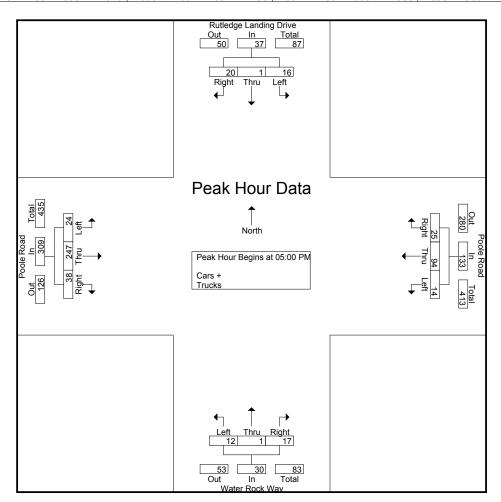


File Name: Knightdale(Water Rock and Poole)PM Peak

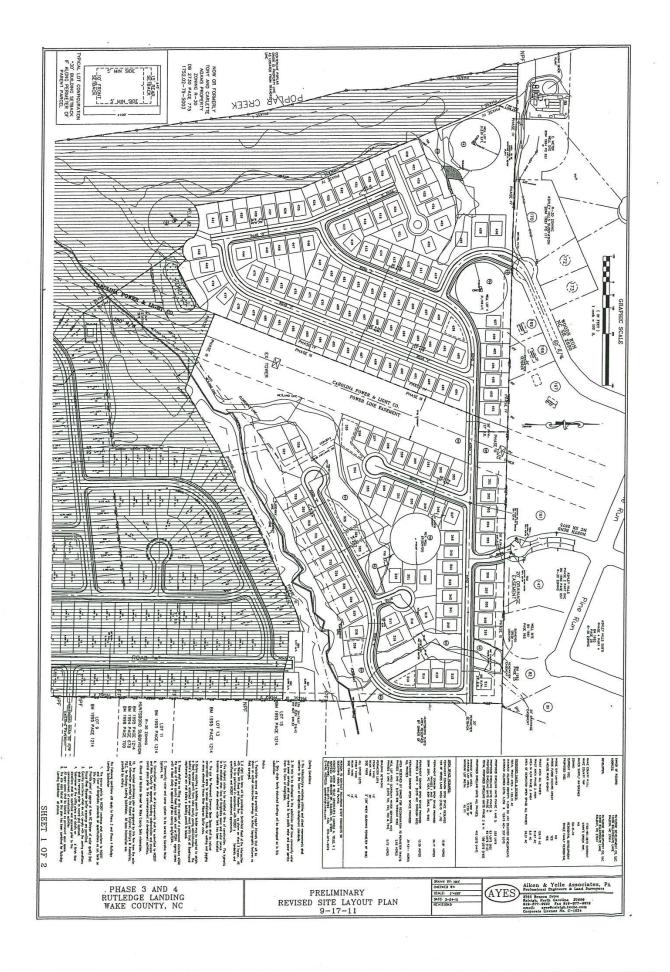
Site Code:

Start Date : 1/9/2020

| | Rutledge Landing Drive | | | | Poole Road | | | | Water Rock Way | | | | |] | | | |
|-----------------|------------------------|----------|--------|------------|------------|-----------|------|------------|----------------|------|------|------------|-------|------|------|------------|------------|
| | | South | bound | | Westbound | | | | Northbound | | | | | | | | |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| Peak Hour Ana | alysis Fro | om 04:0 | 0 PM t | o 05:45 F | PM - Pe | ak 1 of 1 | | | _ | | | | _ | | | | |
| Peak Hour for I | Entire In | tersecti | on Beg | ins at 05 | :00 PM | | | | | | | | | | | | |
| 05:00 PM | 5 | 1 | 3 | 9 | 1 | 24 | 5 | 30 | 7 | 0 | 0 | 7 | 6 | 63 | 8 | 77 | 123 |
| 05:15 PM | 8 | 0 | 8 | 16 | 11 | 30 | 4 | 45 | 6 | 0 | 2 | 8 | 8 | 68 | 6 | 82 | 151 |
| 05:30 PM | 5 | 0 | 3 | 8 | 6 | 16 | 4 | 26 | 2 | 1 | 5 | 8 | 9 | 54 | 10 | 73 | 115 |
| 05:45 PM | 2 | 0 | 2 | 4 | 7 | 24 | 1 | 32 | 2 | 0 | 5 | 7 | 15 | 62 | 0 | 77 | 120 |
| Total Volume | 20 | 1 | 16 | 37 | 25 | 94 | 14 | 133 | 17 | 1 | 12 | 30 | 38 | 247 | 24 | 309 | 509 |
| % App. Total | 54.1 | 2.7 | 43.2 | | 18.8 | 70.7 | 10.5 | | 56.7 | 3.3 | 40 | | 12.3 | 79.9 | 7.8 | | |
| PHF | .625 | .250 | .500 | .578 | .568 | .783 | .700 | .739 | .607 | .250 | .600 | .938 | .633 | .908 | .600 | .942 | .843 |



APPROVED DEVELOPMENT DATA





of Transportation Engineers, Eighth Edition, 2008) and is summarized in Table 1. Detailed trip generation calculations are attached.

| ITE | Table 1 Trip Gene | eration | ı | | | | |
|--------------------------------|----------------------|---------|------|----|-----|-----|-----|
| | | Da | aily | M | P | M | |
| Land Use | Size | In | Out | In | Out | In | Out |
| Single Family Detached Housing | 158 DU | 792 | 792 | 30 | 90 | 100 | 59 |

Table 1 shows that the site has the potential to generate approximately 792 new daily trips in and 792 new daily trips out with 30 new trips entering and 90 new trips exiting in the AM peak hour and 100 new trips entering and 59 new trips exiting in the PM peak hour.

Background Traffic

A 3% annual growth factor was applied to the existing traffic volumes to calculate background traffic volumes in 2014. Traffic for the Poor Boy General Store & Grill Development was also added to the roadway network based on the TIA prepared by CMS Engineering in November 2010. Total background traffic, which includes existing traffic, background growth, and approved development traffic, is shown on Figures 1 and 2 and detailed on the attached intersection worksheets.

Distribution and Assignment

The proposed development site trips were assigned to the study intersections as follows:

- 80% to/from the north on Smithfield Road
- 20% to/from the south on Smithfield Road

Figure 3 shows the site traffic distribution and percent assignment at the study intersections. Site traffic was assigned to the network based on the distributions shown above and added to the background traffic to obtain total traffic volumes. Figures 4 and 5 show the AM and PM peak hour site and total traffic volumes at the two study intersections.

Levels of Service

Capacity analyses were performed for the two study intersections using Synchro Version 7 software. Synchro intersection LOS reports are attached. The level-of-service at each of the study intersections is summarized on Table 2.



A Division of Community Services P.O. Box 550 • Raleigh, NC 27602 www.wakegov.com

April 9, 2019

Brett Clark 2521 Schieffelin Rd, Suite 116 Apex, NC 27502

Re: Rutledge Landing Subdivision (S-08-17)

Dear Mr. Clark,

This letter is in reply to your April 3, 2019 request for an extension of approval for Rutledge Landing Subdivision preliminary plan approval. The Wake County Planning Staff has approved the request for a one (1) year extension of Rutledge Landing Subdivision (S-08-17) approval. The subdivision approval will now expire on **April 27, 2020**. The following conditions of approval still apply:

- 1. Legal documentation must be submitted stating that the public has the authority to use the 50 foot access easement (between Phase 2 and Road Z) as though it were a public road even though it is to be privately maintained. This documentation must be approved by planning staff, the county attorney and the Town of Knightdale prior to final plat approval.
- 2. Smithfield Road at Meadow Run:
 - Construct a northbound and southbound left-turn lane on Smithfield Road with 100 feet of storage and a 100 foot taper. The required turn lanes must be in place prior to any additional traffic being added.
- 3. Construction traffic for Rutledge Landing, phase 3 & 4 must utilize Rutledge Landing Drive located in the existing Rutledge Landing, Phase 1&2.
- 4. Construction traffic for Rutledge Landing, phase 3&4 may only utilized roadways in the existing Ashley Hill Subdivision if the developer bond these roadways for heavy hauling with NCDOT or agrees to strengthen the existing pavement to NCDOT requirements.
- 5. Change the label of the sewer easement from "Proposed 40' City of Raleigh Public Sewer Easement and Town of Knightdale Greenway Easement" to "Proposed 40' City of Raleigh Sewer Easement and Town of Knightdale Greenway Easement".

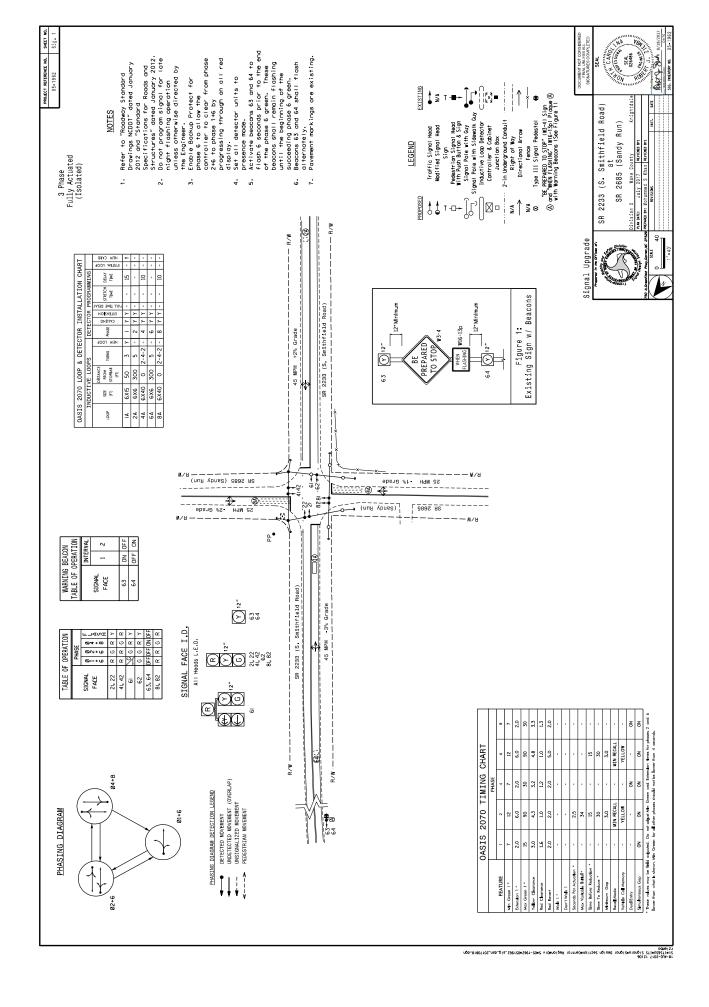
If you need additional information or have any questions or comments regarding this matter, please contact me at 919-856-6214.

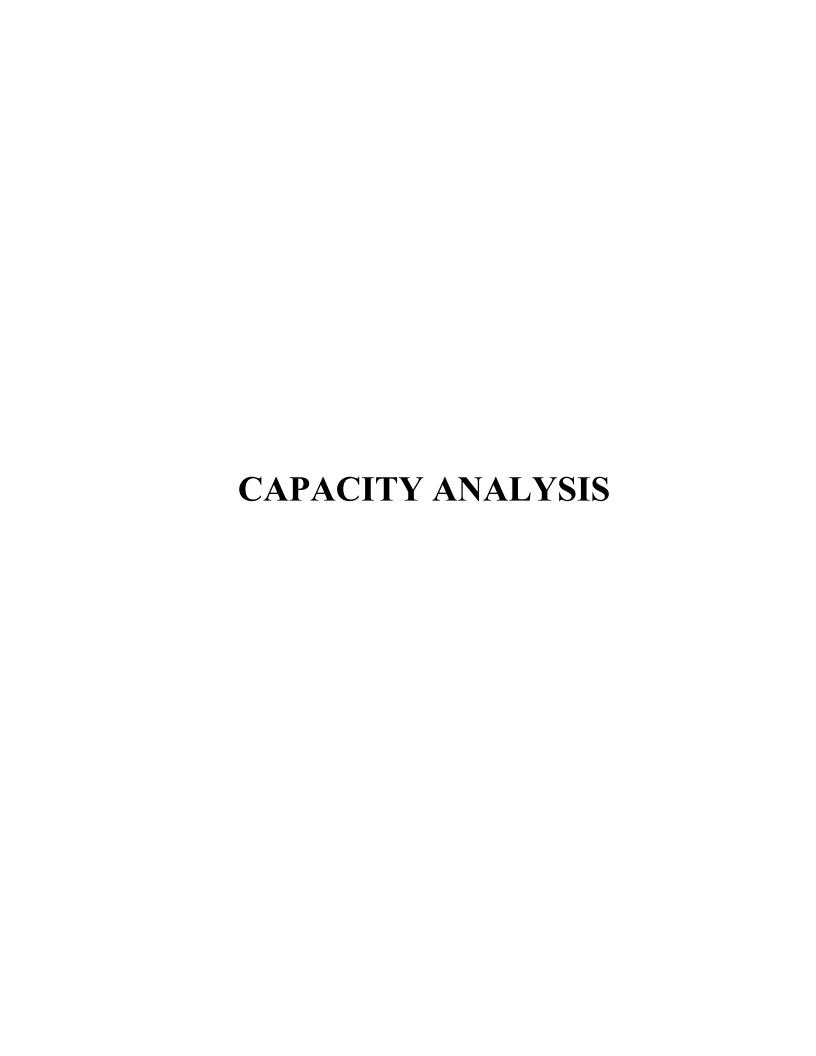
Sincerely,

Celena Everette, Planner II Celena.everette@wakegov.com Wake County Planning Department

cc: file, S-08-17







SMITHFIELD ROAD & POOLE ROAD

| | > | | - | 1 | ← | * | | 1 | 1 | > | ↓ | \checkmark |
|---------------------------------------|-------------|---------|------|-------|----------|------|--------|-------|------|-------------|----------|--------------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | | 4 | | | 43- | |
| Traffic Volume (vph) | 62 | 70 | 17 | 4 | 96 | 23 | 59 | 907 | 4 | 11 | 272 | 52 |
| Future Volume (vph) | 62 | 70 | 17 | 4 | 96 | 23 | 59 | 907 | 4 | 11 | 272 | 52 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (%) | | -1% | | | 3% | | | -2% | | | 2% | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | 0.985 | | | 0.974 | | | 0.999 | | | 0.979 | |
| Flt Protected | | 0.980 | | | 0.999 | | | 0.997 | | | 0.998 | |
| Satd. Flow (prot) | 0 | 1807 | 0 | 0 | 1785 | 0 | 0 | 1874 | 0 | 0 | 1802 | 0 |
| Flt Permitted | | 0.735 | | | 0.991 | | | 0.953 | | | 0.961 | |
| Satd. Flow (perm) | 0 | 1355 | 0 | 0 | 1771 | 0 | 0 | 1791 | 0 | 0 | 1735 | 0 |
| Right Turn on Red | | | No | | | No | | | No | | | No |
| Satd. Flow (RTOR) | | | | | | | | | | | | |
| Link Speed (mph) | | 55 | | | 55 | | | 55 | | | 55 | |
| Link Distance (ft) | | 3665 | | | 2078 | | | 1287 | | | 4951 | |
| Travel Time (s) | | 45.4 | | | 25.8 | | | 16.0 | | | 61.4 | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 69 | 78 | 19 | 4 | 107 | 26 | 66 | 1008 | 4 | 12 | 302 | 58 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 166 | 0 | 0 | 137 | 0 | 0 | 1078 | 0 | 0 | 372 | 0 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | _ | | 6 | _ | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | | 6 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 14.0 | 14.0 | | 14.0 | 14.0 | |
| Minimum Split (s) | 14.0 | 14.0 | | 14.0 | 14.0 | | 21.0 | 21.0 | | 20.0 | 20.0 | |
| Total Split (s) | 40.0 | 40.0 | | 40.0 | 40.0 | | 90.0 | 90.0 | | 90.0 | 90.0 | |
| Total Split (%) | 30.8% | 30.8% | | 30.8% | 30.8% | | 69.2% | 69.2% | | 69.2% | 69.2% | |
| Maximum Green (s) | 33.7 | 33.7 | | 33.6 | 33.6 | | 83.6 | 83.6 | | 84.0 | 84.0 | |
| Yellow Time (s) | 5.3 | 5.3 | | 5.4 | 5.4 | | 5.4 | 5.4 | | 5.0 | 5.0 | |
| All-Red Time (s) | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 | |
| Lost Time Adjust (s) | | -1.3 | | | -1.4 | | | -1.4 | | | -1.0 | |
| Total Lost Time (s) | | 5.0 | | | 5.0 | | | 5.0 | | | 5.0 | |
| Lead/Lag | | | | | | | | | | | | |
| Lead-Lag Optimize? | 6.0 | 6.0 | | 6.0 | 6.0 | | 6.0 | 6.0 | | 6.0 | 6.0 | |
| Vehicle Extension (s) Minimum Gap (s) | 3.4 | 3.4 | | 3.4 | 3.4 | | 3.4 | 3.4 | | 3.4 | 3.4 | |
| Time Before Reduce (s) | 10.0 | 10.0 | | 10.0 | 10.0 | | 20.0 | 20.0 | | 20.0 | 20.0 | |
| Time To Reduce (s) | 20.0 | 20.0 | | 20.0 | 20.0 | | 30.0 | 30.0 | | 30.0 | 30.0 | |
| Recall Mode | None | None | | None | None | | Min | Min | | Min | Min | |
| Act Effct Green (s) | INOILE | 22.2 | | None | 22.2 | | IVIIII | 76.6 | | IVIIII | 76.6 | |
| Actuated g/C Ratio | | 0.20 | | | 0.20 | | | 0.70 | | | 0.70 | |
| v/c Ratio | | 0.60 | | | 0.20 | | | 0.76 | | | 0.70 | |
| Control Delay | | 51.4 | | | 42.8 | | | 21.6 | | | 7.3 | |
| Queue Delay | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Total Delay | | 51.4 | | | 42.8 | | | 21.6 | | | 7.3 | |
| LOS | | D | | | D | | | C C | | | Α | |
| Approach Delay | | 51.4 | | | 42.8 | | | 21.6 | | | 7.3 | |
| | | | | | | | | | | | | |

1: Smithfield Road & Poole Road

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|-------------------------|----------|----------|----------|-----|----------|----------|-----|------|-----|-------------|----------|--------------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Approach LOS | | D | | | D | | | С | | | Α | |
| Queue Length 50th (ft) | | 117 | | | 92 | | | 495 | | | 87 | |
| Queue Length 95th (ft) | | 191 | | | 152 | | | #980 | | | 162 | |
| Internal Link Dist (ft) | | 3585 | | | 1998 | | | 1207 | | | 4871 | |
| Turn Bay Length (ft) | | | | | | | | | | | | |
| Base Capacity (vph) | | 447 | | | 585 | | | 1408 | | | 1364 | |
| Starvation Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Spillback Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Storage Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Reduced v/c Ratio | | 0.37 | | | 0.23 | | | 0.77 | | | 0.27 | |
| Intersection Summary | | | | | | | | | | | | |

Area Type: Other

Cycle Length: 130 Actuated Cycle Length: 109

Natural Cycle: 60

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.86 Intersection Signal Delay: 23.0 Intersection Capacity Utilization 96.3%

Intersection LOS: C
ICU Level of Service F

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 1: Smithfield Road & Poole Road



Lanes, Volumes, Timings 1: Smithfield Road & Poole Road

| | * | | / | _ | + | 4 | 4 | 4 | | / | | 1 |
|--|-------------|--------------|------|-------------|--------------|------|-------------|-------------|------|------------|--------------|------|
| | 5 D. | EDT. | 500 | 14/54 | MOT | WDD | MBI | NDT | MDD | 0.01 | 0.0.7 | 000 |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | 40 | 4 | | 40 | 4 | | 40 | 4 | 50 |
| Traffic Volume (vph) | 80 | 109 | 69 | 12 | 82 | 30 | 16 | 442 | 6 | 12 | 752 | 58 |
| Future Volume (vph) | 80 | 109 | 69 | 12 | 82 | 30 | 16 | 442 | 6 | 12 | 752 | 58 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (%) | | -1% | | | 3% | | | -2% | | | 2% | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | 0.964 | | | 0.967 | | | 0.998 | | | 0.991 | |
| Flt Protected | | 0.985 | | | 0.995 | | | 0.998 | | | 0.999 | |
| Satd. Flow (prot) | 0 | 1778 | 0 | 0 | 1765 | 0 | 0 | 1874 | 0 | 0 | 1826 | 0 |
| Flt Permitted | • | 0.833 | • | • | 0.960 | • | • | 0.959 | • | • | 0.991 | • |
| Satd. Flow (perm) | 0 | 1503 | . 0 | 0 | 1703 | .0 | 0 | 1801 | . 0 | 0 | 1811 | 0 |
| Right Turn on Red | | | No | | | No | | | No | | | No |
| Satd. Flow (RTOR) | | | | | | | | | | | | |
| Link Speed (mph) | | 55 | | | 55 | | | 55 | | | 55 | |
| Link Distance (ft) | | 3665 | | | 2078 | | | 1287 | | | 4951 | |
| Travel Time (s) | | 45.4 | | | 25.8 | | | 16.0 | | | 61.4 | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 89 | 121 | 77 | 13 | 91 | 33 | 18 | 491 | 7 | 13 | 836 | 64 |
| Shared Lane Traffic (%) | | | | | | _ | | | | | | _ |
| Lane Group Flow (vph) | 0 | 287 | 0 | 0 | 137 | 0 | 0 | 516 | 0 | 0 | 913 | 0 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 4 | | • | 8 | | • | 2 | | • | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | _ | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | | 6 | 6 | |
| Switch Phase | 7.0 | 7.0 | | 7.0 | 7.0 | | 440 | 440 | | 44.0 | 440 | |
| Minimum Initial (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 14.0 | 14.0 | | 14.0 | 14.0 | |
| Minimum Split (s) | 14.0 | 14.0 | | 14.0 | 14.0 | | 21.0 | 21.0 | | 20.0 | 20.0 | |
| Total Split (s) | 40.0 | 40.0 | | 40.0 | 40.0 | | 90.0 | 90.0 | | 90.0 | 90.0 | |
| Total Split (%) | 30.8% | 30.8% | | 30.8% | 30.8% | | 69.2% | 69.2% | | 69.2% | 69.2% | |
| Maximum Green (s) | 33.7 | 33.7 | | 33.6 | 33.6 | | 83.6 | 83.6 | | 84.0 | 84.0 | |
| Yellow Time (s) | 5.3 | 5.3 | | 5.4 | 5.4 | | 5.4 | 5.4 | | 5.0 | 5.0 | |
| All-Red Time (s) | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 | |
| Lost Time Adjust (s) | | -1.3 | | | -1.4 | | | -1.4 | | | -1.0 | |
| Total Lost Time (s) | | 5.0 | | | 5.0 | | | 5.0 | | | 5.0 | |
| Lead/Lag | | | | | | | | | | | | |
| Lead-Lag Optimize? | 6.0 | 6.0 | | 6.0 | 6.0 | | 6.0 | 6.0 | | 6.0 | 6.0 | |
| Vehicle Extension (s) | 6.0 3.4 | 6.0 3.4 | | 6.0 3.4 | 6.0 3.4 | | 6.0 | 6.0 3.4 | | 6.0 3.4 | 6.0 3.4 | |
| Minimum Gap (s) Time Before Reduce (s) | 3.4 10.0 | 3.4 10.0 | | 3.4 10.0 | 3.4 10.0 | | 3.4 20.0 | 20.0 | | 20.0 | 20.0 | |
| Time To Reduce (s) | 20.0 | 20.0 | | 20.0 | 20.0 | | 30.0 | 30.0 | | 30.0 | 30.0 | |
| Recall Mode | | | | | | | | | | Min | Min | |
| | None | None 28.9 | | None | None 28.9 | | Min | Min 66.9 | | IVIIII | 66.9 | |
| Act Effct Green (s) | | 0.27 | | | 0.27 | | | 0.63 | | | | |
| Actuated g/C Ratio v/c Ratio | | 0.27 | | | 0.27 | | | 0.63 | | | 0.63 0.80 | |
| Control Delay | | 0.70 48.4 | | | 36.3 | | | 11.9 | | | 21.6 | |
| Queue Delay | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Total Delay | | 48.4 | | | 36.3 | | | 11.9 | | | 21.6 | |
| LOS | | 40.4 D | | | 30.3 D | | | 11.9 B | | | 21.0 C | |
| Approach Delay | | 48.4 | | | 36.3 | | | 11.9 | | | 21.6 | |
| Approach Dolay | | +0.+ | | | 00.0 | | | 11.5 | | | 21.0 | |

1: Smithfield Road & Poole Road

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|-------------------------|-------------|---------|-----|-----|----------|-----|-----|------|-----|-------------|----------|--------------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Approach LOS | | D | | | D | | | В | | | С | |
| Queue Length 50th (ft) | | 187 | | | 78 | | | 180 | | | 459 | |
| Queue Length 95th (ft) | | 327 | | | 151 | | | 270 | | | 690 | |
| Internal Link Dist (ft) | | 3585 | | | 1998 | | | 1207 | | | 4871 | |
| Turn Bay Length (ft) | | | | | | | | | | | | |
| Base Capacity (vph) | | 525 | | | 595 | | | 1440 | | | 1448 | |
| Starvation Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Spillback Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Storage Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Reduced v/c Ratio | | 0.55 | | | 0.23 | | | 0.36 | | | 0.63 | |
| Intersection Summary | | | | | | | | | | | | |

Area Type: Other

Cycle Length: 130

Actuated Cycle Length: 106.4

Natural Cycle: 60

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.80 Intersection Signal Delay: 24.1 Intersection Capacity Utilization 77.3%

Intersection LOS: C ICU Level of Service D

Analysis Period (min) 15

Splits and Phases: 1: Smithfield Road & Poole Road



Total Delay

Approach Delay

LOS

1 Lane Group **EBL EBT EBR WBL WBT WBR** NBL **NBT NBR** SBL **SBR** Lane Configurations 4 4 81 107 25 993 302 Traffic Volume (vph) 32 12 68 4 68 4 57 993 4 Future Volume (vph) 68 81 32 4 107 25 68 12 302 57 Ideal Flow (vphpl) 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 1900 Grade (%) -1% 3% -2% 2% Lane Util. Factor 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 Frt 0.976 0.975 0.979 Flt Protected 0.982 0.999 0.997 0.998 0 0 0 0 0 0 Satd. Flow (prot) 1794 0 1787 1876 0 1802 0.713 0.944 0.954 Flt Permitted 0.992 Satd. Flow (perm) 0 1303 0 0 1775 0 1776 0 0 1722 0 Right Turn on Red No No No No Satd. Flow (RTOR) 55 Link Speed (mph) 55 55 55 2078 1287 Link Distance (ft) 3665 4951 Travel Time (s) 45.4 25.8 16.0 61.4 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 Peak Hour Factor 0.90 Adj. Flow (vph) 76 119 28 76 1103 4 13 336 90 36 4 63 Shared Lane Traffic (%) 0 202 0 0 0 0 0 0 0 Lane Group Flow (vph) 151 1183 412 Perm Turn Type Perm NA Perm NA NA Perm NA **Protected Phases** 8 2 4 6 2 Permitted Phases 4 8 6 8 2 2 6 **Detector Phase** 4 4 8 6 Switch Phase Minimum Initial (s) 7.0 7.0 7.0 7.0 14.0 14.0 14.0 14.0 21.0 21.0 20.0 Minimum Split (s) 14.0 14.0 14.0 14.0 20.0 Total Split (s) 40.0 40.0 40.0 40.0 90.0 90.0 90.0 90.0 Total Split (%) 30.8% 30.8% 30.8% 30.8% 69.2% 69.2% 69.2% 69.2% Maximum Green (s) 33.7 33.7 33.6 33.6 83.6 83.6 84.0 84.0 Yellow Time (s) 5.3 5.3 5.4 5.4 5.4 5.4 5.0 5.0 All-Red Time (s) 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 Lost Time Adjust (s) -1.3 -1.4 -1.4 -1.0 Total Lost Time (s) 5.0 5.0 5.0 5.0 Lead/Lag Lead-Lag Optimize? 6.0 6.0 6.0 6.0 Vehicle Extension (s) 6.0 6.0 6.0 6.0 Minimum Gap (s) 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.4 Time Before Reduce (s) 10.0 10.0 10.0 10.0 20.0 20.0 20.0 20.0 Time To Reduce (s) 20.0 20.0 20.0 20.0 30.0 30.0 30.0 30.0 Recall Mode None None None None Min Min Min Min Act Effct Green (s) 26.0 26.0 85.2 85.2 Actuated q/C Ratio 0.21 0.21 0.70 0.70 v/c Ratio 0.72 0.40 0.95 0.34 Control Delay 59.4 43.6 34.1 8.8 0.0 Queue Delay 0.0 0.0 0.0

Poole Road Project Synchro 10 Report
RKA Page 1

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Background (2023) AM 01/16/2020

1: Smithfield Road & Poole Road

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|-------------------------|----------|----------|-----|-----|----------|-----|-----|-------|-----|-------------|----------|--------------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Approach LOS | | Е | | | D | | | С | | | Α | |
| Queue Length 50th (ft) | | 148 | | | 102 | | | 742 | | | 113 | |
| Queue Length 95th (ft) | | 234 | | | 164 | | | #1317 | | | 207 | |
| Internal Link Dist (ft) | | 3585 | | | 1998 | | | 1207 | | | 4871 | |
| Turn Bay Length (ft) | | | | | | | | | | | | |
| Base Capacity (vph) | | 376 | | | 513 | | | 1247 | | | 1209 | |
| Starvation Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Spillback Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Storage Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Reduced v/c Ratio | | 0.54 | | | 0.29 | | | 0.95 | | | 0.34 | |
| Intersection Summary | | | | | | | | | | | | |

Area Type: Other

Cycle Length: 130

Actuated Cycle Length: 121.3

Natural Cycle: 90

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.95 Intersection Signal Delay: 32.1 Intersection Capacity Utilization 110.3%

Intersection LOS: C
ICU Level of Service H

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 1: Smithfield Road & Poole Road



| | ≯ | | 1 | | ļ | A. | « | 1 | > | / | 1 | 1 |
|--------------------------------|----------|------------|------|----------|------------|------|------------|-------|-------------|----------|-------------|----------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| | LDL | LDI | LDIN | WDL | | WDIX | NDL | | NDIX | JDL | 301 | JUIN |
| Lane Configurations | 87 | 100 | 84 | 12 | 4 | 33 | 32 | 488 | 7 | 12 | 005 | 62 |
| Traffic Volume (vph) | 87 | 122 122 | 84 | 13 13 | 95 95 | 33 | 32 32 | 488 | 7 7 | 13 13 | 825 825 | 63 63 |
| Future Volume (vph) | 1900 | 1900 | 1900 | 1900 | 95 1900 | 1900 | 32 1900 | 1900 | 1900 | 1900 | 025 1900 | 1900 |
| Ideal Flow (vphpl) | 1900 | -1% | 1900 | 1900 | 3% | 1900 | 1900 | -2% | 1900 | 1900 | 2% | 1900 |
| Grade (%) Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.961 | 1.00 | 1.00 | 0.968 | 1.00 | 1.00 | 0.998 | 1.00 | 1.00 | 0.991 | 1.00 |
| FIt Protected | | 0.985 | | | 0.996 | | | 0.997 | | | 0.999 | |
| Satd. Flow (prot) | 0 | 1772 | 0 | 0 | 1769 | 0 | 0 | 1872 | 0 | 0 | 1826 | 0 |
| Flt Permitted | U | 0.796 | U | U | 0.959 | U | U | 0.901 | U | U | 0.990 | U |
| Satd. Flow (perm) | 0 | 1432 | 0 | 0 | 1703 | 0 | 0 | 1692 | 0 | 0 | 1809 | 0 |
| Right Turn on Red | U | 1432 | No | U | 1703 | No | U | 1032 | No | U | 1003 | No |
| Satd. Flow (RTOR) | | | INO | | | 110 | | | INO | | | NO |
| Link Speed (mph) | | 55 | | | 55 | | | 55 | | | 55 | |
| Link Distance (ft) | | 3665 | | | 2078 | | | 1287 | | | 4951 | |
| Travel Time (s) | | 45.4 | | | 25.8 | | | 16.0 | | | 61.4 | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 97 | 136 | 93 | 14 | 106 | 37 | 36 | 542 | 8 | 14 | 917 | 70 |
| Shared Lane Traffic (%) | 31 | 100 | 30 | 17 | 100 | 01 | 30 | 072 | U | 17 | 317 | 70 |
| Lane Group Flow (vph) | 0 | 326 | 0 | 0 | 157 | 0 | 0 | 586 | 0 | 0 | 1001 | 0 |
| Turn Type | Perm | NA | Ū | Perm | NA | Ū | Perm | NA | Ū | Perm | NA | O |
| Protected Phases | 1 01111 | 4 | | 1 01111 | 8 | | 1 01111 | 2 | | 1 01111 | 6 | |
| Permitted Phases | 4 | | | 8 | ŭ | | 2 | _ | | 6 | ŭ | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | | 6 | 6 | |
| Switch Phase | - | • | | · · | · · | | _ | _ | | • | • | |
| Minimum Initial (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 14.0 | 14.0 | | 14.0 | 14.0 | |
| Minimum Split (s) | 14.0 | 14.0 | | 14.0 | 14.0 | | 21.0 | 21.0 | | 20.0 | 20.0 | |
| Total Split (s) | 40.0 | 40.0 | | 40.0 | 40.0 | | 90.0 | 90.0 | | 90.0 | 90.0 | |
| Total Split (%) | 30.8% | 30.8% | | 30.8% | 30.8% | | 69.2% | 69.2% | | 69.2% | 69.2% | |
| Maximum Green (s) | 33.7 | 33.7 | | 33.6 | 33.6 | | 83.6 | 83.6 | | 84.0 | 84.0 | |
| Yellow Time (s) | 5.3 | 5.3 | | 5.4 | 5.4 | | 5.4 | 5.4 | | 5.0 | 5.0 | |
| All-Red Time (s) | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 | |
| Lost Time Adjust (s) | | -1.3 | | | -1.4 | | | -1.4 | | | -1.0 | |
| Total Lost Time (s) | | 5.0 | | | 5.0 | | | 5.0 | | | 5.0 | |
| Lead/Lag | | | | | | | | | | | | |
| Lead-Lag Optimize? | | | | | | | | | | | | |
| Vehicle Extension (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | 6.0 | 6.0 | | 6.0 | 6.0 | |
| Minimum Gap (s) | 3.4 | 3.4 | | 3.4 | 3.4 | | 3.4 | 3.4 | | 3.4 | 3.4 | |
| Time Before Reduce (s) | 10.0 | 10.0 | | 10.0 | 10.0 | | 20.0 | 20.0 | | 20.0 | 20.0 | |
| Time To Reduce (s) | 20.0 | 20.0 | | 20.0 | 20.0 | | 30.0 | 30.0 | | 30.0 | 30.0 | |
| Recall Mode | None | None | | None | None | | Min | Min | | Min | Min | |
| Act Effct Green (s) | | 32.7 | | | 32.7 | | | 75.7 | | | 75.7 | |
| Actuated g/C Ratio | | 0.28 | | | 0.28 | | | 0.64 | | | 0.64 | |
| v/c Ratio | | 0.83 | | | 0.33 | | | 0.54 | | | 0.87 | |
| Control Delay | | 60.9 | | | 39.0 | | | 14.1 | | | 27.2 | |
| Queue Delay | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Total Delay | | 60.9 | | | 39.0 | | | 14.1 | | | 27.2 | |
| LOS | | Е | | | D | | | В | | | С | |
| Approach Delay | | 60.9 | | | 39.0 | | | 14.1 | | | 27.2 | |

Poole Road Project RKA Synchro 10 Report Page 1

1: Smithfield Road & Poole Road

| | > | - | - | 1 | ← | * | | 1 | 1 | > | ↓ | \checkmark |
|-------------------------|-------------|----------|-----|-----|----------|-----|-----|------|-----|-------------|----------|--------------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Approach LOS | | Е | | | D | | | В | | | С | |
| Queue Length 50th (ft) | | 261 | | | 107 | | | 243 | | | 608 | |
| Queue Length 95th (ft) | | #422 | | | 172 | | | 336 | | | 852 | |
| Internal Link Dist (ft) | | 3585 | | | 1998 | | | 1207 | | | 4871 | |
| Turn Bay Length (ft) | | | | | | | | | | | | |
| Base Capacity (vph) | | 432 | | | 514 | | | 1242 | | | 1327 | |
| Starvation Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Spillback Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Storage Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Reduced v/c Ratio | | 0.75 | | | 0.31 | | | 0.47 | | | 0.75 | |
| Intersection Summary | | | | | | | | | | | | |

Area Type:

Cycle Length: 130

Actuated Cycle Length: 118.7

Natural Cycle: 75

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.87 Intersection Signal Delay: 29.7 Intersection Capacity Utilization 87.6%

Intersection LOS: C
ICU Level of Service E

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Other

Splits and Phases: 1: Smithfield Road & Poole Road



| | _ | | | | 4 | _ | | _ | | | | , |
|--|---------|--------------|------|---------|--------------|------|------------|-------------------|------|---------|--------------|----------------------|
| | 1 | | * | 1 | • | | | T | | - | ↓ | \blacktriangleleft |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | | 4 | | | - 4 | |
| Traffic Volume (vph) | 68 | 82 | 36 | 4 | 108 | 25 | 69 | 994 | 4 | 12 | 303 | 57 |
| Future Volume (vph) | 68 | 82 | 36 | 4 | 108 | 25 | 69 | 994 | 4 | 12 | 303 | 57 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (%) | | -1% | | | 3% | | | -2% | | | 2% | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | 0.974 | | | 0.975 | | | | | | 0.979 | |
| Flt Protected | | 0.982 | | | 0.999 | | | 0.997 | | | 0.998 | |
| Satd. Flow (prot) | 0 | 1791 | 0 | 0 | 1787 | 0 | 0 | 1876 | 0 | 0 | 1802 | 0 |
| Flt Permitted | | 0.720 | | | 0.992 | | | 0.943 | | | 0.954 | |
| Satd. Flow (perm) | 0 | 1313 | . 0 | 0 | 1775 | .0 | 0 | 1774 | .0 | 0 | 1722 | 0 |
| Right Turn on Red | | | No | | | No | | | No | | | No |
| Satd. Flow (RTOR) | | | | | | | | | | | | |
| Link Speed (mph) | | 55 2005 | | | 55 | | | 55 4007 | | | 55 4054 | |
| Link Distance (ft) | | 3665 | | | 2078 | | | 1287 | | | 4951 | |
| Travel Time (s) | 0.90 | 45.4 0.90 | 0.90 | 0.90 | 25.8 0.90 | 0.90 | 0.90 | 16.0 0.90 | 0.90 | 0.90 | 61.4 0.90 | 0.90 |
| Peak Hour Factor | 76 | 0.90 91 | 40 | | 120 | 28 | 0.90 77 | 1104 | 0.90 | 13 | 337 | 63 |
| Adj. Flow (vph) Shared Lane Traffic (%) | 70 | 91 | 40 | 4 | 120 | 20 | 11 | 1104 | 4 | 13 | 331 | 03 |
| Lane Group Flow (vph) | 0 | 207 | 0 | 0 | 152 | 0 | 0 | 1185 | 0 | 0 | 413 | 0 |
| Turn Type | Perm | NA | U | Perm | NA | U | Perm | NA | U | Perm | NA | U |
| Protected Phases | i Giiii | 4 | | i Giiii | 8 | | i Cilli | 2 | | i Giiii | 6 | |
| Permitted Phases | 4 | 7 | | 8 | O | | 2 | _ | | 6 | Ū | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | | 6 | 6 | |
| Switch Phase | • | • | | ŭ | ŭ | | _ | _ | | ŭ | · | |
| Minimum Initial (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 14.0 | 14.0 | | 14.0 | 14.0 | |
| Minimum Split (s) | 14.0 | 14.0 | | 14.0 | 14.0 | | 21.0 | 21.0 | | 20.0 | 20.0 | |
| Total Split (s) | 40.0 | 40.0 | | 40.0 | 40.0 | | 90.0 | 90.0 | | 90.0 | 90.0 | |
| Total Split (%) | 30.8% | 30.8% | | 30.8% | 30.8% | | 69.2% | 69.2% | | 69.2% | 69.2% | |
| Maximum Green (s) | 33.7 | 33.7 | | 33.6 | 33.6 | | 83.6 | 83.6 | | 84.0 | 84.0 | |
| Yellow Time (s) | 5.3 | 5.3 | | 5.4 | 5.4 | | 5.4 | 5.4 | | 5.0 | 5.0 | |
| All-Red Time (s) | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 | |
| Lost Time Adjust (s) | | -1.3 | | | -1.4 | | | -1.4 | | | -1.0 | |
| Total Lost Time (s) | | 5.0 | | | 5.0 | | | 5.0 | | | 5.0 | |
| Lead/Lag | | | | | | | | | | | | |
| Lead-Lag Optimize? | | | | | | | | | | | | |
| Vehicle Extension (s) | 6.0 | 6.0 | | 6.0 | 6.0 | | 6.0 | 6.0 | | 6.0 | 6.0 | |
| Minimum Gap (s) | 3.4 | 3.4 | | 3.4 | 3.4 | | 3.4 | 3.4 | | 3.4 | 3.4 | |
| Time Before Reduce (s) | 10.0 | 10.0 | | 10.0 | 10.0 | | 20.0 | 20.0 | | 20.0 | 20.0 | |
| Time To Reduce (s) | 20.0 | 20.0 | | 20.0 | 20.0 | | 30.0 | 30.0 | | 30.0 | 30.0 | |
| Recall Mode | None | None | | None | None | | Min | Min | | Min | Min | |
| Act Effet Green (s) | | 26.4 | | | 26.4 | | | 85.2 | | | 85.2 | |
| Actuated g/C Ratio | | 0.22 | | | 0.22 | | | 0.70 | | | 0.70 | |
| v/c Ratio | | 0.73 59.3 | | | 0.40 43.4 | | | 0.95 35.2 | | | 0.34 8.9 | |
| Control Delay Queue Delay | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Total Delay | | 59.3 | | | 43.4 | | | 35.2 | | | 8.9 | |
| LOS | | 39.3 E | | | 43.4 D | | | 33. <u>2</u> D | | | 0.9 A | |
| Approach Delay | | 59.3 | | | 43.4 | | | 35.2 | | | 8.9 | |
| | | 55.5 | | | .0.1 | | | 50. <u>L</u> | | | 0.0 | |

Poole Road Project RKA Synchro 10 Report Page 1

Combined (2023) AM

01/16/2020

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|-------------------------|----------|----------|----------|-----|----------|-----|-----|-------|-----|-------------|----------|--------------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Approach LOS | | Е | | | D | | | D | | | Α | |
| Queue Length 50th (ft) | | 152 | | | 103 | | | 760 | | | 115 | |
| Queue Length 95th (ft) | | 239 | | | 166 | | | #1322 | | | 208 | |
| Internal Link Dist (ft) | | 3585 | | | 1998 | | | 1207 | | | 4871 | |
| Turn Bay Length (ft) | | | | | | | | | | | | |
| Base Capacity (vph) | | 378 | | | 511 | | | 1242 | | | 1206 | |
| Starvation Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Spillback Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Storage Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Reduced v/c Ratio | | 0.55 | | | 0.30 | | | 0.95 | | | 0.34 | |
| Intersection Summary | | | | | | | | | | | | |

Area Type: Other

Cycle Length: 130

Actuated Cycle Length: 121.6

Natural Cycle: 90

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.95 Intersection Signal Delay: 32.9 Intersection Capacity Utilization 110.8%

Intersection LOS: C
ICU Level of Service H

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 1: Smithfield Road & Poole Road



| Lanes, voiumes, minings | | | COII |
|---------------------------------|--|--|------|
| 1: Smithfield Road & Poole Road | | | |
| | | | |

| Lane Group | | ≯ | | \ | 1 | ← | * | | 1 | / | 1 | ↓ | \checkmark |
|--|--------------------|----------|---------|----------|------|----------|------|------|-------|----------|------|----------|--------------|
| Lane Configurations | Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Traffix Ovlume (vph) | | | | | | | | | 4 | | | 4 | |
| Future Volume (viph) 190 1900 | | 87 | | 86 | 13 | | 33 | 36 | 489 | 7 | 13 | 826 | 63 |
| Ideal Flow (yphp) 1900 1809 1800 18 | | | | | | | | | | 7 | | | |
| Lane Uflil. Factor | Ideal Flow (vphpl) | 1900 | | 1900 | 1900 | 1900 | 1900 | 1900 | | 1900 | 1900 | 1900 | 1900 |
| Fith | Grade (%) | | -1% | | | 3% | | | -2% | | | 2% | |
| Filt Producted | Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Satt Flow (prot) 0 | Frt | | 0.961 | | | 0.968 | | | 0.998 | | | 0.991 | |
| Fit Permitted | Flt Protected | | 0.986 | | | 0.996 | | | 0.997 | | | 0.999 | |
| Satd. Flow (perm) 0 | Satd. Flow (prot) | 0 | 1774 | 0 | 0 | 1769 | 0 | 0 | 1872 | 0 | 0 | 1826 | 0 |
| Right Tum on Red Satd. Flow (RTOR) Satd. F | Flt Permitted | | | | | | | | | | | | |
| Satid. Flow (RTOR) Link Speed (mph) 55 55 2078 1287 4951 1287 4951 1748 | Satd. Flow (perm) | 0 | 1434 | 0 | 0 | 1703 | 0 | 0 | 1667 | 0 | 0 | 1809 | 0 |
| Link Speed (mph) 55 55 55 55 Link Distance (n) 3665 2078 1287 4951 4951 177 4951 178 188 188 188 188 188 188 188 188 189 0.90 9.00 9.00 9.00 9.00 9.00 9.00 9.00 9.00 9.00 9.00 | Right Turn on Red | | | No | | | No | | | No | | | No |
| Link Distance (ft) 3665 2078 1287 4951 Travel Time (s) 45.4 25.8 16.0 61.4 Peak Hour Factor 0.90 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | Satd. Flow (RTOR) | | | | | | | | | | | | |
| Travel Time (s) 45.4 25.8 16.0 61.4 Peak Hour Factor 0.90 | Link Speed (mph) | | | | | | | | | | | | |
| Peak Hour Factor Adj. Flow (vph) 90 0.90 9.00 | | | | | | | | | | | | | |
| Adj. Flow (vph) | | | | | | | | | | | | | |
| Shared Lane Traffic (%) Lane Group Flow (ych) 0 0 330 0 0 0 158 0 0 591 0 0 1002 0 1007 | | | | | | | | | | | | | |
| Lane Group Flow (vph) | | 97 | 137 | 96 | 14 | 107 | 37 | 40 | 543 | 8 | 14 | 918 | 70 |
| Tum Type | ` ' | | | | | | | | | | | | |
| Protected Phases | | | | 0 | | | 0 | | | 0 | | | 0 |
| Permitted Phases | | Perm | | | Perm | | | Perm | | | Perm | | |
| Detector Phase 4 | | | 4 | | | 8 | | | 2 | | | 6 | |
| Switch Phase Minimum Initial (s) 7.0 7.0 7.0 7.0 14.0 21.0 20 | | | | | | | | | _ | | | | |
| Minimum Initial (s) 7.0 7.0 7.0 7.0 14.0 14.0 14.0 14.0 14.0 14.0 14.0 14.0 14.0 14.0 14.0 21.0 21.0 20.0 20.0 20.0 Total Split (s) 40.0 40.0 40.0 40.0 90.0 80.2 80.2% 69.2% 69.2% 69.2% 69.2% 69.2% 69.2% 69.2% 69.2% 69.2% 69.2% 69.2% 69.2% 69.2% | | 4 | 4 | | 8 | 8 | | 2 | 2 | | 6 | 6 | |
| Minimum Split (s) 14.0 14.0 14.0 14.0 21.0 21.0 20.0 20.0 Total Split (s) 40.0 40.0 40.0 40.0 90.0 90.0 90.0 90.0 Total Split (%) 30.8% 30.8% 30.8% 30.8% 69.2% 69.2% 69.2% 69.2% Maximum Green (s) 33.7 33.7 33.6 33.6 83.6 83.6 84.0 84.0 Yellow Time (s) 5.3 5.3 5.4 5.4 5.4 5.4 5.0 5.0 All-Red Time (s) 1.0 </td <td></td> <td>7.0</td> <td></td> <td></td> <td>7.0</td> <td>- 0</td> <td></td> <td>440</td> <td>440</td> <td></td> <td>440</td> <td>440</td> <td></td> | | 7.0 | | | 7.0 | - 0 | | 440 | 440 | | 440 | 440 | |
| Total Split (s) 40.0 40.0 40.0 40.0 90.0 90.0 90.0 90.0 Total Split (%) 30.8% 30.8% 30.8% 30.8% 69.2% 69.2% 69.2% 69.2% Maximum Green (s) 33.7 33.7 33.6 33.6 83.6 83.6 84.0 84.0 Yellow Time (s) 5.3 5.3 5.4 5.4 5.4 5.4 5.0 5.0 All-Red Time (s) 1.0< | ` , | | | | | | | | | | | | |
| Total Split (%) 30.8% 30.8% 30.8% 30.8% 69.2% 69.2% 69.2% 69.2% Maximum Green (s) 33.7 33.7 33.6 33.6 83.6 83.6 84.0 84.0 Yellow Time (s) 5.3 5.3 5.3 5.4 5.4 5.4 5.4 5.4 5.0 5.0 All-Red Time (s) 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 | , | | | | | | | | | | | | |
| Maximum Green (s) 33.7 33.6 33.6 83.6 83.6 84.0 84.0 Yellow Time (s) 5.3 5.3 5.4 5.4 5.4 5.4 5.0 5.0 All-Red Time (s) 1.0 <td></td> | | | | | | | | | | | | | |
| Yellow Time (s) 5.3 5.3 5.4 5.4 5.4 5.4 5.0 5.0 All-Red Time (s) 1.0 </td <td></td> | | | | | | | | | | | | | |
| All-Red Time (s) 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 | | | | | | | | | | | | | |
| Lost Time Adjust (s) -1.3 -1.4 -1.4 -1.0 Total Lost Time (s) 5.0 5.0 5.0 5.0 Lead/Lag Lead-Lag Optimize? Vehicle Extension (s) 6.0 8.0 6.0 6.0 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<> | | | | | | | | | | | | | |
| Total Lost Time (s) 5.0 5.0 5.0 5.0 Lead/Lag Lead-Lag Optimize? Vehicle Extension (s) 6.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 < | | 1.0 | | | 1.0 | | | 1.0 | | | 1.0 | | |
| Lead/Lag Lead-Lag Optimize? Vehicle Extension (s) 6.0 8.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.5 9 7.5 9 7.5 9 7.5 9 7.5 9 7.5 9 7.5 9 7.5 9 7.5 9 7.5 9 7.5 9 7.5 9 7.5 <td></td> | | | | | | | | | | | | | |
| Lead-Lag Optimize? Vehicle Extension (s) 6.0 7.2 7.2 7.2 7.2 7.2 7.5 9 75. | | | 3.0 | | | 3.0 | | | 3.0 | | | 5.0 | |
| Vehicle Extension (s) 6.0 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.0 30.0 30.0 30.0 30.0 30.0 30.0 30.0 30.0 30.0 30.0 75.9 75.9 75.9 75.9 75.9 75.9 | | | | | | | | | | | | | |
| Minimum Gap (s) 3.4 3.0 20.0 20.0 30.0 30.0 30.0 30.0 30.0 30.0 30.0 30.0 30.0 30.0 30.0 30.0 30.0 30.0 75.9 75.9 75.9 75.9 75.9 75.9 75.9 75.9 75.9 75.9 75.9 | | 6.0 | 6.0 | | 6.0 | 6.0 | | 6.0 | 6.0 | | 6.0 | 6.0 | |
| Time Before Reduce (s) 10.0 10.0 10.0 10.0 20.0 30.0 75.9 75. | | | | | | | | | | | | | |
| Time To Reduce (s) 20.0 20.0 20.0 20.0 30.0 75.9 <td></td> | | | | | | | | | | | | | |
| Recall Mode None None None Min | | | | | | | | | | | | | |
| Act Effct Green (s) 33.0 33.0 75.9 75.9 Actuated g/C Ratio 0.28 0.28 0.64 0.64 v/c Ratio 0.83 0.34 0.56 0.87 Control Delay 61.2 39.0 14.5 27.5 Queue Delay 0.0 0.0 0.0 0.0 Total Delay 61.2 39.0 14.5 27.5 LOS E D B C | | | | | | | | | | | | | |
| Actuated g/C Ratio 0.28 0.28 0.64 0.64 v/c Ratio 0.83 0.34 0.56 0.87 Control Delay 61.2 39.0 14.5 27.5 Queue Delay 0.0 0.0 0.0 0.0 Total Delay 61.2 39.0 14.5 27.5 LOS E D B C | | | | | | | | | | | | | |
| v/c Ratio 0.83 0.34 0.56 0.87 Control Delay 61.2 39.0 14.5 27.5 Queue Delay 0.0 0.0 0.0 0.0 Total Delay 61.2 39.0 14.5 27.5 LOS E D B C | ` , | | | | | | | | | | | | |
| Control Delay 61.2 39.0 14.5 27.5 Queue Delay 0.0 0.0 0.0 0.0 Total Delay 61.2 39.0 14.5 27.5 LOS E D B C | | | | | | | | | | | | | |
| Queue Delay 0.0 0.0 0.0 0.0 Total Delay 61.2 39.0 14.5 27.5 LOS E D B C | | | | | | | | | | | | | |
| Total Delay 61.2 39.0 14.5 27.5 LOS E D B C | • | | | | | | | | | | | 0.0 | |
| | Total Delay | | | | | 39.0 | | | 14.5 | | | | |
| Approach Delay 61.2 39.0 14.5 27.5 | LOS | | | | | D | | | | | | С | |
| | Approach Delay | | 61.2 | | | 39.0 | | | 14.5 | | | 27.5 | |

Combined (2023) PM 01/16/2020

1: Smithfield Road & Poole Road

| | ≯ | - | \ | 1 | ← | * | 1 | 1 | 1 | > | ↓ | \checkmark |
|-------------------------|----------|----------|----------|-----|----------|----------|-----|------|-----|-------------|----------|--------------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Approach LOS | | Е | | | D | | | В | | | С | |
| Queue Length 50th (ft) | | 265 | | | 108 | | | 248 | | | 609 | |
| Queue Length 95th (ft) | | #429 | | | 173 | | | 344 | | | 852 | |
| Internal Link Dist (ft) | | 3585 | | | 1998 | | | 1207 | | | 4871 | |
| Turn Bay Length (ft) | | | | | | | | | | | | |
| Base Capacity (vph) | | 431 | | | 511 | | | 1216 | | | 1320 | |
| Starvation Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Spillback Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Storage Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Reduced v/c Ratio | | 0.77 | | | 0.31 | | | 0.49 | | | 0.76 | |
| Intersection Summary | | | | | | | | | | | | |

Area Type: Other

Cycle Length: 130

Actuated Cycle Length: 119.1

Natural Cycle: 75

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.87 Intersection Signal Delay: 30.0 Intersection Capacity Utilization 87.6%

Intersection LOS: C
ICU Level of Service E

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 1: Smithfield Road & Poole Road



SMITHFIELD ROAD & SANDY RUN

| | <u> ر</u> | _ | / | ~ | — | • | ~ | 1 | / | \ | Ţ | √ |
|-------------------------|-----------|-------|------|---------|----------|----------|----------|-------|----------|----------|-------|----------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | LDI | WDL | 1 | WBIT | ITEL | 4 | INDIX | OBL | 4 | OBIT |
| Traffic Volume (vph) | 36 | 4 | 9 | 20 | 4 | 75 | 10 | 1001 | 7 | 17 | 332 | 8 |
| Future Volume (vph) | 36 | 4 | 9 | 20 | 4 | 75 75 | 10 | 1001 | 7 | 17 | 332 | 8 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (%) | 1300 | -1% | 1300 | 1300 | -2% | 1300 | 1300 | 2% | 1300 | 1300 | -3% | 1300 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.975 | 1.00 | 1.00 | 0.897 | 1.00 | 1.00 | 0.999 | 1.00 | 1.00 | 0.997 | 1.00 |
| Flt Protected | | 0.964 | | | 0.037 | | | 0.555 | | | 0.998 | |
| Satd. Flow (prot) | 0 | 1760 | 0 | 0 | 1671 | 0 | 0 | 1842 | 0 | 0 | 1881 | 0 |
| Flt Permitted | U | 0.678 | U | U | 0.926 | U | U | 0.996 | U | U | 0.934 | U |
| Satd. Flow (perm) | 0 | 1238 | 0 | 0 | 1563 | 0 | 0 | 1835 | 0 | 0 | 1761 | 0 |
| Right Turn on Red | U | 1200 | No | U | 1000 | No | U | 1000 | No | U | 1701 | No |
| Satd. Flow (RTOR) | | | 140 | | | 110 | | | 140 | | | 110 |
| Link Speed (mph) | | 25 | | | 25 | | | 45 | | | 45 | |
| Link Distance (ft) | | 1346 | | | 1337 | | | 4951 | | | 431 | |
| Travel Time (s) | | 36.7 | | | 36.5 | | | 75.0 | | | 6.5 | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 40 | 4 | 10 | 22 | 4 | 83 | 11 | 1112 | 8 | 19 | 369 | 9 |
| Shared Lane Traffic (%) | 10 | • | 10 | | | 00 | | 1112 | Ů | 10 | 000 | Ū |
| Lane Group Flow (vph) | 0 | 54 | 0 | 0 | 109 | 0 | 0 | 1131 | 0 | 0 | 397 | 0 |
| Turn Type | Perm | NA | Ū | Perm | NA | Ū | Perm | NA | v | pm+pt | NA | Ū |
| Protected Phases | 1 01111 | 4 | | 1 01111 | 8 | | 1 01111 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | • | | 8 | ŭ | | 2 | _ | | 6 | · | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | | 1 | 6 | |
| Switch Phase | • | • | | ŭ | ŭ | | _ | _ | | • | ŭ | |
| Minimum Initial (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 12.0 | 12.0 | | 7.0 | 12.0 | |
| Minimum Split (s) | 12.0 | 12.0 | | 12.0 | 12.0 | | 18.0 | 18.0 | | 12.0 | 18.0 | |
| Total Split (s) | 30.0 | 30.0 | | 30.0 | 30.0 | | 90.0 | 90.0 | | 15.0 | 90.0 | |
| Total Split (%) | 22.2% | 22.2% | | 22.2% | 22.2% | | 66.7% | 66.7% | | 11.1% | 66.7% | |
| Maximum Green (s) | 25.6 | 25.6 | | 25.4 | 25.4 | | 84.7 | 84.7 | | 10.4 | 84.2 | |
| Yellow Time (s) | 3.2 | 3.2 | | 3.3 | 3.3 | | 4.3 | 4.3 | | 3.0 | 4.8 | |
| All-Red Time (s) | 1.2 | 1.2 | | 1.3 | 1.3 | | 1.0 | 1.0 | | 1.6 | 1.0 | |
| Lost Time Adjust (s) | | 0.6 | | | 0.4 | | | -0.3 | | | -0.8 | |
| Total Lost Time (s) | | 5.0 | | | 5.0 | | | 5.0 | | | 5.0 | |
| Lead/Lag | | | | | | | Lag | Lag | | Lead | | |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | | Yes | | |
| Vehicle Extension (s) | 2.0 | 2.0 | | 2.0 | 2.0 | | 6.0 | 6.0 | | 2.0 | 6.0 | |
| Minimum Gap (s) | 2.0 | 2.0 | | 2.0 | 2.0 | | 3.0 | 3.0 | | 2.0 | 3.0 | |
| Time Before Reduce (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 15.0 | 15.0 | | 0.0 | 15.0 | |
| Time To Reduce (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 30.0 | 30.0 | | 0.0 | 30.0 | |
| Recall Mode | None | None | | None | None | | Min | Min | | None | Min | |
| Act Effct Green (s) | | 11.2 | | | 11.2 | | | 68.0 | | | 68.0 | |
| Actuated g/C Ratio | | 0.13 | | | 0.13 | | | 0.76 | | | 0.76 | |
| v/c Ratio | | 0.35 | | | 0.56 | | | 0.81 | | | 0.30 | |
| Control Delay | | 45.1 | | | 50.5 | | | 13.0 | | | 4.1 | |
| Queue Delay | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Total Delay | | 45.1 | | | 50.5 | | | 13.0 | | | 4.1 | |
| LOS | | D | | | D | | | В | | | Α | |
| Approach Delay | | 45.1 | | | 50.5 | | | 13.0 | | | 4.1 | |

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|-------------------------|----------|----------|----------|----------|----------|-----|-----|------|----------|-------------|----------|--------------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Approach LOS | | D | | | D | | | В | | | Α | |
| Queue Length 50th (ft) | | 27 | | | 55 | | | 312 | | | 54 | |
| Queue Length 95th (ft) | | 75 | | | 131 | | | 631 | | | 106 | |
| Internal Link Dist (ft) | | 1266 | | | 1257 | | | 4871 | | | 351 | |
| Turn Bay Length (ft) | | | | | | | | | | | | |
| Base Capacity (vph) | | 353 | | | 445 | | | 1707 | | | 1725 | |
| Starvation Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Spillback Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Storage Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Reduced v/c Ratio | | 0.15 | | | 0.24 | | | 0.66 | | | 0.23 | |
| Intersection Summary | | | | | | | | | | | | |

Area Type: Other

Cycle Length: 135

Actuated Cycle Length: 89.4

Natural Cycle: 90

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.81 Intersection Signal Delay: 14.4 Intersection Capacity Utilization 72.7%

Intersection LOS: B ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 2: Smithfield Road & Sandy Run



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|--------------------------------|----------|-------------|------|---------|----------|----------|----------|------------|-------------|----------|-------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| | LDL | 4 | LDIN | VVDL | VVD1 | WDIX | NDL | 1ND1 | NDIX | JDL | | JUL |
| Lane Configurations | 28 | | 4 | 11 | 4 | 57 | 7 | 457 | 28 | 73 | 944 | 30 |
| Traffic Volume (vph) | 26 28 | 4 4 | 4 | 11 | 4 4 | 57 57 | 7 7 | 457 457 | 28 | 73 73 | 944 | 30 |
| Future Volume (vph) | 1900 | | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Ideal Flow (vphpl) | 1900 | 1900 -1% | 1900 | 1900 | -2% | 1900 | 1900 | 2% | 1900 | 1900 | -3% | 1900 |
| Grade (%) Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.986 | 1.00 | 1.00 | 0.892 | 1.00 | 1.00 | 0.992 | 1.00 | 1.00 | 0.996 | 1.00 |
| Fit Protected | | 0.962 | | | 0.092 | | | 0.992 | | | 0.990 | |
| Satd. Flow (prot) | 0 | 1776 | 0 | 0 | 1665 | 0 | 0 | 1828 | 0 | 0 | 1877 | 0 |
| Flt Permitted | U | 0.743 | U | U | 0.940 | U | U | 0.984 | U | U | 0.927 | U |
| Satd. Flow (perm) | 0 | 1371 | 0 | 0 | 1577 | 0 | 0 | 1800 | 0 | 0 | 1746 | 0 |
| Right Turn on Red | U | 1371 | No | U | 1377 | No | U | 1000 | No | U | 1740 | No |
| Satd. Flow (RTOR) | | | INO | | | NO | | | INO | | | NO |
| Link Speed (mph) | | 25 | | | 25 | | | 45 | | | 45 | |
| Link Distance (ft) | | 1346 | | | 1337 | | | 4951 | | | 431 | |
| Travel Time (s) | | 36.7 | | | 36.5 | | | 75.0 | | | 6.5 | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 31 | 4 | 4 | 12 | 4 | 63 | 8 | 508 | 31 | 81 | 1049 | 33 |
| Shared Lane Traffic (%) | 01 | 7 | 7 | 12 | 7 | 00 | U | 300 | 01 | 01 | 1043 | 33 |
| Lane Group Flow (vph) | 0 | 39 | 0 | 0 | 79 | 0 | 0 | 547 | 0 | 0 | 1163 | 0 |
| Turn Type | Perm | NA | U | Perm | NA | U | Perm | NA | U | pm+pt | NA | U |
| Protected Phases | i Cilli | 4 | | 1 Cilli | 8 | | 1 Cilli | 2 | | 1 | 6 | |
| Permitted Phases | 4 | 7 | | 8 | J | | 2 | _ | | 6 | Ū | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | | 1 | 6 | |
| Switch Phase | • | | | Ū | Ū | | _ | _ | | | Ū | |
| Minimum Initial (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 12.0 | 12.0 | | 7.0 | 12.0 | |
| Minimum Split (s) | 12.0 | 12.0 | | 12.0 | 12.0 | | 18.0 | 18.0 | | 12.0 | 18.0 | |
| Total Split (s) | 30.0 | 30.0 | | 30.0 | 30.0 | | 90.0 | 90.0 | | 15.0 | 90.0 | |
| Total Split (%) | 22.2% | 22.2% | | 22.2% | 22.2% | | 66.7% | 66.7% | | 11.1% | 66.7% | |
| Maximum Green (s) | 25.6 | 25.6 | | 25.4 | 25.4 | | 84.7 | 84.7 | | 10.4 | 84.2 | |
| Yellow Time (s) | 3.2 | 3.2 | | 3.3 | 3.3 | | 4.3 | 4.3 | | 3.0 | 4.8 | |
| All-Red Time (s) | 1.2 | 1.2 | | 1.3 | 1.3 | | 1.0 | 1.0 | | 1.6 | 1.0 | |
| Lost Time Adjust (s) | | 0.6 | | | 0.4 | | | -0.3 | | | -0.8 | |
| Total Lost Time (s) | | 5.0 | | | 5.0 | | | 5.0 | | | 5.0 | |
| Lead/Lag | | | | | | | Lag | Lag | | Lead | | |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | | Yes | | |
| Vehicle Extension (s) | 2.0 | 2.0 | | 2.0 | 2.0 | | 6.0 | 6.0 | | 2.0 | 6.0 | |
| Minimum Gap (s) | 2.0 | 2.0 | | 2.0 | 2.0 | | 3.0 | 3.0 | | 2.0 | 3.0 | |
| Time Before Reduce (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 15.0 | 15.0 | | 0.0 | 15.0 | |
| Time To Reduce (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 30.0 | 30.0 | | 0.0 | 30.0 | |
| Recall Mode | None | None | | None | None | | Min | Min | | None | Min | |
| Act Effct Green (s) | | 9.5 | | | 9.5 | | | 76.7 | | | 76.7 | |
| Actuated g/C Ratio | | 0.10 | | | 0.10 | | | 0.84 | | | 0.84 | |
| v/c Ratio | | 0.28 | | | 0.48 | | | 0.36 | | | 0.80 | |
| Control Delay | | 47.9 | | | 53.8 | | | 3.5 | | | 11.4 | |
| Queue Delay | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Total Delay | | 47.9 | | | 53.8 | | | 3.5 | | | 11.4 | |
| LOS | | D | | | D | | | Α | | | В | |
| Approach Delay | | 47.9 | | | 53.8 | | | 3.5 | | | 11.4 | |

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|-------------------------|----------|----------|----------|-----|----------|-----|-----|------|-----|-------------|----------|--------------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Approach LOS | | D | | | D | | | Α | | | В | |
| Queue Length 50th (ft) | | 22 | | | 47 | | | 72 | | | 321 | |
| Queue Length 95th (ft) | | 58 | | | 100 | | | 134 | | | 682 | |
| Internal Link Dist (ft) | | 1266 | | | 1257 | | | 4871 | | | 351 | |
| Turn Bay Length (ft) | | | | | | | | | | | | |
| Base Capacity (vph) | | 392 | | | 451 | | | 1593 | | | 1701 | |
| Starvation Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Spillback Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Storage Cap Reductn | | 0 | | | 0 | | | 0 | | | 0 | |
| Reduced v/c Ratio | | 0.10 | | | 0.18 | | | 0.34 | | | 0.68 | |
| Intersection Summary | | | | | | | | | | | | |

Area Type: Other

Cycle Length: 135

Actuated Cycle Length: 91.6

Natural Cycle: 60

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.80 Intersection Signal Delay: 11.7 Intersection Capacity Utilization 101.5%

Intersection LOS: B
ICU Level of Service G

Analysis Period (min) 15

Splits and Phases: 2: Smithfield Road & Sandy Run



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|--|-------------|------------|------|------------|--------------|------|-------------|---------------|------|-------------|-------------|----------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ₽ | | | 4 | | 1 | 1> | | 7 | 1> | |
| Traffic Volume (vph) | 92 | 4 | 15 | 22 | 4 | 82 | 13 | 1094 | 8 | 19 | 363 | 27 |
| Future Volume (vph) | 92 | 4 | 15 | 22 | 4 | 82 | 13 | 1094 | 8 | 19 | 363 | 27 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (%) | | -1% | | | -2% | | | 2% | | | -3% | |
| Storage Length (ft) | 0 | | 0 | 0 | | 0 | 100 | | 0 | 100 | | 0 |
| Storage Lanes | 0 | | 0 | 0 | | 0 | 1 | | 0 | 1 | | 0 |
| Taper Length (ft) | 100 | | | 100 | | | 100 | | | 100 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | 0.981 | | | 0.897 | | | 0.999 | | | 0.990 | |
| Flt Protected | | 0.960 | | | 0.990 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1763 | 0 | 0 | 1671 | 0 | 1752 | 1842 | 0 | 1796 | 1872 | 0 |
| Flt Permitted | | 0.566 | | | 0.934 | | 0.511 | | | 0.050 | | |
| Satd. Flow (perm) | 0 | 1039 | 0 | 0 | 1576 | 0 | 942 | 1842 | 0 | 95 | 1872 | 0 |
| Right Turn on Red | | | No | | | No | | | No | | | No |
| Satd. Flow (RTOR) | | | | | | | | | | | | |
| Link Speed (mph) | | 25 | | | 25 | | | 45 | | | 45 | |
| Link Distance (ft) | | 1346 | | | 1337 | | | 4951 | | | 431 | |
| Travel Time (s) | | 36.7 | | | 36.5 | | | 75.0 | | | 6.5 | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 102 | 4 | 17 | 24 | 4 | 91 | 14 | 1216 | 9 | 21 | 403 | 30 |
| Shared Lane Traffic (%) | | 400 | | | | | | | | • | | |
| Lane Group Flow (vph) | 0 | 123 | 0 | 0 | 119 | 0 | _ 14 | 1225 | 0 | 21 | 433 | 0 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | pm+pt | NA | |
| Protected Phases | | 4 | | • | 8 | | • | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | 8 | 0 | | 2 | • | | 6 | 0 | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | | 1 | 6 | |
| Switch Phase | 7.0 | 7.0 | | 7.0 | 7.0 | | 40.0 | 40.0 | | 7.0 | 40.0 | |
| Minimum Initial (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 12.0 | 12.0 | | 7.0 | 12.0 | |
| Minimum Split (s) | 12.0 | 12.0 | | 12.0 | 12.0 30.0 | | 18.0 | 18.0 | | 12.0 | 18.0 | |
| Total Split (s) | 30.0 | 30.0 | | 30.0 | | | 90.0 | 90.0 66.7% | | 15.0 | 90.0 | |
| Total Split (%) | 22.2% | 22.2% | | 22.2% | 22.2% | | 66.7% | | | 11.1% | 66.7% | |
| Maximum Green (s) | 25.6 | 25.6 | | 25.4 | 25.4 | | 84.7 | 84.7 | | 10.4 | 84.2 | |
| Yellow Time (s) | 3.2 1.2 | 3.2 1.2 | | 3.3 1.3 | 3.3 1.3 | | 4.3 | 4.3 1.0 | | 3.0 1.6 | 4.8 | |
| All-Red Time (s) | 1.2 | 0.6 | | 1.3 | 0.4 | | 1.0 -0.3 | -0.3 | | 0.4 | 1.0 -0.8 | |
| Lost Time Adjust (s) Total Lost Time (s) | | 5.0 | | | 5.0 | | -0.3 5.0 | -0.3 5.0 | | 5.0 | -0.6 5.0 | |
| Lead/Lag | | 5.0 | | | 5.0 | | | | | Lead | 5.0 | |
| Lead-Lag Optimize? | | | | | | | Lag Yes | Lag Yes | | Yes | | |
| Vehicle Extension (s) | 2.0 | 2.0 | | 2.0 | 2.0 | | 6.0 | 6.0 | | 2.0 | 6.0 | |
| Minimum Gap (s) | 2.0 | 2.0 | | 2.0 | 2.0 | | 3.0 | 3.0 | | 2.0 | 3.0 | |
| Time Before Reduce (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 15.0 | 15.0 | | 0.0 | 15.0 | |
| Time To Reduce (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 30.0 | 30.0 | | 0.0 | 30.0 | |
| Recall Mode | None | None | | None | None | | Min | Min | | None | Min | |
| Act Effct Green (s) | INOITE | 16.8 | | NOHE | 16.8 | | 87.3 | 87.3 | | 91.5 | 91.5 | |
| Actuated g/C Ratio | | 0.14 | | | 0.14 | | 0.74 | 0.74 | | 0.77 | 0.77 | |
| v/c Ratio | | 0.14 | | | 0.14 | | 0.74 | 0.74 | | 0.17 | 0.77 | |
| Control Delay | | 90.3 | | | 55.9 | | 7.2 | 26.2 | | 5.6 | 5.2 | |
| Queue Delay | | 0.0 | | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| QUEUE DEIAY | | 0.0 | | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |

Poole Road Project RKA Synchro 10 Report Page 3

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|-------------------------|----------|----------|----------|----------|----------|----------|------|----------|----------|-------------|----------|--------------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Total Delay | | 90.3 | | | 55.9 | | 7.2 | 26.2 | | 5.6 | 5.2 | |
| LOS | | F | | | Ε | | Α | С | | Α | Α | |
| Approach Delay | | 90.3 | | | 55.9 | | | 26.0 | | | 5.2 | |
| Approach LOS | | F | | | Ε | | | С | | | Α | |
| Queue Length 50th (ft) | | 86 | | | 80 | | 2 | 547 | | 3 | 84 | |
| Queue Length 95th (ft) | | 169 | | | 153 | | 12 | #1380 | | 11 | 157 | |
| Internal Link Dist (ft) | | 1266 | | | 1257 | | | 4871 | | | 351 | |
| Turn Bay Length (ft) | | | | | | | 100 | | | 100 | | |
| Base Capacity (vph) | | 220 | | | 335 | | 694 | 1357 | | 217 | 1591 | |
| Starvation Cap Reductn | | 0 | | | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | | 0 | | | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | | 0 | | | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | | 0.56 | | | 0.36 | | 0.02 | 0.90 | | 0.10 | 0.27 | |
| Interception Cummery | | | | | | | | | | | | |

Intersection Summary

Area Type: Other

Cycle Length: 135

Actuated Cycle Length: 118.4

Natural Cycle: 90

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.90 Intersection Signal Delay: 27.0 Intersection Capacity Utilization 79.3%

Intersection LOS: C ICU Level of Service D

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 2: Smithfield Road & Sandy Run



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|-------------------------|----------|-------|------|-------|----------|------|-------------|-------------|-------------|----------|-------------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | LDL | 4 | LDIK | WDL | 4 | WBIX | NDL | 1101 | NDIX | ODL | 1 | ODIT |
| | 66 | • | 7 | 12 | 4 | 62 | 13 | 499 | 31 | 80 | 1032 | 93 |
| Traffic Volume (vph) | | 4 | 7 | 12 | | 62 | 13 | | 31 | 80 | | 93 |
| Future Volume (vph) | 66 | 4 | | | 4 | | | 499 | | | 1032 | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (%) | • | -1% | • | • | -2% | • | 400 | 2% | • | 400 | -3% | • |
| Storage Length (ft) | 0 | | 0 | 0 | | 0 | 100 | | 0 | 100 | | 0 |
| Storage Lanes | 0 | | 0 | 0 | | 0 | 1 | | 0 | 1 | | 0 |
| Taper Length (ft) | 100 | | | 100 | | | 100 | | | 100 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | 0.987 | | | 0.892 | | | 0.991 | | | 0.988 | |
| Flt Protected | | 0.959 | | | 0.992 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1772 | 0 | 0 | 1665 | 0 | 1752 | 1828 | 0 | 1796 | 1868 | 0 |
| Flt Permitted | | 0.701 | | | 0.952 | | 0.118 | | | 0.334 | | |
| Satd. Flow (perm) | 0 | 1295 | 0 | 0 | 1598 | 0 | 218 | 1828 | 0 | 631 | 1868 | 0 |
| Right Turn on Red | | | No | | | No | | | No | | | No |
| Satd. Flow (RTOR) | | | | | | | | | | | | |
| Link Speed (mph) | | 25 | | | 25 | | | 45 | | | 45 | |
| Link Distance (ft) | | 1346 | | | 1337 | | | 4951 | | | 431 | |
| Travel Time (s) | | 36.7 | | | 36.5 | | | 75.0 | | | 6.5 | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 73 | 4 | 8 | 13 | 4 | 69 | 14 | 554 | 34 | 89 | 1147 | 103 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 85 | 0 | 0 | 86 | 0 | 14 | 588 | 0 | 89 | 1250 | 0 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | pm+pt | NA | |
| Protected Phases | . • | 4 | | | 8 | | | 2 | | 1 | 6 | |
| Permitted Phases | 4 | • | | 8 | | | 2 | _ | | 6 | • | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | | 1 | 6 | |
| Switch Phase | • | | | Ū | ŭ | | _ | _ | | • | · | |
| Minimum Initial (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 12.0 | 12.0 | | 7.0 | 12.0 | |
| Minimum Split (s) | 12.0 | 12.0 | | 12.0 | 12.0 | | 18.0 | 18.0 | | 12.0 | 18.0 | |
| Total Split (s) | 30.0 | 30.0 | | 30.0 | 30.0 | | 90.0 | 90.0 | | 15.0 | 90.0 | |
| Total Split (%) | 22.2% | 22.2% | | 22.2% | 22.2% | | 66.7% | 66.7% | | 11.1% | 66.7% | |
| Maximum Green (s) | 25.6 | 25.6 | | 25.4 | 25.4 | | 84.7 | 84.7 | | 10.4 | 84.2 | |
| Yellow Time (s) | 3.2 | 3.2 | | 3.3 | 3.3 | | 4.3 | 4.3 | | 3.0 | 4.8 | |
| All-Red Time (s) | 1.2 | 1.2 | | 1.3 | 1.3 | | 1.0 | 1.0 | | 1.6 | 1.0 | |
| Lost Time Adjust (s) | 1.2 | 0.6 | | 1.5 | 0.4 | | -0.3 | -0.3 | | 0.4 | -0.8 | |
| Total Lost Time (s) | | 5.0 | | | 5.0 | | -0.3 5.0 | -0.3 5.0 | | 5.0 | -0.6 5.0 | |
| | | 5.0 | | | 5.0 | | | | | Lead | 5.0 | |
| Lead/Lag | | | | | | | Lag | Lag | | | | |
| Lead-Lag Optimize? | 2.0 | 2.0 | | 2.0 | 2.0 | | Yes | Yes | | Yes | 6.0 | |
| Vehicle Extension (s) | 2.0 | 2.0 | | 2.0 | 2.0 | | 6.0 | 6.0 | | 2.0 | 6.0 | |
| Minimum Gap (s) | 2.0 | 2.0 | | 2.0 | 2.0 | | 3.0 | 3.0 | | 2.0 | 3.0 | |
| Time Before Reduce (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 15.0 | 15.0 | | 0.0 | 15.0 | |
| Time To Reduce (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 30.0 | 30.0 | | 0.0 | 30.0 | |
| Recall Mode | None | None | | None | None | | Min | Min | | None | Min | |
| Act Effct Green (s) | | 11.1 | | | 11.1 | | 61.5 | 61.5 | | 73.6 | 73.6 | |
| Actuated g/C Ratio | | 0.12 | | | 0.12 | | 0.65 | 0.65 | | 0.77 | 0.77 | |
| v/c Ratio | | 0.56 | | | 0.46 | | 0.10 | 0.50 | | 0.16 | 0.86 | |
| Control Delay | | 58.1 | | | 50.9 | | 8.5 | 10.4 | | 3.4 | 16.0 | |
| Queue Delay | | 0.0 | | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |

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|-------------------------|----------|---------|-----|-----|----------|-----|------|----------|-----|----------|----------|----------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Total Delay | | 58.1 | | | 50.9 | | 8.5 | 10.4 | | 3.4 | 16.0 | |
| LOS | | Ε | | | D | | Α | В | | Α | В | |
| Approach Delay | | 58.1 | | | 50.9 | | | 10.3 | | | 15.2 | |
| Approach LOS | | Ε | | | D | | | В | | | В | |
| Queue Length 50th (ft) | | 54 | | | 54 | | 3 | 161 | | 10 | 397 | |
| Queue Length 95th (ft) | | 108 | | | 107 | | 13 | 277 | | 25 | #875 | |
| Internal Link Dist (ft) | | 1266 | | | 1257 | | | 4871 | | | 351 | |
| Turn Bay Length (ft) | | | | | | | 100 | | | 100 | | |
| Base Capacity (vph) | | 352 | | | 434 | | 190 | 1598 | | 615 | 1789 | |
| Starvation Cap Reductn | | 0 | | | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | | 0 | | | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | | 0 | | | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | | 0.24 | | | 0.20 | | 0.07 | 0.37 | | 0.14 | 0.70 | |
| Intersection Summary | | | | | | | | | | | | |

Intersection Summary

Area Type: Other

Cycle Length: 135 Actuated Cycle Length: 95 Natural Cycle: 65

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.86 Intersection Signal Delay: 17.0 Intersection Capacity Utilization 85.8%

Intersection LOS: B ICU Level of Service E

Analysis Period (min) 15

^{# 95}th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.





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|-------------------------|----------|---------|----------|-------|----------|------|-------|-------|------|-------|----------|------|
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| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | 7 | 1- | | 7 | ĵ, | |
| Traffic Volume (vph) | 107 | 4 | 16 | 22 | 4 | 82 | 14 | 1094 | 8 | 19 | 363 | 31 |
| Future Volume (vph) | 107 | 4 | 16 | 22 | 4 | 82 | 14 | 1094 | 8 | 19 | 363 | 31 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (%) | | -1% | | | -2% | | | 2% | | | -3% | |
| Storage Length (ft) | 0 | | 0 | 0 | | 0 | 100 | | 0 | 100 | | 0 |
| Storage Lanes | 0 | | 0 | 0 | | 0 | 1 | | 0 | 1 | | 0 |
| Taper Length (ft) | 100 | | | 100 | | | 100 | | | 100 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | 0.983 | | | 0.897 | | | 0.999 | | | 0.988 | |
| Flt Protected | | 0.960 | | | 0.990 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1767 | 0 | 0 | 1671 | 0 | 1752 | 1842 | 0 | 1796 | 1868 | 0 |
| Flt Permitted | | 0.575 | | | 0.934 | | 0.509 | | | 0.044 | | |
| Satd. Flow (perm) | 0 | 1058 | 0 | 0 | 1576 | 0 | 939 | 1842 | 0 | 83 | 1868 | 0 |
| Right Turn on Red | | | No | | | No | | | No | | | No |
| Satd. Flow (RTOR) | | | | | | | | | | | | |
| Link Speed (mph) | | 25 | | | 25 | | | 45 | | | 45 | |
| Link Distance (ft) | | 1346 | | | 1337 | | | 4951 | | | 431 | |
| Travel Time (s) | | 36.7 | | | 36.5 | | | 75.0 | | | 6.5 | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 119 | 4 | 18 | 24 | 4 | 91 | 16 | 1216 | 9 | 21 | 403 | 34 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 141 | 0 | 0 | 119 | 0 | 16 | 1225 | 0 | 21 | 437 | 0 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | pm+pt | NA | |
| Protected Phases | | 4 | | | 8 | | | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 12.0 | 12.0 | | 7.0 | 12.0 | |
| Minimum Split (s) | 12.0 | 12.0 | | 12.0 | 12.0 | | 18.0 | 18.0 | | 12.0 | 18.0 | |
| Total Split (s) | 30.0 | 30.0 | | 30.0 | 30.0 | | 90.0 | 90.0 | | 15.0 | 90.0 | |
| Total Split (%) | 22.2% | 22.2% | | 22.2% | 22.2% | | 66.7% | 66.7% | | 11.1% | 66.7% | |
| Maximum Green (s) | 25.6 | 25.6 | | 25.4 | 25.4 | | 84.7 | 84.7 | | 10.4 | 84.2 | |
| Yellow Time (s) | 3.2 | 3.2 | | 3.3 | 3.3 | | 4.3 | 4.3 | | 3.0 | 4.8 | |
| All-Red Time (s) | 1.2 | 1.2 | | 1.3 | 1.3 | | 1.0 | 1.0 | | 1.6 | 1.0 | |
| Lost Time Adjust (s) | | 0.6 | | | 0.4 | | -0.3 | -0.3 | | 0.4 | -0.8 | |
| Total Lost Time (s) | | 5.0 | | | 5.0 | | 5.0 | 5.0 | | 5.0 | 5.0 | |
| Lead/Lag | | | | | | | Lag | Lag | | Lead | | |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | | Yes | | |
| Vehicle Extension (s) | 2.0 | 2.0 | | 2.0 | 2.0 | | 6.0 | 6.0 | | 2.0 | 6.0 | |
| Minimum Gap (s) | 2.0 | 2.0 | | 2.0 | 2.0 | | 3.0 | 3.0 | | 2.0 | 3.0 | |
| Time Before Reduce (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 15.0 | 15.0 | | 0.0 | 15.0 | |
| Time To Reduce (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 30.0 | 30.0 | | 0.0 | 30.0 | |
| Recall Mode | None | None | | None | None | | Min | Min | | None | Min | |
| Act Effct Green (s) | | 18.9 | | | 18.9 | | 86.7 | 86.7 | | 93.2 | 93.2 | |
| Actuated g/C Ratio | | 0.15 | | | 0.15 | | 0.71 | 0.71 | | 0.76 | 0.76 | |
| v/c Ratio | | 0.87 | | | 0.49 | | 0.02 | 0.94 | | 0.13 | 0.31 | |
| Control Delay | | 92.8 | | | 54.4 | | 8.1 | 33.1 | | 6.3 | 5.7 | |
| Queue Delay | | 0.0 | | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |

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|-------------------------|----------|----------|----------|-----|----------|-----|------|-------|-----|----------|----------|--------------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Total Delay | | 92.8 | | | 54.4 | | 8.1 | 33.1 | | 6.3 | 5.7 | |
| LOS | | F | | | D | | Α | С | | Α | Α | |
| Approach Delay | | 92.8 | | | 54.4 | | | 32.8 | | | 5.7 | |
| Approach LOS | | F | | | D | | | С | | | Α | |
| Queue Length 50th (ft) | | 114 | | | 90 | | 4 | 918 | | 4 | 97 | |
| Queue Length 95th (ft) | | #210 | | | 153 | | 13 | #1380 | | 11 | 159 | |
| Internal Link Dist (ft) | | 1266 | | | 1257 | | | 4871 | | | 351 | |
| Turn Bay Length (ft) | | | | | | | 100 | | | 100 | | |
| Base Capacity (vph) | | 217 | | | 324 | | 665 | 1306 | | 204 | 1538 | |
| Starvation Cap Reductn | | 0 | | | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | | 0 | | | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | | 0 | | | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | | 0.65 | | | 0.37 | | 0.02 | 0.94 | | 0.10 | 0.28 | |
| Intersection Summary | | | | | | | | | | | | |

Intersection Summary

Area Type: Other

Cycle Length: 135

Actuated Cycle Length: 122.2

Natural Cycle: 110

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.94 Intersection Signal Delay: 32.1 Intersection Capacity Utilization 80.2%

Intersection LOS: C ICU Level of Service D

Analysis Period (min) 15

^{# 95}th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.





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|---------------------------------|----------|--------------|------|-------|------------|------|-------------|-------------|------|------------|----------------|--------------|
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| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | 7 | 12 | | 15 | T _a | |
| Traffic Volume (vph) | 76 | 4 | 8 | 12 | 4 | 62 | 14 | 499 | 31 | 80 | 1032 | 109 |
| Future Volume (vph) | 76 | 4 | 8 | 12 | 4 | 62 | 14 | 499 | 31 | 80 | 1032 | 109 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (%) | | -1% | | | -2% | | | 2% | | | -3% | |
| Storage Length (ft) | 0 | .,. | 0 | 0 | _,, | 0 | 100 | _,, | 0 | 100 | | 0 |
| Storage Lanes | 0 | | 0 | 0 | | 0 | 1 | | 0 | 1 | | 0 |
| Taper Length (ft) | 100 | | Ū | 100 | | Ů | 100 | | ŭ | 100 | | · |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | 0.987 | | | 0.892 | | | 0.991 | | | 0.986 | |
| Flt Protected | | 0.958 | | | 0.992 | | 0.950 | 0.00 | | 0.950 | 0.000 | |
| Satd. Flow (prot) | 0 | 1770 | 0 | 0 | 1665 | 0 | 1752 | 1828 | 0 | 1796 | 1864 | 0 |
| Flt Permitted | | 0.694 | · | · | 0.954 | · | 0.102 | .020 | · | 0.334 | | • |
| Satd. Flow (perm) | 0 | 1282 | 0 | 0 | 1601 | 0 | 188 | 1828 | 0 | 631 | 1864 | 0 |
| Right Turn on Red | · | 1202 | No | Ū | 1001 | No | 100 | 1020 | No | 001 | 1001 | No |
| Satd. Flow (RTOR) | | | 110 | | | 110 | | | | | | |
| Link Speed (mph) | | 25 | | | 25 | | | 45 | | | 45 | |
| Link Distance (ft) | | 1346 | | | 1337 | | | 4951 | | | 431 | |
| Travel Time (s) | | 36.7 | | | 36.5 | | | 75.0 | | | 6.5 | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 84 | 4 | 9 | 13 | 4 | 69 | 16 | 554 | 34 | 89 | 1147 | 121 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 97 | 0 | 0 | 86 | 0 | 16 | 588 | 0 | 89 | 1268 | 0 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | pm+pt | NA | |
| Protected Phases | | 4 | | | 8 | | | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | | 1 | 6 | |
| Switch Phase | | | | | | | 400 | 40.0 | | | 40.0 | |
| Minimum Initial (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 12.0 | 12.0 | | 7.0 | 12.0 | |
| Minimum Split (s) | 12.0 | 12.0 | | 12.0 | 12.0 | | 18.0 | 18.0 | | 12.0 | 18.0 | |
| Total Split (s) | 30.0 | 30.0 | | 30.0 | 30.0 | | 90.0 | 90.0 | | 15.0 | 90.0 | |
| Total Split (%) | 22.2% | 22.2% | | 22.2% | 22.2% | | 66.7% | 66.7% | | 11.1% | 66.7% | |
| Maximum Green (s) | 25.6 | 25.6 | | 25.4 | 25.4 | | 84.7 | 84.7 | | 10.4 | 84.2 | |
| Yellow Time (s) | 3.2 | 3.2 | | 3.3 | 3.3 | | 4.3 | 4.3 | | 3.0 | 4.8 | |
| All-Red Time (s) | 1.2 | 1.2 | | 1.3 | 1.3 | | 1.0 | 1.0 | | 1.6 | 1.0 | |
| Lost Time Adjust (s) | | 0.6 5.0 | | | 0.4 5.0 | | -0.3 5.0 | -0.3 5.0 | | 0.4 5.0 | -0.8 5.0 | |
| Total Lost Time (s) Lead/Lag | | 5.0 | | | 5.0 | | Lag | Lag | | Lead | 5.0 | |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | | Yes | | |
| Vehicle Extension (s) | 2.0 | 2.0 | | 2.0 | 2.0 | | 6.0 | 6.0 | | 2.0 | 6.0 | |
| Minimum Gap (s) | 2.0 | 2.0 | | 2.0 | 2.0 | | 3.0 | 3.0 | | 2.0 | 3.0 | |
| Time Before Reduce (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 15.0 | 15.0 | | 0.0 | 15.0 | |
| Time To Reduce (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 30.0 | 30.0 | | 0.0 | 30.0 | |
| Recall Mode | None | None | | None | None | | Min | Min | | None | Min | |
| Act Effct Green (s) | | 12.1 | | | 12.1 | | 63.3 | 63.3 | | 75.4 | 75.4 | |
| Actuated g/C Ratio | | 0.12 | | | 0.12 | | 0.65 | 0.65 | | 0.77 | 0.77 | |
| v/c Ratio | | 0.61 | | | 0.43 | | 0.13 | 0.50 | | 0.16 | 0.88 | |
| Control Delay | | 60.8 | | | 49.9 | | 10.3 | 10.8 | | 3.7 | 18.1 | |
| Queue Delay | | 0.0 | | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| | | | | | | | | | | | | |

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|-------------------------|----------|----------|----------|-----|----------|-----|------|------|-----|-------------|----------|--------------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Total Delay | | 60.8 | | | 49.9 | | 10.3 | 10.8 | | 3.7 | 18.1 | |
| LOS | | Ε | | | D | | В | В | | Α | В | |
| Approach Delay | | 60.8 | | | 49.9 | | | 10.8 | | | 17.2 | |
| Approach LOS | | Ε | | | D | | | В | | | В | |
| Queue Length 50th (ft) | | 65 | | | 56 | | 3 | 168 | | 11 | 447 | |
| Queue Length 95th (ft) | | 120 | | | 106 | | 16 | 293 | | 27 | #1130 | |
| Internal Link Dist (ft) | | 1266 | | | 1257 | | | 4871 | | | 351 | |
| Turn Bay Length (ft) | | | | | | | 100 | | | 100 | | |
| Base Capacity (vph) | | 338 | | | 423 | | 160 | 1561 | | 609 | 1760 | |
| Starvation Cap Reductn | | 0 | | | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | | 0 | | | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | | 0 | | | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | | 0.29 | | | 0.20 | | 0.10 | 0.38 | | 0.15 | 0.72 | |
| Intersection Summary | | | | | | | | | | | | |

Intersection Summary

Area Type: Other

Cycle Length: 135

Actuated Cycle Length: 97.8

Natural Cycle: 65

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.88 Intersection Signal Delay: 18.7 Intersection Capacity Utilization 86.4%

Intersection LOS: B ICU Level of Service E

Analysis Period (min) 15

^{# 95}th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.





SMITHFIELD ROAD & MEADOW RUN

| Intersection | | | | | | | | | | | | |
|------------------------|--------|-------|-------|--------|--------|-------|--------|------|------|--------|------|------|
| Int Delay, s/veh | 1.4 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | | 4 | | | 4 | |
| Traffic Vol, veh/h | 4 | 4 | 4 | 4 | 4 | 34 | 4 | 1108 | 4 | 5 | 355 | 6 |
| Future Vol, veh/h | 4 | 4 | 4 | 4 | 4 | 34 | 4 | 1108 | 4 | 5 | 355 | 6 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | ·- | ·- | None | · - | ·- | None | - | _ | None | _ | _ | None |
| Storage Length | - | - | _ | - | - | _ | - | _ | - | _ | _ | _ |
| Veh in Median Storage | e,# - | 0 | _ | - | 0 | _ | - | 0 | - | _ | 0 | _ |
| Grade, % | _ | 0 | _ | _ | 0 | _ | _ | 0 | _ | _ | 0 | _ |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 4 | 4 | 4 | 4 | 4 | 38 | 4 | 1231 | 4 | 6 | 394 | 7 |
| | | | | | | | | | | | | |
| Major/Minor I | Minor2 | | ı | Minor1 | | ı | Major1 | | | Major2 | | |
| Conflicting Flow All | 1672 | 1653 | 398 | 1655 | 1654 | 1233 | 401 | 0 | 0 | 1235 | 0 | 0 |
| Stage 1 | 410 | 410 | - | 1241 | 1241 | - | - | - | - | - | - | - |
| Stage 2 | 1262 | 1243 | _ | 414 | 413 | _ | - | _ | - | _ | _ | _ |
| Critical Hdwy | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 | 4.12 | _ | - | 4.12 | _ | _ |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | _ | 6.12 | 5.52 | _ | - | _ | - | _ | _ | _ |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | _ | 6.12 | 5.52 | _ | - | _ | - | _ | _ | _ |
| Follow-up Hdwy | | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 | 2.218 | _ | - | 2.218 | _ | _ |
| Pot Cap-1 Maneuver | 76 | 98 | 652 | 78 | 98 | 216 | 1158 | _ | - | 564 | _ | _ |
| Stage 1 | 619 | 595 | _ | 214 | 247 | _ | - | _ | - | _ | _ | _ |
| Stage 2 | 208 | 246 | _ | 616 | 594 | _ | - | _ | - | _ | _ | _ |
| Platoon blocked, % | | | | | | | | _ | - | | _ | _ |
| Mov Cap-1 Maneuver | 59 | 96 | 652 | 73 | 96 | 216 | 1158 | - | - | 564 | _ | - |
| Mov Cap-2 Maneuver | 59 | 96 | - | 73 | 96 | - | - | - | - | - | _ | - |
| Stage 1 | 612 | 587 | - | 212 | 244 | - | _ | - | _ | _ | _ | _ |
| Stage 2 | 167 | 243 | - | 599 | 586 | - | - | - | - | - | - | - |
| Ŭ | | | | | | | | | | | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 44.6 | | | 35.2 | | | 0 | | | 0.2 | | |
| HCM LOS | Е | | | Е | | | | | | | | |
| | | | | | | | | | | | | |
| Minor Lane/Major Mvm | nt | NBL | NBT | NBR | EBLn1\ | | SBL | SBT | SBR | | | |
| Capacity (veh/h) | | 1158 | - | - | 104 | 165 | 564 | - | - | | | |
| HCM Lane V/C Ratio | | 0.004 | - | - | 0.128 | | 0.01 | - | - | | | |
| HCM Control Delay (s) |) | 8.1 | 0 | - | 44.6 | 35.2 | 11.4 | 0 | - | | | |
| HCM Lane LOS | | Α | Α | - | Ε | Ε | В | Α | - | | | |
| HCM 95th %tile Q(veh |) | 0 | - | - | 0.4 | 1.1 | 0 | - | - | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|--------|-------|-------|--------|------------|-------|--------|------|------|--------|------|------|
| Int Delay, s/veh | 1.1 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | - ♣ | | | 4 | | | 4 | |
| Traffic Vol, veh/h | 4 | 4 | 4 | 4 | 4 | 16 | 4 | 536 | 4 | 21 | 1043 | 15 |
| Future Vol, veh/h | 4 | 4 | 4 | 4 | 4 | 16 | 4 | 536 | 4 | 21 | 1043 | 15 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | ·- | ·- | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage | e,# - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 4 | 4 | 4 | 4 | 4 | 18 | 4 | 596 | 4 | 23 | 1159 | 17 |
| | | | | | | | | | | | | |
| Major/Minor I | Minor2 | | | Minor1 | | | Major1 | | | Major2 | | |
| Conflicting Flow All | 1831 | 1822 | 1168 | 1824 | 1828 | 598 | 1176 | 0 | 0 | 600 | 0 | 0 |
| Stage 1 | 1214 | 1214 | - | 606 | 606 | - | - | - | - | - | - | - |
| Stage 2 | 617 | 608 | - | 1218 | 1222 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 | 4.12 | - | - | 4.12 | - | - |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - | 6.12 | 5.52 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - | 6.12 | 5.52 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 | 2.218 | - | - | 2.218 | - | - |
| Pot Cap-1 Maneuver | 59 | 77 | 235 | 59 | 77 | 502 | 594 | - | - | 977 | - | - |
| Stage 1 | 222 | 254 | - | 484 | 487 | - | - | - | - | - | - | - |
| Stage 2 | 477 | 486 | - | 221 | 252 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | | - | - |
| Mov Cap-1 Maneuver | 51 | 71 | 235 | 52 | 71 | 502 | 594 | - | - | 977 | _ | - |
| Mov Cap-2 Maneuver | 51 | 71 | | 52 | 71 | - | - | - | - | _ | _ | - |
| Stage 1 | 220 | 237 | - | 479 | 482 | - | - | - | - | - | - | - |
| Stage 2 | 451 | 481 | - | 198 | 235 | - | - | - | - | - | - | - |
| | | | | | | | | | | | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 59.6 | | | 35.3 | | | 0.1 | | | 0.2 | | |
| HCM LOS | F | | | Е | | | | | | | | |
| | | | | | | MDI : | 07: | 0== | 0== | | | |
| Minor Lane/Major Mvm | nt | NBL | NBT | | EBLn1\ | | SBL | SBT | SBR | | | |
| Capacity (veh/h) | | 594 | - | - | 79 | 145 | 977 | - | - | | | |
| HCM Lane V/C Ratio | | 0.007 | - | - | | 0.184 | | - | - | | | |
| HCM Control Delay (s) |) | 11.1 | 0 | - | 59.6 | 35.3 | 8.8 | 0 | - | | | |
| HCM Lane LOS | | В | Α | - | F | E | Α | Α | - | | | |
| HCM 95th %tile Q(veh |) | 0 | - | - | 0.6 | 0.6 | 0.1 | - | - | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|-----------|-------|------|--------|--------------|-----------|--------|------|------|--------|------|------|
| Int Delay, s/veh | 1.8 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | (| | | 4 | | | - 43 | |
| Traffic Vol, veh/h | 4 | 4 | 4 | 4 | 4 | 37 | 4 | 1264 | 4 | 5 | 406 | 7 |
| Future Vol, veh/h | 4 | 4 | 4 | 4 | 4 | 37 | 4 | 1264 | 4 | 5 | 406 | 7 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | _ | _ | - | _ | _ | - | _ | _ | - | _ | _ | - |
| Veh in Median Storage | e.# - | 0 | _ | _ | 0 | _ | _ | 0 | _ | _ | 0 | _ |
| Grade, % | -, | 0 | _ | _ | 0 | _ | _ | 0 | _ | _ | 0 | _ |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mymt Flow | 4 | 4 | 4 | 4 | 4 | 41 | 4 | 1404 | 4 | 6 | 451 | 8 |
| | r | r | r | , | | | ŕ | | r | J | .01 | 3 |
| Major/Minor | Minor2 | | | Minor1 | | | Major1 | | | Major2 | | |
| Conflicting Flow All | 1904 | 1883 | 455 | 1885 | 1885 | 1406 | 459 | 0 | 0 | | 0 | 0 |
| Stage 1 | 467 | 467 | | 1414 | 1414 | | - | - | - | - 100 | - | - |
| Stage 2 | 1437 | 1416 | _ | 471 | 471 | _ | _ | - | _ | _ | _ | _ |
| Critical Hdwy | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 | 4.12 | _ | _ | 4.12 | _ | |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | 0.22 | 6.12 | 5.52 | 0.22 | 7.12 | | | 7.12 | | |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | _ | 6.12 | 5.52 | _ | _ | | | _ | | |
| Follow-up Hdwy | 3.518 | | | 3.518 | | 3.318 | 2.218 | | | 2.218 | | |
| Pot Cap-1 Maneuver | 52 | 71 | 605 | 54 | 71 | 171 | 1102 | | | 485 | | |
| Stage 1 | 576 | 562 | - | 171 | 204 | 171 | 1102 | - | - | 403 | - | - |
| Stage 2 | 166 | 203 | - | 573 | 560 | - | - | - | - | - | - | - |
| Platoon blocked, % | 100 | 203 | - | 313 | 500 | - | - | - | - | - | - | - |
| | 27 | 69 | 605 | 50 | 69 | 171 | 1102 | - | - | 485 | - | - |
| Mov Cap-1 Maneuver | 37 37 | 69 | 000 | 50 | 69 | 171 | 1102 | - | - | 400 | - | - |
| Mov Cap-2 Maneuver | | 552 | - | | 201 | - | - | - | - | - | - | - |
| Stage 1 | 566 | | - | 168 | | - | - | - | - | - | - | - |
| Stage 2 | 121 | 200 | - | 555 | 550 | - | - | - | - | - | - | - |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | | | | 50.7 | | | 0 | | | 0.1 | | |
| HCM LOS | 55.5 F | | | F | | | J | | | J | | |
| 200 | | | | • | | | | | | | | |
| Minor Lane/Major Mvn | nt | NBL | NBT | NBR | EBLn1V | WBLn1 | SBL | SBT | SBR | | | |
| Capacity (veh/h) | | 1102 | - | - | 69 | 127 | 485 | - | - | | | |
| HCM Lane V/C Ratio | | 0.004 | _ | _ | 0.193 | | | _ | _ | | | |
| HCM Control Delay (s) |) | 8.3 | 0 | _ | 69.3 | 50.7 | 12.5 | 0 | _ | | | |
| HCM Lane LOS | ′ | Α | A | _ | 55.5 F | 50.7 F | 12.0 | A | _ | | | |
| HCM 95th %tile Q(veh | 1) | 0 | - | _ | 0.7 | 1.7 | 0 | - | _ | | | |
| TION JOHN JUHIE W(VEI) | '/ | J | _ | _ | 0.1 | 1.7 | J | - | _ | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|----------|------------|------|-----------|------------|-------|--------|------|------|--------|-------|------|
| Int Delay, s/veh | 1.5 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | - ♣ | | | ₽ | | | €\$ | | | 4 | |
| Traffic Vol, veh/h | 4 | 4 | 4 | 4 | 4 | 17 | 4 | 621 | 4 | 23 | 1200 | 16 |
| Future Vol, veh/h | 4 | 4 | 4 | 4 | 4 | 17 | 4 | 621 | 4 | 23 | 1200 | 16 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | _ | _ | - | _ | _ | - | _ | _ | - | _ | _ | - |
| Veh in Median Storage | e.# - | 0 | _ | _ | 0 | - | _ | 0 | _ | _ | 0 | _ |
| Grade, % | - | 0 | _ | _ | 0 | _ | _ | 0 | _ | _ | 0 | _ |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mymt Flow | 4 | 4 | 4 | 4 | 4 | 19 | 4 | 690 | 4 | 26 | 1333 | 18 |
| | , | , | r | , | г | 10 | ŕ | 500 | r | 20 | . 500 | 13 |
| Major/Minor | Minor2 | | ı | Minor1 | | I | Major1 | | | Major2 | | |
| Conflicting Flow All | 2106 | 2096 | 1342 | | 2103 | 692 | | 0 | 0 | 694 | 0 | 0 |
| Stage 1 | 1394 | 1394 | - | 700 | 700 | 032 | 1001 | - | - | - | - | - |
| Stage 2 | 712 | 702 | - | 1398 | 1403 | - | _ | - | - | - | - | - |
| Critical Hdwy | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 | 4.12 | - | - | 4.12 | - | - |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | 0.22 | 6.12 | 5.52 | 0.22 | 4.12 | - | - | 4.12 | - | - |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - | 6.12 | 5.52 | • | - | - | - | - | - | - |
| Follow-up Hdwy | | 4.018 | | 3.518 | | 3.318 | 2.218 | - | - | 2.218 | - | - |
| Pot Cap-1 Maneuver | 3.516 | 52 | 186 | 3.516 | 52 | 444 | 509 | - | - | 901 | - | - |
| | 175 | 208 | | 430 | | 444 | 509 | - | - | 901 | - | - |
| Stage 1 | | | - | | 441 206 | - | - | - | - | - | - | - |
| Stage 2 | 423 | 440 | - | 174 | 200 | - | - | - | - | - | - | - |
| Platoon blocked, % | 20 | 4.5 | 400 | 24 | 4.5 | A A A | E00 | - | - | 004 | - | - |
| Mov Cap-1 Maneuver | | 45 | 186 | 31 | 45 | 444 | 509 | - | - | 901 | - | - |
| Mov Cap-2 Maneuver | 30 | 45 | - | 31 | 45 | - | - | - | - | - | - | - |
| Stage 1 | 173 | 184 | - | 424 | 435 | - | - | - | - | - | - | - |
| Stage 2 | 396 | 434 | - | 146 | 182 | - | - | - | - | - | - | - |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | | | | 55.7 | | | 0.1 | | | 0.2 | | |
| HCM LOS | 104 F | | | 55.7 F | | | 0.1 | | | 0.2 | | |
| HOW LOS | г | | | г | | | | | | | | |
| Minor Lane/Major Mvn | nt | NBL | NBT | NBR | EBLn1\ | WBLn1 | SBL | SBT | SBR | | | |
| Capacity (veh/h) | | 509 | - | - | 49 | 98 | 901 | - | - | | | |
| HCM Lane V/C Ratio | | 0.009 | _ | _ | | 0.283 | | _ | _ | | | |
| HCM Control Delay (s |) | 12.1 | 0 | _ | 104 | 55.7 | 9.1 | 0 | _ | | | |
| HCM Lane LOS | , | В | Ā | _ | F | F | A | Ā | _ | | | |
| HCM 95th %tile Q(veh | 1) | 0 | - | _ | 0.9 | 1.1 | 0.1 | - | _ | | | |
| | '/ | 0 | | | 0.5 | 1.1 | 5.1 | | | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|-----------|-----------|-------|-----------|-----------|--------|-----------|------|-------|----------|------|------|
| Int Delay, s/veh | 1.9 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | | 4 | 11211 | <u> </u> | 412 | |
| Traffic Vol, veh/h | 4 | 4 | 4 | 4 | 4 | 37 | 4 | 1279 | 4 | 5 | 410 | 7 |
| Future Vol, veh/h | 4 | 4 | 4 | 4 | 4 | 37 | 4 | 1279 | 4 | 5 | 410 | 7 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | Stop | Stop - | None | Stop - | Stop - | None | 1166 | 1166 | None | 1166 | 1166 | None |
| Storage Length | - | - | NOHE | - | - | NOHE | - | - | INOHE | - | - | NOHE |
| Veh in Median Storage | . # | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| • | €,# - | | - | - | | | - | | - | - | | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 4 | 4 | 4 | 4 | 4 | 41 | 4 | 1421 | 4 | 6 | 456 | 8 |
| | | | | | | | | | | | | |
| | Minor2 | 4655 | | Minor1 | 16 | | Major1 | | | Major2 | | |
| Conflicting Flow All | 1926 | 1905 | 460 | 1907 | 1907 | 1423 | 464 | 0 | 0 | 1425 | 0 | 0 |
| Stage 1 | 472 | 472 | - | 1431 | 1431 | - | - | - | - | - | - | - |
| Stage 2 | 1454 | 1433 | - | 476 | 476 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 | 4.12 | - | - | 4.12 | - | - |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - | 6.12 | 5.52 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - | 6.12 | 5.52 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 | 2.218 | - | - | 2.218 | - | - |
| Pot Cap-1 Maneuver | 50 | 69 | 601 | 52 | 68 | 167 | 1097 | - | - | 477 | - | - |
| Stage 1 | 573 | 559 | - | 167 | 200 | - | - | - | - | - | - | - |
| Stage 2 | 162 | 200 | - | 570 | 557 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | | - | - |
| Mov Cap-1 Maneuver | 35 | 67 | 601 | 48 | 66 | 167 | 1097 | _ | _ | 477 | _ | _ |
| Mov Cap-2 Maneuver | 35 | 67 | - | 48 | 66 | - | - | _ | _ | - | _ | _ |
| Stage 1 | 563 | 549 | _ | 164 | 196 | _ | _ | _ | _ | _ | _ | _ |
| Stage 2 | 117 | 196 | - | 552 | 548 | - | - | _ | - | _ | _ | - |
| J - | | | | | | | | | | | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 72.9 | | | 53 | | | 0 | | | 0.1 | | |
| HCM LOS | 72.5 F | | | F | | | J | | | 0.1 | | |
| | ' | | | | | | | | | | | |
| Minor Lane/Major Mvn | nt | NBL | NBT | NRR | EBLn1\ | NRI n1 | SBL | SBT | SBR | | | |
| Capacity (veh/h) | | 1097 | - | - 1011 | 66 | 123 | 477 | - | ODIX | | | |
| HCM Lane V/C Ratio | | 0.004 | _ | _ | | 0.407 | | _ | _ | | | |
| HCM Control Delay (s) | ١ | 8.3 | 0 | - | 72.9 | 53 | 12.6 | 0 | - | | | |
| HCM Lane LOS | ' | 0.5 A | A | - | 72.9 F | F | 12.0 B | A | - | | | |
| HCM 95th %tile Q(veh | ٨ | 0 | - | - | 0.7 | 1.7 | 0 | A | - | | | |
| TION SOUL /OUR Q(VEH |) | U | - | - | 0.7 | 1.7 | U | - | - | | | |

| Movement EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL SBT SBR | | | | | | | | | | | | | | |
|--|----------------------|--------|------|-------|--------|---------|---------|--------|-----|-----|--------|------|-----|------|
| Int Delay, s/veh | Intersection | | | | | | | | | | | | | |
| Lane Configurations | Int Delay, s/veh | 1.6 | | | | | | | | | | | | |
| Lane Configurations | Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Traffic Vol, veh/h 4 | - | | | | | 4 | | | | | | 4 | | |
| Future Vol, veh/h Conflicting Peds, #hr O O O O O O O O O O O O O O O O O O O | | 4 | • | 4 | 4 | 4 | 17 | 4 | 631 | 4 | 23 | 1216 | 16 | |
| Conflicting Peds, #/hr | | | | | | | | | | | | | | |
| Sign Control Stop | | | | | | | | | | | | | | |
| RT Channelized | | | | - | - | | - | | - | - | | | - | |
| Storage Length | | - | - | | | | | | - | | - | | | |
| Veh in Median Storage, # - 0 | | _ | _ | - | _ | _ | - | _ | _ | - | _ | _ | - | |
| Grade, % - 0 | | - # - | 0 | _ | _ | 0 | _ | _ | ٥ | _ | _ | ٥ | _ | |
| Peak Hour Factor 90 | • | -, " - | | _ | | | | | | - | - | | _ | |
| Heavy Vehicles, % 2 2 2 2 2 2 2 2 2 | | an | | | | | | | | | | | ٩n | |
| Mymit Flow 4 4 4 4 4 9 4 701 4 26 1351 18 Major/Minor Minor1 Major1 Major2 Major2 Minor1 Major3 Major3 Major4 Major4 </td <td></td> | | | | | | | | | | | | | | |
| Major/Minor Minor2 Minor1 Major1 Major2 Major3 Major4 Major5 Major5 Major6 Major7 Major6 Major | • | | | | | | | | | | | | | |
| Conflicting Flow All 2135 2125 1360 2127 2132 703 1369 0 0 705 0 0 Stage 1 | WIVITIL I TOW | 4 | 4 | 4 | 4 | 4 | 19 | 4 | 701 | 4 | 20 | 1001 | 10 | |
| Conflicting Flow All 2135 2125 1360 2127 2132 703 1369 0 0 705 0 0 Stage 1 | Major/Minor | Minor2 | | ı | Minor1 | | ı | Major1 | | ı | Major2 | | | |
| Stage 1 | Conflicting Flow All | | 2125 | | | 2132 | | | 0 | | | 0 | 0 | |
| Stage 2 | • | | | | | | | _ | _ | _ | _ | _ | _ | |
| Critical Hdwy 7.12 6.52 6.22 7.12 6.52 6.22 4.12 - 4.12 - - Critical Hdwy Stg 1 6.12 5.52 - 6.12 5.52 - - - - - - Critical Hdwy Stg 2 6.12 5.52 - 6.12 5.52 - | • | | | _ | | | _ | _ | _ | _ | _ | _ | _ | |
| Critical Hdwy Stg 1 6.12 5.52 - 6.12 5.52 - | • | | | 6.22 | | | 6.22 | 4.12 | _ | _ | 4.12 | _ | _ | |
| Critical Hdwy Stg 2 6.12 5.52 - 6.12 5.52 - | • | | | - | | | - | - | _ | _ | - | _ | _ | |
| Follow-up Hdwy 3.518 4.018 3.318 3.518 4.018 3.318 2.218 2.218 Pot Cap-1 Maneuver 36 50 182 36 49 438 501 - 893 Stage 1 171 204 - 424 436 | , , | | | _ | | | _ | _ | _ | _ | _ | _ | _ | |
| Pot Cap-1 Maneuver 36 50 182 36 49 438 501 - - 893 - - Stage 1 171 204 - 424 436 - <t< td=""><td>, ,</td><td></td><td></td><td>3.318</td><td></td><td></td><td>3.318</td><td>2.218</td><td>_</td><td>_</td><td>2.218</td><td>_</td><td>_</td><td></td></t<> | , , | | | 3.318 | | | 3.318 | 2.218 | _ | _ | 2.218 | _ | _ | |
| Stage 1 171 204 - 424 436 - | | | | | | | | | _ | _ | | _ | _ | |
| Stage 2 417 435 - 170 202 - | • | | | | | | _ | _ | _ | _ | _ | _ | _ | |
| Platoon blocked, % Mov Cap-1 Maneuver 28 43 182 29 42 438 501 - 893 Mov Cap-2 Maneuver 28 43 - 29 42 Stage 1 169 179 - 418 430 Stage 2 390 429 - 142 177 Stage 2 390 429 - 142 177 Approach EB WB NB SB HCM Control Delay, s 109.5 60.2 0.1 0.2 HCM LOS F F F Minor Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR Capacity (veh/h) 501 - 47 92 893 HCM Lane V/C Ratio 0.009 - 0.284 0.302 0.029 HCM Control Delay (s) 12.2 0 - 109.5 60.2 9.2 0 - HCM Control Delay (s) 12.2 0 - 109.5 60.2 9.2 0 - HCM Lane LOS B A - F F A A - | | | | _ | | | _ | _ | _ | _ | _ | _ | _ | |
| Mov Cap-1 Maneuver 28 43 182 29 42 438 501 - 893 - - Mov Cap-2 Maneuver 28 43 - 29 42 - | | | | | | | | | _ | _ | | _ | _ | |
| Mov Cap-2 Maneuver 28 43 - 29 42 - | | 28 | 43 | 182 | 29 | 42 | 438 | 501 | _ | _ | 893 | _ | _ | |
| Stage 1 169 179 - 418 430 - | • | | | | | | - | - | _ | _ | - | _ | _ | |
| Stage 2 390 429 - 142 177 - | • | | | _ | | | _ | _ | _ | _ | _ | _ | _ | |
| Approach EB WB NB SB HCM Control Delay, s 109.5 HCM LOS 60.2 F 0.1 0.2 Minor Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR Capacity (veh/h) 501 - - 47 92 893 - - HCM Lane V/C Ratio 0.009 - - 0.284 0.302 0.029 - - HCM Control Delay (s) 12.2 0 - 109.5 60.2 9.2 0 - HCM Lane LOS B A - F F A A - | | | | _ | | | _ | _ | _ | _ | _ | _ | - | |
| HCM Control Delay, s 109.5 | J | | | | | | | | | | | | | |
| Minor Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR Capacity (veh/h) 501 - - 47 92 893 - - HCM Lane V/C Ratio 0.009 - - 0.284 0.302 0.029 - - HCM Control Delay (s) 12.2 0 - 109.5 60.2 9.2 0 - HCM Lane LOS B A - F F A A - | Approach | EB | | | WB | | | NB | | | SB | | | |
| Minor Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR Capacity (veh/h) 501 - - 47 92 893 - - HCM Lane V/C Ratio 0.009 - - 0.284 0.302 0.029 - - HCM Control Delay (s) 12.2 0 - 109.5 60.2 9.2 0 - HCM Lane LOS B A - F F A A - | HCM Control Delay, s | 109.5 | | | 60.2 | | | 0.1 | | | 0.2 | | | |
| Capacity (veh/h) 501 - - 47 92 893 - - HCM Lane V/C Ratio 0.009 - - 0.284 0.302 0.029 - - HCM Control Delay (s) 12.2 0 - 109.5 60.2 9.2 0 - HCM Lane LOS B A - F F A A - | HCM LOS | | | | F | | | | | | | | | |
| Capacity (veh/h) 501 - - 47 92 893 - - HCM Lane V/C Ratio 0.009 - - 0.284 0.302 0.029 - - HCM Control Delay (s) 12.2 0 - 109.5 60.2 9.2 0 - HCM Lane LOS B A - F F A A - | Minaul and Maria A4 | .1 | NDI | NDT | NDD | EDL - A | MDL - 4 | ODI | ODT | CDD | | | | |
| HCM Lane V/C Ratio 0.009 0.284 0.302 0.029 HCM Control Delay (s) 12.2 0 - 109.5 60.2 9.2 0 - HCM Lane LOS B A - F F A A - | | 11(| | | NRK | | | | | | | | | |
| HCM Control Delay (s) 12.2 0 - 109.5 60.2 9.2 0 - HCM Lane LOS B A - F F A A - | | | | - | - | | | | - | - | | | | |
| HCM Lane LOS | | | | | - | | | | - | - | | | | |
| | |) | | | - | | | | | - | | | | |
| HCM 95th %tile Q(veh) 0 1 1.1 0.1 | | , | | Α | - | | | | Α | - | | | | |
| | HCM 95th %tile Q(veh | 1) | 0 | - | - | 1 | 1.1 | 0.1 | - | - | | | | |

POOLE ROAD & WATER ROCK WAY / RUTLEDGE LANDING DRIVE

| Intersection | | | | | | | | | | | | |
|------------------------|--------|-------|-------|--------|------|-------|--------|-------|-------|--------|-------|-------|
| Int Delay, s/veh | 3 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 1, | | 7 | î, | | | 4 | | | 4 | |
| Traffic Vol, veh/h | 8 | 84 | 9 | 7 | 217 | 13 | 38 | 4 | 20 | 23 | 4 | 20 |
| Future Vol, veh/h | 8 | 84 | 9 | 7 | 217 | 13 | 38 | 4 | 20 | 23 | 4 | 20 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | · - | None | · - | ·- | None |
| Storage Length | 100 | - | - | 100 | - | - | - | - | - | - | - | - |
| Veh in Median Storage | e,# - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 9 | 93 | 10 | 8 | 241 | 14 | 42 | 4 | 22 | 26 | 4 | 22 |
| | | | | | | | | | | | | |
| Major/Minor | Major1 | | ı | Major2 | | ı | Minor1 | | 1 | Minor2 | | |
| Conflicting Flow All | 255 | 0 | 0 | 103 | 0 | 0 | 393 | 387 | 98 | 393 | 385 | 248 |
| Stage 1 | | - | - | - | - | - | 116 | 116 | - | 264 | 264 | |
| Stage 2 | _ | _ | _ | _ | _ | _ | 277 | 271 | _ | 129 | 121 | _ |
| Critical Hdwy | 4.12 | _ | _ | 4.12 | _ | _ | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 |
| Critical Hdwy Stg 1 | - | _ | _ | - | _ | _ | 6.12 | 5.52 | - | 6.12 | 5.52 | - |
| Critical Hdwy Stg 2 | _ | _ | _ | _ | _ | _ | 6.12 | 5.52 | _ | 6.12 | 5.52 | _ |
| Follow-up Hdwy | 2.218 | _ | _ | 2.218 | _ | _ | 3.518 | | 3.318 | 3.518 | 4.018 | 3.318 |
| Pot Cap-1 Maneuver | 1310 | _ | - | 1489 | - | - | 566 | 547 | 958 | 566 | 549 | 791 |
| Stage 1 | - | _ | _ | - | _ | _ | 889 | 800 | - | 741 | 690 | - |
| Stage 2 | _ | _ | _ | _ | _ | _ | 729 | 685 | _ | 875 | 796 | _ |
| Platoon blocked, % | | _ | - | | - | - | _, | | | | | |
| Mov Cap-1 Maneuver | 1310 | _ | _ | 1489 | _ | _ | 542 | 540 | 958 | 544 | 542 | 791 |
| Mov Cap-2 Maneuver | - | _ | _ | - | _ | _ | 542 | 540 | - | 544 | 542 | - |
| Stage 1 | _ | _ | _ | _ | _ | _ | 883 | 794 | _ | 736 | 687 | _ |
| Stage 2 | _ | _ | - | - | - | - | 700 | 682 | _ | 844 | 790 | - |
| 3 - | | | | | | | | | | | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 0.6 | | | 0.2 | | | 11.4 | | | 11.3 | | |
| HCM LOS | 0.0 | | | ٥.٢ | | | В | | | В | | |
| 1.5111 200 | | | | | | | J | | | | | |
| Minor Lane/Major Mvm | nt . | NBLn1 | EBL | EBT | EBR | WBL | WBT | \//DD | SBLn1 | | | |
| | IL | | | | | | | | | | | |
| Capacity (veh/h) | | 630 | 1310 | - | - | 1489 | - | - | 627 | | | |
| HCM Cantral Dalay (a) | | | 0.007 | - | - | 0.005 | - | - | 0.083 | | | |
| HCM Control Delay (s) |) | 11.4 | 7.8 | - | - | 7.4 | - | - | 11.3 | | | |
| HCM Lane LOS | ١ | В | Α | - | - | A | - | - | В | | | |
| HCM 95th %tile Q(veh |) | 0.4 | 0 | - | - | 0 | - | - | 0.3 | | | |

| - | | | | | | | | | | | | |
|------------------------|--------|-------|-------|--------|------------|-------|--------|------------|-------|--------|-------|--------|
| Intersection | | | | | | | | | | | | |
| Int Delay, s/veh | 2.2 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 13 | | Ŋ | 1 2 | | | - ♣ | | | 4 | |
| Traffic Vol, veh/h | 24 | 247 | 38 | 14 | 94 | 25 | 12 | 4 | 17 | 16 | 4 | 20 |
| Future Vol, veh/h | 24 | 247 | 38 | 14 | 94 | 25 | 12 | 4 | 17 | 16 | 4 | 20 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | | | None | | | None . |
| Storage Length | 100 | - | - | 100 | - | - | - | - | - | - | - | - |
| Veh in Median Storage | e,# - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | _ |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | _ |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 27 | 274 | 42 | 16 | 104 | 28 | 13 | 4 | 19 | 18 | 4 | 22 |
| | | | | | | | | | | | | |
| Major/Minor I | Major1 | | ı | Major2 | | ı | Minor1 | | | Minor2 | | |
| Conflicting Flow All | 132 | 0 | 0 | 316 | 0 | 0 | 512 | 513 | 295 | 511 | 520 | 118 |
| Stage 1 | _ | _ | _ | _ | _ | _ | 349 | 349 | - | 150 | 150 | _ |
| Stage 2 | _ | _ | - | _ | _ | - | 163 | 164 | _ | 361 | 370 | _ |
| Critical Hdwy | 4.12 | _ | _ | 4.12 | _ | _ | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 |
| Critical Hdwy Stg 1 | - | _ | _ | - | _ | _ | 6.12 | 5.52 | - | 6.12 | 5.52 | - |
| Critical Hdwy Stg 2 | _ | _ | _ | _ | _ | _ | 6.12 | 5.52 | _ | 6.12 | 5.52 | _ |
| Follow-up Hdwy | 2.218 | _ | - | 2.218 | _ | - | 3.518 | 4.018 | 3.318 | | 4.018 | 3.318 |
| Pot Cap-1 Maneuver | 1453 | _ | - | 1244 | _ | - | 472 | 465 | 744 | 473 | 461 | 934 |
| Stage 1 | _ | _ | _ | _ | _ | _ | 667 | 633 | _ | 853 | 773 | _ |
| Stage 2 | _ | _ | _ | _ | _ | _ | 839 | 762 | _ | 657 | 620 | _ |
| Platoon blocked, % | | _ | _ | | _ | _ | | | | | | |
| Mov Cap-1 Maneuver | 1453 | _ | - | 1244 | _ | - | 447 | 450 | 744 | 447 | 446 | 934 |
| Mov Cap-2 Maneuver | - | _ | - | - | _ | - | 447 | 450 | - | 447 | 446 | - |
| Stage 1 | _ | _ | - | _ | _ | - | 654 | 621 | _ | 837 | 763 | - |
| Stage 2 | _ | _ | - | _ | _ | - | 804 | 752 | _ | 624 | 608 | - |
| 3 | | | | | | | | | | | | |
| Approach | ЕВ | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 0.6 | | | 0.8 | | | 11.8 | | | 11.4 | | |
| HCM LOS | | | | | | | В | | | В | | |
| | | | | | | | _ | | | _ | | |
| Minor Lane/Major Mvm | nt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | | | |
| Capacity (veh/h) | | 563 | 1453 | - | - | 1244 | - | - | 604 | | | |
| HCM Lane V/C Ratio | | | 0.018 | _ | _ | 0.013 | _ | _ | 0.074 | | | |
| HCM Control Delay (s) | ١ | 11.8 | 7.5 | _ | _ | 7.9 | _ | _ | 11.4 | | | |
| HCM Lane LOS | , | В | Α | _ | _ | Α | _ | _ | В | | | |
| HCM 95th %tile Q(veh |) | 0.2 | 0.1 | _ | _ | 0 | _ | _ | 0.2 | | | |
| // (10) | , | ٠.ــ | 0.1 | | | • | | | ٥.٢ | | | |

| Intersection | 2.0 | | | | | | | | | | | |
|------------------------|--------|----------|-------|--------|----------|-------|--------|-------|-----------|--------|------------|-------|
| Int Delay, s/veh | 3.8 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | } | | - 1 | ∱ | | | 4 | | | - ♣ | |
| Traffic Vol, veh/h | 13 | 92 | 10 | 8 | 237 | 20 | 42 | 4 | 22 | 43 | 4 | 36 |
| Future Vol, veh/h | 13 | 92 | 10 | 8 | 237 | 20 | 42 | 4 | 22 | 43 | 4 | 36 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 100 | - | - | 100 | - | - | - | - | - | - | - | - |
| Veh in Median Storage | e,# - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 14 | 102 | 11 | 9 | 263 | 22 | 47 | 4 | 24 | 48 | 4 | 40 |
| Major/Minor N | Major1 | | ı | Major2 | | ı | Minor1 | | ı | Minor2 | | |
| Conflicting Flow All | 285 | 0 | 0 | 113 | 0 | 0 | 450 | 439 | 108 | 442 | 433 | 274 |
| Stage 1 | 200 | - | - | - | - | - | 136 | 136 | - | 292 | 292 | |
| Stage 2 | _ | _ | _ | _ | _ | _ | 314 | 303 | _ | 150 | 141 | _ |
| Critical Hdwy | 4.12 | _ | _ | 4.12 | _ | _ | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 |
| Critical Hdwy Stg 1 | 7.12 | _ | _ | 7.12 | _ | _ | 6.12 | 5.52 | 0.22 | 6.12 | 5.52 | 0.22 |
| Critical Hdwy Stg 2 | _ | _ | _ | _ | _ | _ | 6.12 | 5.52 | _ | 6.12 | 5.52 | _ |
| Follow-up Hdwy | 2.218 | _ | _ | 2.218 | _ | _ | 3.518 | 4.018 | 3.318 | 3.518 | | 3.318 |
| Pot Cap-1 Maneuver | 1277 | _ | _ | 1476 | _ | _ | 519 | 512 | 946 | 526 | 516 | 765 |
| Stage 1 | | _ | _ | - | _ | _ | 867 | 784 | - | 716 | 671 | - |
| Stage 2 | _ | _ | _ | _ | _ | _ | 697 | 664 | _ | 853 | 780 | _ |
| Platoon blocked, % | | _ | _ | | _ | _ | 001 | 00. | | 000 | 100 | |
| Mov Cap-1 Maneuver | 1277 | _ | _ | 1476 | _ | _ | 482 | 503 | 946 | 502 | 507 | 765 |
| Mov Cap 1 Maneuver | | _ | _ | | _ | _ | 482 | 503 | J-10 - | 502 | 507 | |
| Stage 1 | _ | _ | _ | _ | _ | _ | 857 | 775 | _ | 708 | 667 | _ |
| Stage 2 | _ | _ | _ | _ | _ | _ | 652 | 660 | _ | 817 | 771 | _ |
| olugo L | | | | | | | 302 | 300 | | 317 | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 0.9 | | | 0.2 | | | 12.2 | | | 12.2 | | |
| HCM LOS | | | | | | | В | | | В | | |
| Minor Lanc/Major Mar | ر م | NDI 51 | EBL | EBT | EBR | \//DI | WBT | WBR | CDI n1 | | | |
| Minor Lane/Major Mvm | it l | NBLn1 | | | | WBL | VVDI | | | | | |
| Capacity (veh/h) | | 575 | 1277 | - | - | 1476 | - | - | 590 | | | |
| HCM Cantral Dalay (a) | | 0.131 | 0.011 | - | - | 0.006 | - | - | 0.156 | | | |
| HCM Control Delay (s) |) | 12.2 | 7.9 | - | - | 7.5 | - | - | 12.2 | | | |
| HCM Lane LOS | ` | В | A | - | - | Α | - | - | В | | | |
| HCM 95th %tile Q(veh |) | 0.5 | 0 | - | - | 0 | - | - | 0.6 | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|--------|-----------|------|--------|------|------|-----------|-------|-----------|-----------|-------------|--------|
| Int Delay, s/veh | 2.8 | | | | | _ | _ | _ | | _ | _ | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 1 | | 7 | 1, | | | 4 | | | 4 | |
| Traffic Vol, veh/h | 41 | 270 | 42 | 15 | 103 | 47 | 13 | 4 | 19 | 29 | 4 | 31 |
| Future Vol, veh/h | 41 | 270 | 42 | 15 | 103 | 47 | 13 | 4 | 19 | 29 | 4 | 31 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | _ | - | None | _ | - | None | | | None | | | None . |
| Storage Length | 100 | - | - | 100 | - | - | - | - | - | - | - | _ |
| Veh in Median Storage | e,# - | 0 | - | _ | 0 | - | - | 0 | - | - | 0 | _ |
| Grade, % | _ | 0 | - | _ | 0 | - | - | 0 | - | - | 0 | _ |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 46 | 300 | 47 | 17 | 114 | 52 | 14 | 4 | 21 | 32 | 4 | 34 |
| | | | | | | | | | | | | |
| Major/Minor N | Major1 | | ı | Major2 | | ı | Minor1 | | | Minor2 | | |
| Conflicting Flow All | 166 | 0 | 0 | 347 | 0 | 0 | 609 | 616 | 324 | 602 | 613 | 140 |
| Stage 1 | - | - | - | - | - | - | 416 | 416 | - | 174 | 174 | - |
| Stage 2 | _ | _ | _ | _ | _ | _ | 193 | 200 | _ | 428 | 439 | _ |
| Critical Hdwy | 4.12 | _ | _ | 4.12 | _ | _ | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 |
| Critical Hdwy Stg 1 | - | _ | _ | - | _ | _ | 6.12 | 5.52 | - | 6.12 | 5.52 | - |
| Critical Hdwy Stg 2 | _ | _ | _ | _ | _ | _ | 6.12 | 5.52 | _ | 6.12 | 5.52 | _ |
| Follow-up Hdwy | 2.218 | _ | _ | 2.218 | _ | _ | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 |
| Pot Cap-1 Maneuver | 1412 | _ | _ | 1212 | _ | _ | 407 | 406 | 717 | 412 | 408 | 908 |
| Stage 1 | - | _ | _ | | _ | _ | 614 | 592 | | 828 | 755 | - |
| Stage 2 | _ | _ | _ | _ | _ | _ | 809 | 736 | _ | 605 | 578 | _ |
| Platoon blocked, % | | _ | _ | | _ | _ | 300 | | | 3.00 | J. J | |
| Mov Cap-1 Maneuver | 1412 | _ | _ | 1212 | _ | _ | 374 | 387 | 717 | 382 | 389 | 908 |
| Mov Cap-2 Maneuver | - | _ | _ | | _ | _ | 374 | 387 | | 382 | 389 | - |
| Stage 1 | _ | _ | _ | _ | _ | _ | 594 | 572 | _ | 801 | 744 | _ |
| Stage 2 | _ | - | - | _ | _ | - | 763 | 726 | _ | 564 | 559 | - |
| J | | | | | | | | _, | | | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 0.9 | | | 0.7 | | | 12.8 | | | 12.8 | | |
| HCM LOS | 5.5 | | | 5.1 | | | 12.0 B | | | 12.0 B | | |
| | | | | | | | 5 | | | J | | |
| Minor Lane/Major Mvm | nt I | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | | | |
| Capacity (veh/h) | | 503 | 1412 | | - | 1212 | - | - | 532 | | | |
| HCM Lane V/C Ratio | | 0.08 | | _ | _ | | _ | | 0.134 | | | |
| HCM Control Delay (s) | | 12.8 | 7.6 | _ | _ | 8 | _ | _ | 12.8 | | | |
| HCM Lane LOS | | 12.0 B | Α. | _ | _ | A | _ | _ | 12.0 B | | | |
| HCM 95th %tile Q(veh |) | 0.3 | 0.1 | _ | _ | 0 | _ | _ | 0.5 | | | |
| | , | 0.0 | 0.1 | | | 3 | | | 0.0 | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|--------|-------|------|--------|----------|-------|--------|-------|-------|--------|-------|-------|
| Int Delay, s/veh | 3.9 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | 1, | | 7 | <u>f</u> | | | 4 | | | 4 | |
| Traffic Vol, veh/h | 14 | 92 | 10 | 8 | 237 | 22 | 42 | 4 | 22 | 48 | 4 | 40 |
| Future Vol, veh/h | 14 | 92 | 10 | 8 | 237 | 22 | 42 | 4 | 22 | 48 | 4 | 40 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 100 | - | - | 100 | - | - | - | - | - | - | - | - |
| Veh in Median Storage | e,# - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 16 | 102 | 11 | 9 | 263 | 24 | 47 | 4 | 24 | 53 | 4 | 44 |
| | | | | | | | | | | | | |
| Major/Minor | Major1 | | ı | Major2 | | I | Minor1 | | 1 | Minor2 | | |
| Conflicting Flow All | 287 | 0 | 0 | 113 | 0 | 0 | 457 | 445 | 108 | 447 | 438 | 275 |
| Stage 1 | - | - | - | - | - | - | 140 | 140 | - | 293 | 293 | - |
| Stage 2 | - | - | - | - | - | - | 317 | 305 | - | 154 | 145 | _ |
| Critical Hdwy | 4.12 | - | - | 4.12 | - | - | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.12 | 5.52 | - | 6.12 | 5.52 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.12 | 5.52 | - | 6.12 | 5.52 | - |
| Follow-up Hdwy | 2.218 | - | - | 2.218 | - | - | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 |
| Pot Cap-1 Maneuver | 1275 | - | - | 1476 | - | - | 514 | 508 | 946 | 522 | 512 | 764 |
| Stage 1 | - | - | - | - | - | - | 863 | 781 | - | 715 | 670 | - |
| Stage 2 | - | - | - | - | - | - | 694 | 662 | - | 848 | 777 | - |
| Platoon blocked, % | | - | - | | - | - | | | | | | |
| Mov Cap-1 Maneuver | 1275 | - | - | 1476 | - | - | 474 | 498 | 946 | 498 | 502 | 764 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 474 | 498 | - | 498 | 502 | - |
| Stage 1 | - | - | - | - | - | - | 852 | 771 | - | 706 | 666 | - |
| Stage 2 | - | - | - | - | - | - | 645 | 658 | - | 811 | 767 | - |
| | | | | | | | | | | | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 0.9 | | | 0.2 | | | 12.3 | | | 12.4 | | |
| HCM LOS | | | | | | | В | | | В | | |
| | | | | | | | | | | | | |
| Minor Lane/Major Mvm | nt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR: | | | | |
| Capacity (veh/h) | | 567 | 1275 | - | - | 1476 | - | - | 587 | | | |
| HCM Lane V/C Ratio | | 0.133 | | - | - | 0.006 | - | - | 0.174 | | | |
| HCM Control Delay (s) |) | 12.3 | 7.9 | - | - | 7.5 | - | - | 12.4 | | | |
| HCM Lane LOS | | В | Α | - | - | Α | - | - | В | | | |
| HCM 95th %tile Q(veh |) | 0.5 | 0 | - | - | 0 | - | - | 0.6 | | | |

4: Water Rock Way/Rutledge Landing Drive & Poole Road

| Intersection | | | | | | | | | | | | |
|------------------------|--------|-------|-------|--------|------|------|----------|------------|-------|------------|-------|-------|
| Int Delay, s/veh | 2.9 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 14 | 1, | | 7 | Î, | | | - ♣ | | | 4 | |
| Traffic Vol, veh/h | 45 | 270 | 42 | 15 | 103 | 52 | 13 | 4 | 19 | 32 | 4 | 33 |
| Future Vol, veh/h | 45 | 270 | 42 | 15 | 103 | 52 | 13 | 4 | 19 | 32 | 4 | 33 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | _ | - | None | - | _ | None | <u>.</u> | ·- | None | <u>'</u> - | ·- | None |
| Storage Length | 100 | - | - | 100 | - | _ | _ | _ | - | _ | _ | _ |
| Veh in Median Storage | | 0 | - | - | 0 | _ | _ | 0 | _ | _ | 0 | _ |
| Grade, % | - | 0 | - | _ | 0 | _ | _ | 0 | - | _ | 0 | _ |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 50 | 300 | 47 | 17 | 114 | 58 | 14 | 4 | 21 | 36 | 4 | 37 |
| | | | | - | | | | | | | | |
| Major/Minor I | Major1 | | ı | Major2 | | ı | Minor1 | | | Minor2 | | |
| Conflicting Flow All | 172 | 0 | 0 | 347 | 0 | 0 | 622 | 630 | 324 | 613 | 624 | 143 |
| Stage 1 | - | - | - | - | - | - | 424 | 424 | - | 177 | 177 | - |
| Stage 2 | _ | _ | _ | _ | _ | _ | 198 | 206 | _ | 436 | 447 | _ |
| Critical Hdwy | 4.12 | _ | _ | 4.12 | _ | _ | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 |
| Critical Hdwy Stg 1 | - | _ | _ | - | _ | _ | 6.12 | 5.52 | - | 6.12 | 5.52 | - |
| Critical Hdwy Stg 2 | _ | _ | _ | _ | _ | _ | 6.12 | 5.52 | _ | 6.12 | 5.52 | _ |
| Follow-up Hdwy | 2.218 | - | - | 2.218 | _ | - | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 |
| Pot Cap-1 Maneuver | 1405 | - | - | 1212 | - | - | 399 | 399 | 717 | 405 | 402 | 905 |
| Stage 1 | - | - | - | - | - | - | 608 | 587 | - | 825 | 753 | - |
| Stage 2 | - | - | - | - | - | - | 804 | 731 | - | 599 | 573 | - |
| Platoon blocked, % | | - | - | | - | - | | | | | | |
| Mov Cap-1 Maneuver | 1405 | - | - | 1212 | - | - | 365 | 379 | 717 | 375 | 382 | 905 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 365 | 379 | - | 375 | 382 | - |
| Stage 1 | - | - | - | - | - | - | 586 | 566 | - | 795 | 742 | - |
| Stage 2 | - | - | - | - | - | - | 756 | 721 | - | 556 | 552 | - |
| Ü | | | | | | | | | | | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 1 | | | 0.7 | | | 12.9 | | | 13.1 | | |
| HCM LOS | • | | | | | | В | | | В | | |
| | | | | | | | _ | | | _ | | |
| Minor Lane/Major Mvn | nt I | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | | | |
| Capacity (veh/h) | | 495 | 1405 | _ | - | 1212 | - | _ | 522 | | | |
| HCM Lane V/C Ratio | | | 0.036 | _ | _ | | _ | _ | 0.147 | | | |
| HCM Control Delay (s) |) | 12.9 | 7.7 | _ | _ | 8 | _ | _ | 13.1 | | | |
| HCM Lane LOS | ' | В | Α | _ | _ | A | _ | _ | В | | | |
| HCM 95th %tile Q(veh |) | 0.3 | 0.1 | _ | _ | 0 | _ | _ | 0.5 | | | |
| | , | 0.0 | | | | • | | | 0.0 | | | |